

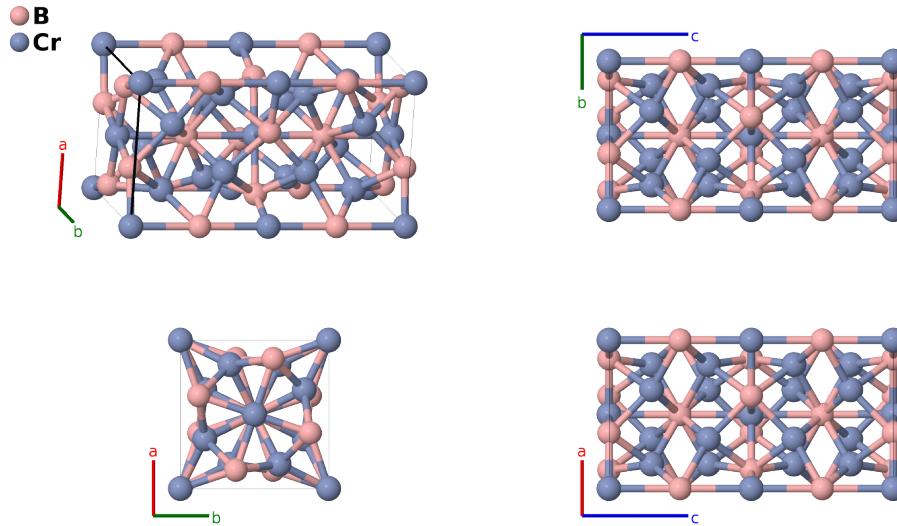
Cr_5B_3 ($D8_l$) Structure: A3B5_tI32_140_ah_cl-001

This structure originally had the label A3B5_tI32_140_ah_cl. Calls to that address will be redirected here.

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<https://aflow.org/p/AK18>

https://aflow.org/p/A3B5_tI32_140_ah_cl-001



Prototype	B_3Cr_5
AFLOW prototype label	A3B5_tI32_140_ah_cl-001
Strukturbericht designation	$D8_l$
ICSD	27124
Pearson symbol	tI32
Space group number	140
Space group symbol	$I4/mcm$
AFLOW prototype command	<code>aflow --proto=A3B5_tI32_140_ah_cl-001 --params=a, c/a, x₃, x₄, z₄</code>

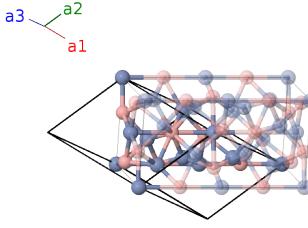
Other compounds with this structure

Eu_5Ge_3 , Pr_5Si_3 , Ta_5Ge_3 , Nb_5Si_3 , Ta_5Si_3 , EuIrGe_2 , Fe_5PB_2 , Fe_5SiB_2 , Fe_4CoPB_2 , Fe_4MnPB_2 , $\text{Fe}_4\text{CoSiB}_2$, $\text{Fe}_4\text{MnSiB}_2$, Mo_5SiB_2 , Sr_5In_3 , Gd_5CoSi_2 , Ca_5Si_3 , Sr_5Si_3

- We have been unable to obtain a copy of (Bertaut, 1953), so we use the data found online from (Downs, 2003). Although Cr_5B_3 is universally regarded as the prototype for $D8_l$, it appears that no other determination of the internal parameters has ever been made. The values found in (Downs, 2003) seem to be reasonable choices, and agree with the ICSD entry.

Body-centered Tetragonal primitive vectors

$$\begin{aligned}\mathbf{a}_1 &= -\frac{1}{2}a\hat{\mathbf{x}} + \frac{1}{2}a\hat{\mathbf{y}} + \frac{1}{2}c\hat{\mathbf{z}} \\ \mathbf{a}_2 &= \frac{1}{2}a\hat{\mathbf{x}} - \frac{1}{2}a\hat{\mathbf{y}} + \frac{1}{2}c\hat{\mathbf{z}} \\ \mathbf{a}_3 &= \frac{1}{2}a\hat{\mathbf{x}} + \frac{1}{2}a\hat{\mathbf{y}} - \frac{1}{2}c\hat{\mathbf{z}}\end{aligned}$$



