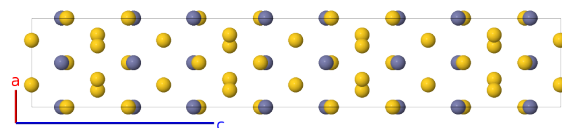
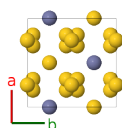
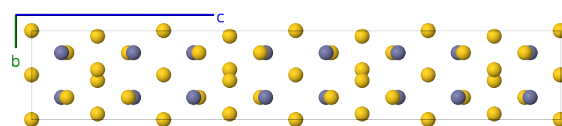
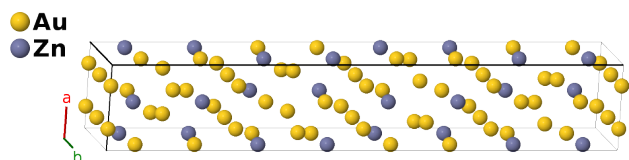


# R<sub>1</sub> Au<sub>3</sub>Zn Structure: A3B\_tI64\_142\_def\_d-001

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<https://afLOW.org/p/Q6FW>

[https://afLOW.org/p/A3B\\_tI64\\_142\\_def\\_d-001](https://afLOW.org/p/A3B_tI64_142_def_d-001)

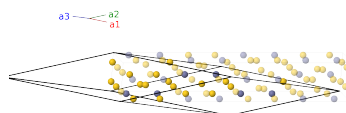


<b>Prototype</b>	Au <sub>3</sub> Zn
<b>AFLOW prototype label</b>	A3B_tI64_142_def_d-001
<b>ICSD</b>	58628
<b>Pearson symbol</b>	tI64
<b>Space group number</b>	142
<b>Space group symbol</b>	<i>I</i> 4 <sub>1</sub> / <i>acd</i>
<b>AFLOW prototype command</b>	<code>afLOW --proto=A3B_tI64_142_def_d-001 --params=a, c/a, z<sub>1</sub>, z<sub>2</sub>, x<sub>3</sub>, x<sub>4</sub></code>

- Au<sub>3</sub>Zn is known to exist in three forms, depending upon the exact composition and temperature (Hisatsune, 1998):
  - The tetragonal *R*<sub>1</sub> phase (this structure) is stable below ≈ 475K with a composition very nearly stoichiometric.
  - The orthorhombic *R*<sub>2</sub> phase is stable below ≈ 550K with a composition range somewhat wider than the *R*<sub>1</sub> phase.
  - The tetragonal *H* phase has the *D*0<sub>23</sub> structure and is stable at temperatures up to ≈ 700K over a considerably wider range of stoichiometries than either the *R*<sub>1</sub> or *R*<sub>2</sub> phases.
- (Iwaskai, 1962) gave structure of the *R*<sub>1</sub> phase in setting 1 of space group *I*4<sub>1</sub>/*acd* #142. We used FINDSYM to transform this to the standard setting 2.
- (Iwaskai, 1962) gave the lattice constants in kX units. We used the conversion factor 1 kX = 1.00202Å. (Wood, 1947)

## Body-centered Tetragonal primitive vectors

$$\begin{aligned} \mathbf{a}_1 &= -\frac{1}{2}a \hat{\mathbf{x}} + \frac{1}{2}a \hat{\mathbf{y}} + \frac{1}{2}c \hat{\mathbf{z}} \\ \mathbf{a}_2 &= \frac{1}{2}a \hat{\mathbf{x}} - \frac{1}{2}a \hat{\mathbf{y}} + \frac{1}{2}c \hat{\mathbf{z}} \\ \mathbf{a}_3 &= \frac{1}{2}a \hat{\mathbf{x}} + \frac{1}{2}a \hat{\mathbf{y}} - \frac{1}{2}c \hat{\mathbf{z}} \end{aligned}$$



