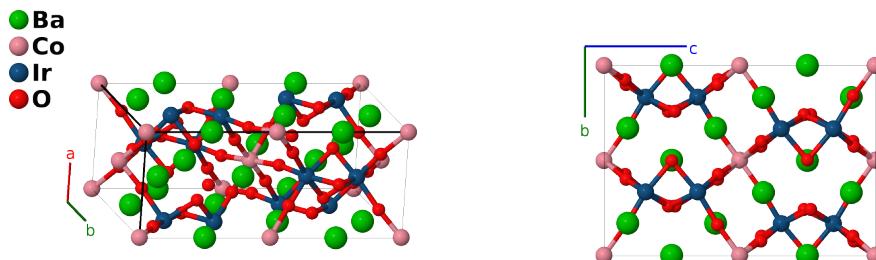


Monoclinic (I) $\text{Ba}_3\text{CoIr}_2\text{O}_9$ Structure: A3BC2D9_mC60_15_ef_a_f_e4f-001

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<https://aflow.org/p/G3XE>

https://aflow.org/p/A3BC2D9_mC60_15_ef_a_f_e4f-001



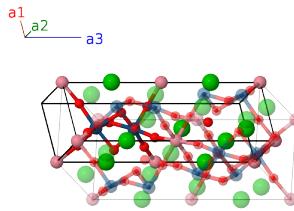
| | |
|--------------------------------|---|
| Prototype | $\text{Ba}_3\text{CoIr}_2\text{O}_9$ |
| AFLOW prototype label | A3BC2D9_mC60_15_ef_a_f_e4f-001 |
| ICSD | 35995 |
| Pearson symbol | mC60 |
| Space group number | 15 |
| Space group symbol | $C2/c$ |
| AFLOW prototype command | <pre>aflow --proto=A3BC2D9_mC60_15_ef_a_f_e4f-001 --params=a,b/a,c/a,\beta,y2,y3,x4,y4,z4,x5,y5,z5,x6,y6,z6,x7,y7,z7,x8,y8,z8,x9,y9, z9</pre> |

- $\text{Ba}_3\text{CoIr}_2\text{O}_9$ has been observed in three phases (Garg, 2020):
 - Above 107K it is in the hexagonal $\text{Ba}_3\text{CoIr}_2\text{O}_9$ structure, an ordered quaternary form of the hexagonal BaTiO_3 structure.
 - Below 107K it transforms into this monoclinic (I) $\text{Ba}_3\text{CoIr}_2\text{O}_9$ structure.
 - “On further reduction of temperature,” apparently at some point above 60K, the primitive cell doubles and the monoclinic (II) $\text{Ba}_3\text{CoIr}_2\text{O}_9$ structure appears. The monoclinic (I) and monoclinic (II) structures coexist down to absolute zero.

- Data for this structure was taken at 60K.

Base-centered Monoclinic primitive vectors

$$\begin{aligned}\mathbf{a}_1 &= \frac{1}{2}a\hat{\mathbf{x}} - \frac{1}{2}b\hat{\mathbf{y}} \\ \mathbf{a}_2 &= \frac{1}{2}a\hat{\mathbf{x}} + \frac{1}{2}b\hat{\mathbf{y}} \\ \mathbf{a}_3 &= c\cos\beta\hat{\mathbf{x}} + c\sin\beta\hat{\mathbf{z}}\end{aligned}$$



