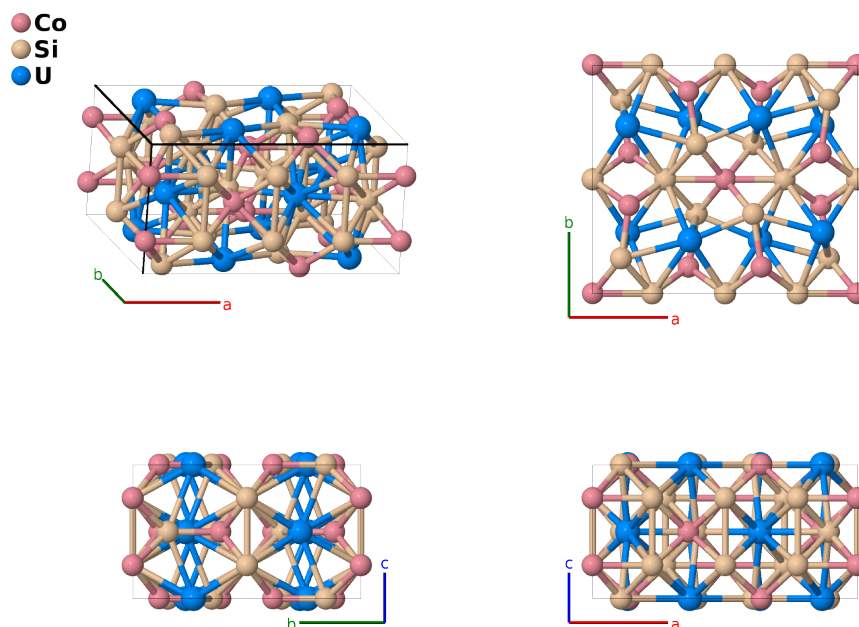


U₂Co₃Si₅ Structure: A3B5C2_oI40_72_aj_bfj_j-001

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<https://aflow.org/p/LD1K>

https://aflow.org/p/A3B5C2_oI40_72_aj_bfj_j-001

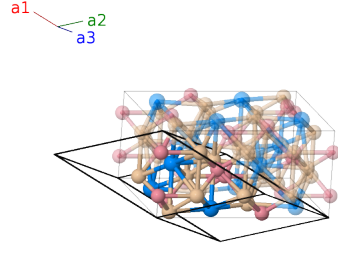


Prototype	Co ₃ Si ₅ U ₂
AFLOW prototype label	A3B5C2_oI40_72_aj_bfj_j-001
ICSD	20930
Pearson symbol	oI40
Space group number	72
Space group symbol	<i>Ibam</i>
AFLOW prototype command	<code>aflow --proto=A3B5C2_oI40_72_aj_bfj_j-001 --params=a, b/a, c/a, x₃, x₄, y₄, x₅, y₅, x₆, y₆</code>

Other compounds with this structure

Ce₂Co₃Si₅, Ce₂Pt₃Si₅, Ce₂Rh₃Ge₅, Ce₂Ru₃Ge₅, Dy₂Ni₃Si₅, Gd₂Ru₃Ge₅, Ho₂Ni₃Si₅, La₂Ru₃Ge₅, Li₂Ir₃Si₅, Lu₂Ir₃Si₅, Lu₂Ru₃Si₅, Nd₂Ru₃Ge₅, Pu₂Pt₃Si₅, Tb₂Ni₃Si₅, Tb₂Ru₃Ge₅, Y₂Ni₃Si₅

Body-centered Orthorhombic primitive vectors



$$\begin{aligned}\mathbf{a}_1 &= -\frac{1}{2}a \hat{\mathbf{x}} + \frac{1}{2}b \hat{\mathbf{y}} + \frac{1}{2}c \hat{\mathbf{z}} \\ \mathbf{a}_2 &= \frac{1}{2}a \hat{\mathbf{x}} - \frac{1}{2}b \hat{\mathbf{y}} + \frac{1}{2}c \hat{\mathbf{z}} \\ \mathbf{a}_3 &= \frac{1}{2}a \hat{\mathbf{x}} + \frac{1}{2}b \hat{\mathbf{y}} - \frac{1}{2}c \hat{\mathbf{z}}\end{aligned}$$