## Basis vectors

	Lattice coordinates		Cartesian coordinates	Wyckoff position	Atom type
$\mathbf{B}_1$	$= (z_1 + \frac{1}{4}) \mathbf{a}_1 + z_1 \mathbf{a}_2 + \frac{1}{4} \mathbf{a}_3$	$=$	$\frac{1}{4} a \hat{\mathbf{y}} + cz_1 \hat{\mathbf{z}}$	(16d)	Au I
$\mathbf{B}_2$	$= z_1 \mathbf{a}_1 + (z_1 + \frac{1}{4}) \mathbf{a}_2 + \frac{3}{4} \mathbf{a}_3$	$=$	$\frac{1}{2} a \hat{\mathbf{x}} + \frac{1}{4} a \hat{\mathbf{y}} + c (z_1 - \frac{1}{4}) \hat{\mathbf{z}}$	(16d)	Au I
$\mathbf{B}_3$	$= -(z_1 - \frac{1}{4}) \mathbf{a}_1 - (z_1 - \frac{1}{2}) \mathbf{a}_2 +$ $\frac{3}{4} \mathbf{a}_3$	$=$	$\frac{1}{2} a \hat{\mathbf{x}} + \frac{1}{4} a \hat{\mathbf{y}} - cz_1 \hat{\mathbf{z}}$	(16d)	Au I
$\mathbf{B}_4$	$= -(z_1 - \frac{1}{2}) \mathbf{a}_1 - (z_1 - \frac{1}{4}) \mathbf{a}_2 +$ $\frac{1}{4} \mathbf{a}_3$	$=$	$\frac{1}{4} a \hat{\mathbf{y}} - c (z_1 - \frac{1}{4}) \hat{\mathbf{z}}$	(16d)	Au I
$\mathbf{B}_5$	$= -(z_1 - \frac{3}{4}) \mathbf{a}_1 - z_1 \mathbf{a}_2 + \frac{3}{4} \mathbf{a}_3$	$=$	$\frac{3}{4} a \hat{\mathbf{y}} - cz_1 \hat{\mathbf{z}}$	(16d)	Au I
$\mathbf{B}_6$	$= -z_1 \mathbf{a}_1 - (z_1 - \frac{3}{4}) \mathbf{a}_2 + \frac{1}{4} \mathbf{a}_3$	$=$	$\frac{1}{2} a \hat{\mathbf{x}} - \frac{1}{4} a \hat{\mathbf{y}} - c (z_1 - \frac{1}{4}) \hat{\mathbf{z}}$	(16d)	Au I
$\mathbf{B}_7$	$= (z_1 + \frac{3}{4}) \mathbf{a}_1 + (z_1 + \frac{1}{2}) \mathbf{a}_2 + \frac{1}{4} \mathbf{a}_3$	$=$	$\frac{1}{4} a \hat{\mathbf{y}} + c (z_1 + \frac{1}{2}) \hat{\mathbf{z}}$	(16d)	Au I
$\mathbf{B}_8$	$= (z_1 + \frac{1}{2}) \mathbf{a}_1 + (z_1 + \frac{3}{4}) \mathbf{a}_2 + \frac{3}{4} \mathbf{a}_3$	$=$	$\frac{1}{2} a \hat{\mathbf{x}} + \frac{1}{4} a \hat{\mathbf{y}} + c (z_1 + \frac{1}{4}) \hat{\mathbf{z}}$	(16d)	Au I
$\mathbf{B}_9$	$= (z_2 + \frac{1}{4}) \mathbf{a}_1 + z_2 \mathbf{a}_2 + \frac{1}{4} \mathbf{a}_3$	$=$	$\frac{1}{4} a \hat{\mathbf{y}} + cz_2 \hat{\mathbf{z}}$	(16d)	Zn I
$\mathbf{B}_{10}$	$= z_2 \mathbf{a}_1 + (z_2 + \frac{1}{4}) \mathbf{a}_2 + \frac{3}{4} \mathbf{a}_3$	$=$	$\frac{1}{2} a \hat{\mathbf{x}} + \frac{1}{4} a \hat{\mathbf{y}} + c (z_2 - \frac{1}{4}) \hat{\mathbf{z}}$	(16d)	Zn I
$\mathbf{B}_{11}$	$= -(z_2 - \frac{1}{4}) \mathbf{a}_1 - (z_2 - \frac{1}{2}) \mathbf{a}_2 +$ $\frac{3}{4} \mathbf{a}_3$	$=$	$\frac{1}{2} a \hat{\mathbf{x}} + \frac{1}{4} a \hat{\mathbf{y}} - cz_2 \hat{\mathbf{z}}$	(16d)	Zn I
$\mathbf{B}_{12}$	$= -(z_2 - \frac{1}{2}) \mathbf{a}_1 - (z_2 - \frac{1}{4}) \mathbf{a}_2 +$ $\frac{1}{4} \mathbf{a}_3$	$=$	$\frac{1}{4} a \hat{\mathbf{y}} - c (z_2 - \frac{1}{4}) \hat{\mathbf{z}}$	(16d)	Zn I