Basis vectors

| | Lattice coordinates | = | Cartesian coordinates | Wyckoff position | Atom type |
|-------------------|--|---|--|------------------|-----------|
| \mathbf{B}_1 | 0 | = | 0 | (4a) | Co I |
| \mathbf{B}_2 | $\frac{1}{2}\mathbf{a}_3$ | = | $\frac{1}{2}c\cos\beta\hat{\mathbf{x}} + \frac{1}{2}c\sin\beta\hat{\mathbf{z}}$ | (4a) | Co I |
| \mathbf{B}_3 | $-y_2\mathbf{a}_1 + y_2\mathbf{a}_2 + \frac{1}{4}\mathbf{a}_3$ | = | $\frac{1}{4}c\cos\beta\hat{\mathbf{x}} + by_2\hat{\mathbf{y}} + \frac{1}{4}c\sin\beta\hat{\mathbf{z}}$ | (4e) | Ba I |
| \mathbf{B}_4 | $y_2\mathbf{a}_1 - y_2\mathbf{a}_2 + \frac{3}{4}\mathbf{a}_3$ | = | $\frac{3}{4}c\cos\beta\hat{\mathbf{x}} - by_2\hat{\mathbf{y}} + \frac{3}{4}c\sin\beta\hat{\mathbf{z}}$ | (4e) | Ba I |
| \mathbf{B}_5 | $-y_3\mathbf{a}_1 + y_3\mathbf{a}_2 + \frac{1}{4}\mathbf{a}_3$ | = | $\frac{1}{4}c\cos\beta\hat{\mathbf{x}} + by_3\hat{\mathbf{y}} + \frac{1}{4}c\sin\beta\hat{\mathbf{z}}$ | (4e) | O I |
| \mathbf{B}_6 | $y_3\mathbf{a}_1 - y_3\mathbf{a}_2 + \frac{3}{4}\mathbf{a}_3$ | = | $\frac{3}{4}c\cos\beta\hat{\mathbf{x}} - by_3\hat{\mathbf{y}} + \frac{3}{4}c\sin\beta\hat{\mathbf{z}}$ | (4e) | O I |
| \mathbf{B}_7 | $(x_4 - y_4)\mathbf{a}_1 + (x_4 + y_4)\mathbf{a}_2 + z_4\mathbf{a}_3$ | = | $(ax_4 + cz_4\cos\beta)\hat{\mathbf{x}} + by_4\hat{\mathbf{y}} + cz_4\sin\beta\hat{\mathbf{z}}$ | (8f) | Ba II |
| \mathbf{B}_8 | $-(x_4 + y_4)\mathbf{a}_1 - (x_4 - y_4)\mathbf{a}_2 - (z_4 - \frac{1}{2})\mathbf{a}_3$ | = | $-(ax_4 + c(z_4 - \frac{1}{2})\cos\beta)\hat{\mathbf{x}} + by_4\hat{\mathbf{y}} - c(z_4 - \frac{1}{2})\sin\beta\hat{\mathbf{z}}$ | (8f) | Ba II |
| \mathbf{B}_9 | $-(x_4 - y_4)\mathbf{a}_1 - (x_4 + y_4)\mathbf{a}_2 - z_4\mathbf{a}_3$ | = | $-(ax_4 + cz_4\cos\beta)\hat{\mathbf{x}} - by_4\hat{\mathbf{y}} - cz_4\sin\beta\hat{\mathbf{z}}$ | (8f) | Ba II |
| \mathbf{B}_{10} | $(x_4 + y_4)\mathbf{a}_1 + (x_4 - y_4)\mathbf{a}_2 + (z_4 + \frac{1}{2})\mathbf{a}_3$ | = | $(ax_4 + c(z_4 + \frac{1}{2})\cos\beta)\hat{\mathbf{x}} - by_4\hat{\mathbf{y}} + c(z_4 + \frac{1}{2})\sin\beta\hat{\mathbf{z}}$ | (8f) | Ba II |
