

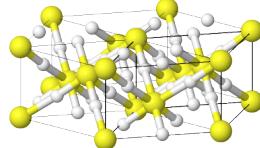
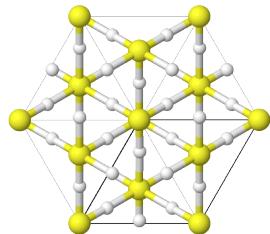
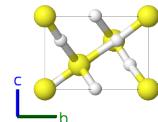
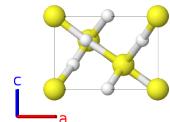
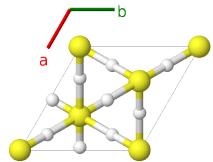
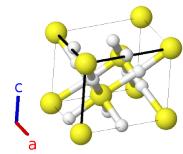
H_3S (130 GPa) Structure: A3B_hR4_160_b_a-001

This structure originally had the label A3B_hR4_160_b_a. Calls to that address will be redirected here.

Cite this page as: D. Hicks, M. J. Mehl, E. Gossett, C. Toher, O. Levy, R. M. Hanson, G. Hart, and S. Curtarolo, *The AFLOW Library of Crystallographic Prototypes: Part 2*, Comput. Mater. Sci. **161**, S1 (2019). doi: 10.1016/j.commatsci.2018.10.043

<https://aflow.org/p/P2LA>

https://aflow.org/p/A3B_hR4_160_b_a-001



Prototype

H_3S

AFLOW prototype label

A3B_hR4_160_b_a-001

ICSD

291501

Pearson symbol

hR4

Space group number

160

Space group symbol

$R\bar{3}m$

AFLOW prototype command

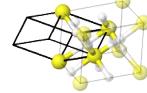
```
aflow --proto=A3B_hR4_160_b_a-001  
--params=a, c/a, x1, x2, z2
```

- This structure was found by first-principles electronic structure calculations and is predicted to be the stable structure of H_3S for pressures between 90 and 150 GPa. When $c/a \rightarrow \sqrt{8}$, $x_2 \rightarrow 1/2$ and $z_2 \rightarrow 0$ this structure continuously evolves into the cubic 200 GPa H_3S structure.

- The data presented here was computed at 130 GPa.

Rhombohedral primitive vectors

$$\begin{aligned}
 \mathbf{a}_1 &= \frac{1}{2}a\hat{\mathbf{x}} - \frac{\sqrt{3}}{6}a\hat{\mathbf{y}} + \frac{1}{3}c\hat{\mathbf{z}} \\
 \mathbf{a}_2 &= \frac{1}{\sqrt{3}}a\hat{\mathbf{y}} + \frac{1}{3}c\hat{\mathbf{z}} \\
 \mathbf{a}_3 &= -\frac{1}{2}a\hat{\mathbf{x}} - \frac{\sqrt{3}}{6}a\hat{\mathbf{y}} + \frac{1}{3}c\hat{\mathbf{z}}
 \end{aligned}$$



Basis vectors

	Lattice coordinates	Cartesian coordinates	Wyckoff position	Atom type
\mathbf{B}_1	$x_1 \mathbf{a}_1 + x_1 \mathbf{a}_2 + x_1 \mathbf{a}_3$	$= cx_1 \hat{\mathbf{z}}$	(1a)	S I
\mathbf{B}_2	$x_2 \mathbf{a}_1 + x_2 \mathbf{a}_2 + z_2 \mathbf{a}_3$	$= \frac{1}{2}a(x_2 - z_2) \hat{\mathbf{x}} + \frac{\sqrt{3}}{6}a(x_2 - z_2) \hat{\mathbf{y}} + \frac{1}{3}c(2x_2 + z_2) \hat{\mathbf{z}}$	(3b)	H I
\mathbf{B}_3	$z_2 \mathbf{a}_1 + x_2 \mathbf{a}_2 + x_2 \mathbf{a}_3$	$= -\frac{1}{2}a(x_2 - z_2) \hat{\mathbf{x}} + \frac{\sqrt{3}}{6}a(x_2 - z_2) \hat{\mathbf{y}} + \frac{1}{3}c(2x_2 + z_2) \hat{\mathbf{z}}$	(3b)	H I
\mathbf{B}_4	$x_2 \mathbf{a}_1 + z_2 \mathbf{a}_2 + x_2 \mathbf{a}_3$	$= -\frac{1}{\sqrt{3}}a(x_2 - z_2) \hat{\mathbf{y}} + \frac{1}{3}c(2x_2 + z_2) \hat{\mathbf{z}}$	(3b)	H I

References

- [1] D. Duan, Y. Liu, F. T. D. Li, X. Huang, Z. Zhao, H. Yu, B. Liu, W. Tian, and T. Cui, *Pressure-induced metallization of dense $(H_2S)_2H_2$ with high- T_c superconductivity* **4**, 6968 (2014), doi:10.1038/srep06968.