$\mathbf{B}_{13}$	$= -(z_2 - \frac{3}{4}) \mathbf{a}_1 - z_2 \mathbf{a}_2 + \frac{3}{4} \mathbf{a}_3$	$=$	$\frac{3}{4} a \hat{\mathbf{y}} - cz_2 \hat{\mathbf{z}}$	(16d)	Zn I
$\mathbf{B}_{14}$	$= -z_2 \mathbf{a}_1 - (z_2 - \frac{3}{4}) \mathbf{a}_2 + \frac{1}{4} \mathbf{a}_3$	$=$	$\frac{1}{2} a \hat{\mathbf{x}} - \frac{1}{4} a \hat{\mathbf{y}} - c (z_2 - \frac{1}{4}) \hat{\mathbf{z}}$	(16d)	Zn I
$\mathbf{B}_{15}$	$= (z_2 + \frac{3}{4}) \mathbf{a}_1 + (z_2 + \frac{1}{2}) \mathbf{a}_2 + \frac{1}{4} \mathbf{a}_3$	$=$	$\frac{1}{4} a \hat{\mathbf{y}} + c (z_2 + \frac{1}{2}) \hat{\mathbf{z}}$	(16d)	Zn I
$\mathbf{B}_{16}$	$= (z_2 + \frac{1}{2}) \mathbf{a}_1 + (z_2 + \frac{3}{4}) \mathbf{a}_2 + \frac{3}{4} \mathbf{a}_3$	$=$	$\frac{1}{2} a \hat{\mathbf{x}} + \frac{1}{4} a \hat{\mathbf{y}} + c (z_2 + \frac{1}{4}) \hat{\mathbf{z}}$	(16d)	Zn I
$\mathbf{B}_{17}$	$= \frac{1}{4} \mathbf{a}_1 + (x_3 + \frac{1}{4}) \mathbf{a}_2 + x_3 \mathbf{a}_3$	$=$	$ax_3 \hat{\mathbf{x}} + \frac{1}{4} c \hat{\mathbf{z}}$	(16e)	Au II
$\mathbf{B}_{18}$	$= \frac{3}{4} \mathbf{a}_1 - (x_3 - \frac{1}{4}) \mathbf{a}_2 - (x_3 - \frac{1}{2}) \mathbf{a}_3$	$=$	$-ax_3 \hat{\mathbf{x}} + \frac{1}{2} a \hat{\mathbf{y}} + \frac{1}{4} c \hat{\mathbf{z}}$	(16e)	Au II
$\mathbf{B}_{19}$	$= (x_3 + \frac{1}{4}) \mathbf{a}_1 + \frac{3}{4} \mathbf{a}_2 + x_3 \mathbf{a}_3$	$=$	$\frac{1}{4} a \hat{\mathbf{x}} + a (x_3 - \frac{1}{4}) \hat{\mathbf{y}} + \frac{1}{2} c \hat{\mathbf{z}}$	(16e)	Au II
$\mathbf{B}_{20}$	$= -(x_3 - \frac{1}{4}) \mathbf{a}_1 + \frac{1}{4} \mathbf{a}_2 -$ $(x_3 - \frac{1}{2}) \mathbf{a}_3$	$=$	$\frac{1}{4} a \hat{\mathbf{x}} - a (x_3 - \frac{1}{4}) \hat{\mathbf{y}}$	(16e)	Au II
$\mathbf{B}_{21}$	$= \frac{3}{4} \mathbf{a}_1 - (x_3 - \frac{3}{4}) \mathbf{a}_2 - x_3 \mathbf{a}_3$	$=$	$-ax_3 \hat{\mathbf{x}} + \frac{3}{4} c \hat{\mathbf{z}}$	(16e)	Au II
$\mathbf{B}_{22}$	$= \frac{1}{4} \mathbf{a}_1 + (x_3 + \frac{3}{4}) \mathbf{a}_2 + (x_3 + \frac{1}{2}) \mathbf{a}_3$	$=$	$a (x_3 + \frac{1}{2}) \hat{\mathbf{x}} + \frac{1}{4} c \hat{\mathbf{z}}$	(16e)	Au II
$\mathbf{B}_{23}$	$= -(x_3 - \frac{3}{4}) \mathbf{a}_1 + \frac{1}{4} \mathbf{a}_2 - x_3 \mathbf{a}_3$	$=$	$-\frac{1}{4} a \hat{\mathbf{x}} - a (x_3 - \frac{1}{4}) \hat{\mathbf{y}} + \frac{1}{2} c \hat{\mathbf{z}}$	(16e)	Au II