| \mathbf{B}_{11} | $(x_5 - y_5)\mathbf{a}_1 + (x_5 + y_5)\mathbf{a}_2 + z_5\mathbf{a}_3$ | = | $(ax_5 + cz_5\cos\beta)\hat{\mathbf{x}} + by_5\hat{\mathbf{y}} + cz_5\sin\beta\hat{\mathbf{z}}$ | (8f) | Ir I |
| \mathbf{B}_{12} | $-(x_5 + y_5)\mathbf{a}_1 - (x_5 - y_5)\mathbf{a}_2 - (z_5 - \frac{1}{2})\mathbf{a}_3$ | = | $-(ax_5 + c(z_5 - \frac{1}{2})\cos\beta)\hat{\mathbf{x}} + by_5\hat{\mathbf{y}} - c(z_5 - \frac{1}{2})\sin\beta\hat{\mathbf{z}}$ | (8f) | Ir I |
| \mathbf{B}_{13} | $-(x_5 - y_5)\mathbf{a}_1 - (x_5 + y_5)\mathbf{a}_2 - z_5\mathbf{a}_3$ | = | $-(ax_5 + cz_5\cos\beta)\hat{\mathbf{x}} - by_5\hat{\mathbf{y}} - cz_5\sin\beta\hat{\mathbf{z}}$ | (8f) | Ir I |
| \mathbf{B}_{14} | $(x_5 + y_5)\mathbf{a}_1 + (x_5 - y_5)\mathbf{a}_2 + (z_5 + \frac{1}{2})\mathbf{a}_3$ | = | $(ax_5 + c(z_5 + \frac{1}{2})\cos\beta)\hat{\mathbf{x}} - by_5\hat{\mathbf{y}} + c(z_5 + \frac{1}{2})\sin\beta\hat{\mathbf{z}}$ | (8f) | Ir I |
| \mathbf{B}_{15} | $(x_6 - y_6)\mathbf{a}_1 + (x_6 + y_6)\mathbf{a}_2 + z_6\mathbf{a}_3$ | = | $(ax_6 + cz_6\cos\beta)\hat{\mathbf{x}} + by_6\hat{\mathbf{y}} + cz_6\sin\beta\hat{\mathbf{z}}$ | (8f) | O II |
| \mathbf{B}_{16} | $-(x_6 + y_6)\mathbf{a}_1 - (x_6 - y_6)\mathbf{a}_2 - (z_6 - \frac{1}{2})\mathbf{a}_3$ | = | $-(ax_6 + c(z_6 - \frac{1}{2})\cos\beta)\hat{\mathbf{x}} + by_6\hat{\mathbf{y}} - c(z_6 - \frac{1}{2})\sin\beta\hat{\mathbf{z}}$ | (8f) | O II |
| \mathbf{B}_{17} | $-(x_6 - y_6)\mathbf{a}_1 - (x_6 + y_6)\mathbf{a}_2 - z_6\mathbf{a}_3$ | = | $-(ax_6 + cz_6\cos\beta)\hat{\mathbf{x}} - by_6\hat{\mathbf{y}} - cz_6\sin\beta\hat{\mathbf{z}}$ | (8f) | O II |
| \mathbf{B}_{18} | $(x_6 + y_6)\mathbf{a}_1 + (x_6 - y_6)\mathbf{a}_2 + (z_6 + \frac{1}{2})\mathbf{a}_3$ | = | $(ax_6 + c(z_6 + \frac{1}{2})\cos\beta)\hat{\mathbf{x}} - by_6\hat{\mathbf{y}} + c(z_6 + \frac{1}{2})\sin\beta\hat{\mathbf{z}}$ | (8f) | O II |
| \mathbf{B}_{19} | $(x_7 - y_7)\mathbf{a}_1 + (x_7 + y_7)\mathbf{a}_2 + z_7\mathbf{a}_3$ | = | $(ax_7 + cz_7\cos\beta)\hat{\mathbf{x}} + by_7\hat{\mathbf{y}} + cz_7\sin\beta\hat{\mathbf{z}}$ | (8f) | O III |

