

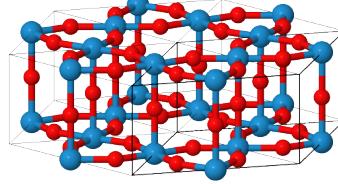
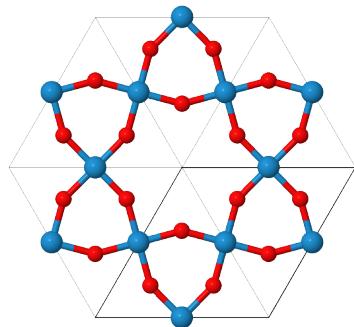
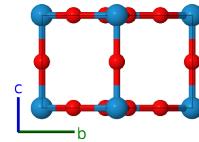
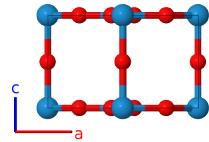
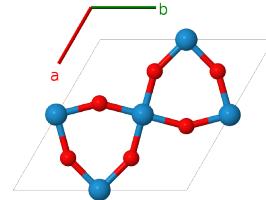
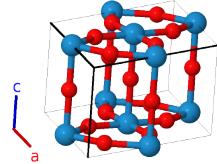
Hexagonal WO₃ Structure: A3B_hP12_191_gl_f-001

This structure originally had the label A3B_hP12_191_gl_f. Calls to that address will be redirected here.

Cite this page as: D. Hicks, M. J. Mehl, M. Esters, C. Oses, O. Levy, G. L. W. Hart, C. Toher, and S. Curtarolo, *The AFLOW Library of Crystallographic Prototypes: Part 3*, Comput. Mater. Sci. **199**, 110450 (2021), doi: 10.1016/j.commatsci.2021.110450.

<https://aflow.org/p/SQAX>

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Prototype O₃W

AFLOW prototype label A3B_hP12_191_gl_f-001

ICSD 32001

Pearson symbol hP12

Space group number 191

Space group symbol P6/mmm

AFLOW prototype command `aflow --proto=A3B_hP12_191_gl_f-001
--params=a, c/a, x3`

- All stable phases of WO_3 are distortions of the cubic $\alpha\text{-ReO}_3$ ($D0_9$) phase. Based on (Woodward, 1997 and Vogt, 1999), the known stable phases and their approximate temperature ranges are:
 - $\alpha\text{-WO}_3$ (1010-1170 K) (Vogt, 1999)
 - $\beta\text{-WO}_3$ (600-1170 K) (Vogt, 1999)
 - $\gamma\text{-WO}_3$ (290-600 K) (Vogt, 1999)
 - $\delta\text{-WO}_3$ (230-290 K) (Diehl, 1978)
 - $\epsilon\text{-WO}_3$ (below 23 K) (Woodward, 1997)
- Woodward notes that “The transition temperatures display large hysteresis effects and universal agreement is not found in the literature.”
- In addition, several other structures have been proposed and/or found:
 - The original $D0_{10}$ structure (Bräkken, 1931; Hermann, 1937), superseded by $\delta\text{-WO}_3$
 - The original $\beta\text{-WO}_3$ (Salje, 1977)
 - Hexagonal WO_3 , presumably metastable, found by (Gerand, 1979) while dehydrating $\text{WO}_3\cdot\text{H}_2\text{O}$ (this structure)
- (Gerand, 1979) determined the structure of hexagonal WO_3 by X-ray diffraction of powdered samples. They found evidence of super-reflection, indicating that the unit cell should be doubled along the c -axis, but were unable to determine the shift in atomic positions for the double unit cell. We report what they called the “half-cell” structure.

Hexagonal primitive vectors



Basis vectors

	Lattice coordinates	Cartesian coordinates	Wyckoff position	Atom type
\mathbf{B}_1 =	$\frac{1}{2}\mathbf{a}_1$	$\frac{1}{4}a\hat{\mathbf{x}} - \frac{\sqrt{3}}{4}a\hat{\mathbf{y}}$	(3f)	W I
\mathbf{B}_2 =	$\frac{1}{2}\mathbf{a}_2$	$\frac{1}{4}a\hat{\mathbf{x}} + \frac{\sqrt{3}}{4}a\hat{\mathbf{y}}$	(3f)	W I
\mathbf{B}_3 =	$\frac{1}{2}\mathbf{a}_1 + \frac{1}{2}\mathbf{a}_2$	$\frac{1}{2}a\hat{\mathbf{x}}$	(3f)	W I
\mathbf{B}_4 =	$\frac{1}{2}\mathbf{a}_1 + \frac{1}{2}\mathbf{a}_3$	$\frac{1}{4}a\hat{\mathbf{x}} - \frac{\sqrt{3}}{4}a\hat{\mathbf{y}} + \frac{1}{2}c\hat{\mathbf{z}}$	(3g)	O I
\mathbf{B}_5 =	$\frac{1}{2}\mathbf{a}_2 + \frac{1}{2}\mathbf{a}_3$	$\frac{1}{4}a\hat{\mathbf{x}} + \frac{\sqrt{3}}{4}a\hat{\mathbf{y}} + \frac{1}{2}c\hat{\mathbf{z}}$	(3g)	O I
\mathbf{B}_6 =	$\frac{1}{2}\mathbf{a}_1 + \frac{1}{2}\mathbf{a}_2 + \frac{1}{2}\mathbf{a}_3$	$\frac{1}{2}a\hat{\mathbf{x}} + \frac{1}{2}c\hat{\mathbf{z}}$	(3g)	O I
\mathbf{B}_7 =	$x_3\mathbf{a}_1 + 2x_3\mathbf{a}_2$	$\frac{3}{2}ax_3\hat{\mathbf{x}} + \frac{\sqrt{3}}{2}ax_3\hat{\mathbf{y}}$	(6l)	O II
\mathbf{B}_8 =	$-2x_3\mathbf{a}_1 - x_3\mathbf{a}_2$	$-\frac{3}{2}ax_3\hat{\mathbf{x}} + \frac{\sqrt{3}}{2}ax_3\hat{\mathbf{y}}$	(6l)	O II
\mathbf{B}_9 =	$x_3\mathbf{a}_1 - x_3\mathbf{a}_2$	$-\sqrt{3}ax_3\hat{\mathbf{y}}$	(6l)	O II
\mathbf{B}_{10} =	$-x_3\mathbf{a}_1 - 2x_3\mathbf{a}_2$	$-\frac{3}{2}ax_3\hat{\mathbf{x}} - \frac{\sqrt{3}}{2}ax_3\hat{\mathbf{y}}$	(6l)	O II
\mathbf{B}_{11} =	$2x_3\mathbf{a}_1 + x_3\mathbf{a}_2$	$\frac{3}{2}ax_3\hat{\mathbf{x}} - \frac{\sqrt{3}}{2}ax_3\hat{\mathbf{y}}$	(6l)	O II
\mathbf{B}_{12} =	$-x_3\mathbf{a}_1 + x_3\mathbf{a}_2$	$\sqrt{3}ax_3\hat{\mathbf{y}}$	(6l)	O II

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