$\mathbf{B}_{24}$	$= (x_3 + \frac{3}{4}) \mathbf{a}_1 + \frac{3}{4} \mathbf{a}_2 + (x_3 + \frac{1}{2}) \mathbf{a}_3$	$=$	$\frac{1}{4} a \hat{\mathbf{x}} + a (x_3 + \frac{1}{4}) \hat{\mathbf{y}} + \frac{1}{2} c \hat{\mathbf{z}}$	(16e)	Au II
$\mathbf{B}_{25}$	$= (x_4 + \frac{3}{8}) \mathbf{a}_1 + (x_4 + \frac{1}{8}) \mathbf{a}_2 +$ $(2x_4 + \frac{1}{4}) \mathbf{a}_3$	$=$	$ax_4 \hat{\mathbf{x}} + a (x_4 + \frac{1}{4}) \hat{\mathbf{y}} + \frac{1}{8} c \hat{\mathbf{z}}$	(16f)	Au III
$\mathbf{B}_{26}$	$= -(x_4 - \frac{3}{8}) \mathbf{a}_1 - (x_4 - \frac{1}{8}) \mathbf{a}_2 -$ $(2x_4 - \frac{1}{4}) \mathbf{a}_3$	$=$	$-ax_4 \hat{\mathbf{x}} - a (x_4 - \frac{1}{4}) \hat{\mathbf{y}} + \frac{1}{8} c \hat{\mathbf{z}}$	(16f)	Au III
$\mathbf{B}_{27}$	$= (x_4 + \frac{1}{8}) \mathbf{a}_1 - (x_4 - \frac{3}{8}) \mathbf{a}_2 + \frac{3}{4} \mathbf{a}_3$	$=$	$-a (x_4 - \frac{1}{2}) \hat{\mathbf{x}} + a (x_4 + \frac{1}{4}) \hat{\mathbf{y}} - \frac{1}{8} c \hat{\mathbf{z}}$	(16f)	Au III
$\mathbf{B}_{28}$	$= -(x_4 - \frac{1}{8}) \mathbf{a}_1 + (x_4 + \frac{3}{8}) \mathbf{a}_2 +$ $\frac{3}{4} \mathbf{a}_3$	$=$	$a (x_4 + \frac{1}{2}) \hat{\mathbf{x}} - a (x_4 - \frac{1}{4}) \hat{\mathbf{y}} - \frac{1}{8} c \hat{\mathbf{z}}$	(16f)	Au III
$\mathbf{B}_{29}$	$= -(x_4 - \frac{5}{8}) \mathbf{a}_1 - (x_4 - \frac{7}{8}) \mathbf{a}_2 -$ $(2x_4 - \frac{3}{4}) \mathbf{a}_3$	$=$	$-a (x_4 - \frac{1}{2}) \hat{\mathbf{x}} - a (x_4 - \frac{1}{4}) \hat{\mathbf{y}} + \frac{3}{8} c \hat{\mathbf{z}}$	(16f)	Au III
$\mathbf{B}_{30}$	$= (x_4 + \frac{5}{8}) \mathbf{a}_1 + (x_4 + \frac{7}{8}) \mathbf{a}_2 +$ $(2x_4 + \frac{3}{4}) \mathbf{a}_3$	$=$	$a (x_4 + \frac{1}{2}) \hat{\mathbf{x}} + a (x_4 + \frac{1}{4}) \hat{\mathbf{y}} + \frac{3}{8} c \hat{\mathbf{z}}$	(16f)	Au III
$\mathbf{B}_{31}$	$= -(x_4 - \frac{7}{8}) \mathbf{a}_1 + (x_4 + \frac{5}{8}) \mathbf{a}_2 +$ $\frac{1}{4} \mathbf{a}_3$	$=$	$ax_4 \hat{\mathbf{x}} - a (x_4 - \frac{1}{4}) \hat{\mathbf{y}} + \frac{5}{8} c \hat{\mathbf{z}}$	(16f)	Au III

$$\mathbf{B}_{32} = \left(x_4 + \frac{7}{8}\right) \mathbf{a}_1 - \left(x_4 - \frac{5}{8}\right) \mathbf{a}_2 + \frac{1}{4} \mathbf{a}_3 = -ax_4 \hat{\mathbf{x}} + a \left(x_4 + \frac{1}{4}\right) \hat{\mathbf{y}} + \frac{5}{8}c \hat{\mathbf{z}} \quad (16f) \quad \text{Au III}$$

## References

- [1] H. Iwaskai, *Study on the Ordered Phases with Long Period in the Gold-Zinc Alloy System II. Structure Analysis of  $Au_3Zn[R_1]$ ,  $Au_3Zn[R_2]$  and  $Au_3+Zn$* , J. Phys. Soc. Jpn. **17**, 1620–1633 (1962), doi:10.1143/JPSJ.17.1620.
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