| | | | | | | |
|-------------------|-----|---|-----|---|------|-------|
| \mathbf{B}_{20} | $=$ | $-(x_7 + y_7) \mathbf{a}_1 - (x_7 - y_7) \mathbf{a}_2 - (z_7 - \frac{1}{2}) \mathbf{a}_3$ | $=$ | $-(ax_7 + c(z_7 - \frac{1}{2}) \cos \beta) \hat{\mathbf{x}} + by_7 \hat{\mathbf{y}} - c(z_7 - \frac{1}{2}) \sin \beta \hat{\mathbf{z}}$ | (8f) | O III |
| \mathbf{B}_{21} | $=$ | $-(x_7 - y_7) \mathbf{a}_1 - (x_7 + y_7) \mathbf{a}_2 - z_7 \mathbf{a}_3$ | $=$ | $-(ax_7 + cz_7 \cos \beta) \hat{\mathbf{x}} - by_7 \hat{\mathbf{y}} - cz_7 \sin \beta \hat{\mathbf{z}}$ | (8f) | O III |
| \mathbf{B}_{22} | $=$ | $(x_7 + y_7) \mathbf{a}_1 + (x_7 - y_7) \mathbf{a}_2 + (z_7 + \frac{1}{2}) \mathbf{a}_3$ | $=$ | $(ax_7 + c(z_7 + \frac{1}{2}) \cos \beta) \hat{\mathbf{x}} - by_7 \hat{\mathbf{y}} + c(z_7 + \frac{1}{2}) \sin \beta \hat{\mathbf{z}}$ | (8f) | O III |
| \mathbf{B}_{23} | $=$ | $(x_8 - y_8) \mathbf{a}_1 + (x_8 + y_8) \mathbf{a}_2 + z_8 \mathbf{a}_3$ | $=$ | $(ax_8 + cz_8 \cos \beta) \hat{\mathbf{x}} + by_8 \hat{\mathbf{y}} + cz_8 \sin \beta \hat{\mathbf{z}}$ | (8f) | O IV |
| \mathbf{B}_{24} | $=$ | $-(x_8 + y_8) \mathbf{a}_1 - (x_8 - y_8) \mathbf{a}_2 - (z_8 - \frac{1}{2}) \mathbf{a}_3$ | $=$ | $-(ax_8 + c(z_8 - \frac{1}{2}) \cos \beta) \hat{\mathbf{x}} + by_8 \hat{\mathbf{y}} - c(z_8 - \frac{1}{2}) \sin \beta \hat{\mathbf{z}}$ | (8f) | O IV |
| \mathbf{B}_{25} | $=$ | $-(x_8 - y_8) \mathbf{a}_1 - (x_8 + y_8) \mathbf{a}_2 - z_8 \mathbf{a}_3$ | $=$ | $-(ax_8 + cz_8 \cos \beta) \hat{\mathbf{x}} - by_8 \hat{\mathbf{y}} - cz_8 \sin \beta \hat{\mathbf{z}}$ | (8f) | O IV |
| \mathbf{B}_{26} | $=$ | $(x_8 + y_8) \mathbf{a}_1 + (x_8 - y_8) \mathbf{a}_2 + (z_8 + \frac{1}{2}) \mathbf{a}_3$ | $=$ | $(ax_8 + c(z_8 + \frac{1}{2}) \cos \beta) \hat{\mathbf{x}} - by_8 \hat{\mathbf{y}} + c(z_8 + \frac{1}{2}) \sin \beta \hat{\mathbf{z}}$ | (8f) | O IV |
| \mathbf{B}_{27} | $=$ | $(x_9 - y_9) \mathbf{a}_1 + (x_9 + y_9) \mathbf{a}_2 + z_9 \mathbf{a}_3$ | $=$ | $(ax_9 + cz_9 \cos \beta) \hat{\mathbf{x}} + by_9 \hat{\mathbf{y}} + cz_9 \sin \beta \hat{\mathbf{z}}$ | (8f) | O V |
| \mathbf{B}_{28} | $=$ | $-(x_9 + y_9) \mathbf{a}_1 - (x_9 - y_9) \mathbf{a}_2 - (z_9 - \frac{1}{2}) \mathbf{a}_3$ | $=$ | $-(ax_9 + c(z_9 - \frac{1}{2}) \cos \beta) \hat{\mathbf{x}} + by_9 \hat{\mathbf{y}} - c(z_9 - \frac{1}{2}) \sin \beta \hat{\mathbf{z}}$ | (8f) | O V |
| \mathbf{B}_{29} | $=$ | $-(x_9 - y_9) \mathbf{a}_1 - (x_9 + y_9) \mathbf{a}_2 - z_9 \mathbf{a}_3$ | $=$ | $-(ax_9 + cz_9 \cos \beta) \hat{\mathbf{x}} - by_9 \hat{\mathbf{y}} - cz_9 \sin \beta \hat{\mathbf{z}}$ | (8f) | O V |
| \mathbf{B}_{30} | $=$ | $(x_9 + y_9) \mathbf{a}_1 + (x_9 - y_9) \mathbf{a}_2 + (z_9 + \frac{1}{2}) \mathbf{a}_3$ | $=$ | $(ax_9 + c(z_9 + \frac{1}{2}) \cos \beta) \hat{\mathbf{x}} - by_9 \hat{\mathbf{y}} + c(z_9 + \frac{1}{2}) \sin \beta \hat{\mathbf{z}}$ | (8f) | O V |

References

- [1] C. Garg, D. Roy, M. Lonsky, P. Manuel, A. Cervellino, J. Müller, M. Kabir, and S. Nair, *Evolution of the structural, magnetic and electronic properties of the triple perovskite Ba₃CoIr₂O₉*, Phys. Rev. B **103**, 014437 (2021), doi:10.1103/PhysRevB.103.014437.