Basis vectors

	Lattice coordinates	=	Cartesian coordinates	Wyckoff position	Atom type
\mathbf{B}_1	$\frac{1}{4}\mathbf{a}_1 + \frac{1}{4}\mathbf{a}_2$	=	$\frac{1}{4}c\hat{\mathbf{z}}$	(4a)	B I
\mathbf{B}_2	$\frac{3}{4}\mathbf{a}_1 + \frac{3}{4}\mathbf{a}_2$	=	$\frac{3}{4}c\hat{\mathbf{z}}$	(4a)	B I
\mathbf{B}_3	0	=	0	(4c)	Cr I
\mathbf{B}_4	$\frac{1}{2}\mathbf{a}_1 + \frac{1}{2}\mathbf{a}_2$	=	$\frac{1}{2}c\hat{\mathbf{z}}$	(4c)	Cr I
\mathbf{B}_5	$(x_3 + \frac{1}{2})\mathbf{a}_1 + x_3\mathbf{a}_2 + (2x_3 + \frac{1}{2})\mathbf{a}_3$	=	$ax_3\hat{\mathbf{x}} + a(x_3 + \frac{1}{2})\hat{\mathbf{y}}$	(8h)	B II
\mathbf{B}_6	$-(x_3 - \frac{1}{2})\mathbf{a}_1 - x_3\mathbf{a}_2 - (2x_3 - \frac{1}{2})\mathbf{a}_3$	=	$-ax_3\hat{\mathbf{x}} - a(x_3 - \frac{1}{2})\hat{\mathbf{y}}$	(8h)	B II
\mathbf{B}_7	$x_3\mathbf{a}_1 - (x_3 - \frac{1}{2})\mathbf{a}_2 + \frac{1}{2}\mathbf{a}_3$	=	$-a(x_3 - \frac{1}{2})\hat{\mathbf{x}} + ax_3\hat{\mathbf{y}}$	(8h)	B II
\mathbf{B}_8	$-x_3\mathbf{a}_1 + (x_3 + \frac{1}{2})\mathbf{a}_2 + \frac{1}{2}\mathbf{a}_3$	=	$a(x_3 + \frac{1}{2})\hat{\mathbf{x}} - ax_3\hat{\mathbf{y}}$	(8h)	B II
\mathbf{B}_9	$(x_4 + z_4 + \frac{1}{2})\mathbf{a}_1 + (x_4 + z_4)\mathbf{a}_2 + (2x_4 + \frac{1}{2})\mathbf{a}_3$	=	$ax_4\hat{\mathbf{x}} + a(x_4 + \frac{1}{2})\hat{\mathbf{y}} + cz_4\hat{\mathbf{z}}$	(16l)	Cr II
\mathbf{B}_{10}	$(-x_4 + z_4 + \frac{1}{2})\mathbf{a}_1 - (x_4 - z_4)\mathbf{a}_2 - (2x_4 - \frac{1}{2})\mathbf{a}_3$	=	$-ax_4\hat{\mathbf{x}} - a(x_4 - \frac{1}{2})\hat{\mathbf{y}} + cz_4\hat{\mathbf{z}}$	(16l)	Cr II
\mathbf{B}_{11}	$(x_4 + z_4)\mathbf{a}_1 + (-x_4 + z_4 + \frac{1}{2})\mathbf{a}_2 + \frac{1}{2}\mathbf{a}_3$	=	$-a(x_4 - \frac{1}{2})\hat{\mathbf{x}} + ax_4\hat{\mathbf{y}} + cz_4\hat{\mathbf{z}}$	(16l)	Cr II
\mathbf{B}_{12}	$-(x_4 - z_4)\mathbf{a}_1 + (x_4 + z_4 + \frac{1}{2})\mathbf{a}_2 + \frac{1}{2}\mathbf{a}_3$	=	$a(x_4 + \frac{1}{2})\hat{\mathbf{x}} - ax_4\hat{\mathbf{y}} + cz_4\hat{\mathbf{z}}$	(16l)	Cr II
\mathbf{B}_{13}	$(x_4 - z_4)\mathbf{a}_1 - (x_4 + z_4 - \frac{1}{2})\mathbf{a}_2 + \frac{1}{2}\mathbf{a}_3$	=	$-a(x_4 - \frac{1}{2})\hat{\mathbf{x}} + ax_4\hat{\mathbf{y}} - cz_4\hat{\mathbf{z}}$	(16l)	Cr II
\mathbf{B}_{14}	$-(x_4 + z_4)\mathbf{a}_1 + (x_4 - z_4 + \frac{1}{2})\mathbf{a}_2 + \frac{1}{2}\mathbf{a}_3$	=	$a(x_4 + \frac{1}{2})\hat{\mathbf{x}} - ax_4\hat{\mathbf{y}} - cz_4\hat{\mathbf{z}}$	(16l)	Cr II
\mathbf{B}_{15}	$(x_4 - z_4 + \frac{1}{2})\mathbf{a}_1 + (x_4 - z_4)\mathbf{a}_2 + (2x_4 + \frac{1}{2})\mathbf{a}_3$	=	$ax_4\hat{\mathbf{x}} + a(x_4 + \frac{1}{2})\hat{\mathbf{y}} - cz_4\hat{\mathbf{z}}$	(16l)	Cr II
\mathbf{B}_{16}	$-(x_4 + z_4 - \frac{1}{2})\mathbf{a}_1 - (x_4 + z_4)\mathbf{a}_2 - (2x_4 - \frac{1}{2})\mathbf{a}_3$	=	$-ax_4\hat{\mathbf{x}} - a(x_4 - \frac{1}{2})\hat{\mathbf{y}} - cz_4\hat{\mathbf{z}}$	(16l)	Cr II

References

- [1] F. Bertaut and P. Blum, *C. R. Acad. Sci.*, Comptes Rendus Hebdomadaires des Séances de l'Academie des Sciences **236**, 1055–1056 (1953).

Found in

- [1] R. T. Downs and M. Hall-Wallace, *The American Mineralogist Crystal Structure Database*, Am. Mineral. **88**, 247–250 (2003).