Basis vectors

	Lattice coordinates		Cartesian coordinates	Wyckoff position	Atom type
\mathbf{B}_1	$= \frac{1}{4} \mathbf{a}_1 + \frac{1}{4} \mathbf{a}_2$	$=$	$\frac{1}{4}c \hat{\mathbf{z}}$	(4a)	Co I
\mathbf{B}_2	$= \frac{3}{4} \mathbf{a}_1 + \frac{3}{4} \mathbf{a}_2$	$=$	$\frac{3}{4}c \hat{\mathbf{z}}$	(4a)	Co I
\mathbf{B}_3	$= \frac{1}{4} \mathbf{a}_1 + \frac{3}{4} \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	$=$	$\frac{1}{2}a \hat{\mathbf{x}} + \frac{1}{4}c \hat{\mathbf{z}}$	(4b)	Si I
\mathbf{B}_4	$= \frac{3}{4} \mathbf{a}_1 + \frac{1}{4} \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	$=$	$\frac{1}{2}b \hat{\mathbf{y}} + \frac{1}{4}c \hat{\mathbf{z}}$	(4b)	Si I
\mathbf{B}_5	$= \frac{1}{4} \mathbf{a}_1 + (x_3 + \frac{1}{4}) \mathbf{a}_2 + x_3 \mathbf{a}_3$	$=$	$ax_3 \hat{\mathbf{x}} + \frac{1}{4}c \hat{\mathbf{z}}$	(8f)	Si II
\mathbf{B}_6	$= \frac{1}{4} \mathbf{a}_1 - (x_3 - \frac{1}{4}) \mathbf{a}_2 - x_3 \mathbf{a}_3$	$=$	$-ax_3 \hat{\mathbf{x}} + \frac{1}{4}c \hat{\mathbf{z}}$	(8f)	Si II
\mathbf{B}_7	$= \frac{3}{4} \mathbf{a}_1 - (x_3 - \frac{3}{4}) \mathbf{a}_2 - x_3 \mathbf{a}_3$	$=$	$-ax_3 \hat{\mathbf{x}} + \frac{3}{4}c \hat{\mathbf{z}}$	(8f)	Si II
\mathbf{B}_8	$= \frac{3}{4} \mathbf{a}_1 + (x_3 + \frac{3}{4}) \mathbf{a}_2 + x_3 \mathbf{a}_3$	$=$	$ax_3 \hat{\mathbf{x}} + \frac{3}{4}c \hat{\mathbf{z}}$	(8f)	Si II
\mathbf{B}_9	$= y_4 \mathbf{a}_1 + x_4 \mathbf{a}_2 + (x_4 + y_4) \mathbf{a}_3$	$=$	$ax_4 \hat{\mathbf{x}} + by_4 \hat{\mathbf{y}}$	(8j)	Co II
\mathbf{B}_{10}	$= -y_4 \mathbf{a}_1 - x_4 \mathbf{a}_2 - (x_4 + y_4) \mathbf{a}_3$	$=$	$-ax_4 \hat{\mathbf{x}} - by_4 \hat{\mathbf{y}}$	(8j)	Co II
\mathbf{B}_{11}	$= (y_4 + \frac{1}{2}) \mathbf{a}_1 - (x_4 - \frac{1}{2}) \mathbf{a}_2 - (x_4 - y_4) \mathbf{a}_3$	$=$	$-ax_4 \hat{\mathbf{x}} + by_4 \hat{\mathbf{y}} + \frac{1}{2}c \hat{\mathbf{z}}$	(8j)	Co II
\mathbf{B}_{12}	$= -(y_4 - \frac{1}{2}) \mathbf{a}_1 + (x_4 + \frac{1}{2}) \mathbf{a}_2 + (x_4 - y_4) \mathbf{a}_3$	$=$	$ax_4 \hat{\mathbf{x}} - by_4 \hat{\mathbf{y}} + \frac{1}{2}c \hat{\mathbf{z}}$	(8j)	Co II
\mathbf{B}_{13}	$= y_5 \mathbf{a}_1 + x_5 \mathbf{a}_2 + (x_5 + y_5) \mathbf{a}_3$	$=$	$ax_5 \hat{\mathbf{x}} + by_5 \hat{\mathbf{y}}$	(8j)	Si III
\mathbf{B}_{14}	$= -y_5 \mathbf{a}_1 - x_5 \mathbf{a}_2 - (x_5 + y_5) \mathbf{a}_3$	$=$	$-ax_5 \hat{\mathbf{x}} - by_5 \hat{\mathbf{y}}$	(8j)	Si III
\mathbf{B}_{15}	$= (y_5 + \frac{1}{2}) \mathbf{a}_1 - (x_5 - \frac{1}{2}) \mathbf{a}_2 - (x_5 - y_5) \mathbf{a}_3$	$=$	$-ax_5 \hat{\mathbf{x}} + by_5 \hat{\mathbf{y}} + \frac{1}{2}c \hat{\mathbf{z}}$	(8j)	Si III
\mathbf{B}_{16}	$= -(y_5 - \frac{1}{2}) \mathbf{a}_1 + (x_5 + \frac{1}{2}) \mathbf{a}_2 + (x_5 - y_5) \mathbf{a}_3$	$=$	$ax_5 \hat{\mathbf{x}} - by_5 \hat{\mathbf{y}} + \frac{1}{2}c \hat{\mathbf{z}}$	(8j)	Si III
\mathbf{B}_{17}	$= y_6 \mathbf{a}_1 + x_6 \mathbf{a}_2 + (x_6 + y_6) \mathbf{a}_3$	$=$	$ax_6 \hat{\mathbf{x}} + by_6 \hat{\mathbf{y}}$	(8j)	U I
\mathbf{B}_{18}	$= -y_6 \mathbf{a}_1 - x_6 \mathbf{a}_2 - (x_6 + y_6) \mathbf{a}_3$	$=$	$-ax_6 \hat{\mathbf{x}} - by_6 \hat{\mathbf{y}}$	(8j)	U I
\mathbf{B}_{19}	$= (y_6 + \frac{1}{2}) \mathbf{a}_1 - (x_6 - \frac{1}{2}) \mathbf{a}_2 - (x_6 - y_6) \mathbf{a}_3$	$=$	$-ax_6 \hat{\mathbf{x}} + by_6 \hat{\mathbf{y}} + \frac{1}{2}c \hat{\mathbf{z}}$	(8j)	U I
\mathbf{B}_{20}	$= -(y_6 - \frac{1}{2}) \mathbf{a}_1 + (x_6 + \frac{1}{2}) \mathbf{a}_2 + (x_6 - y_6) \mathbf{a}_3$	$=$	$ax_6 \hat{\mathbf{x}} - by_6 \hat{\mathbf{y}} + \frac{1}{2}c \hat{\mathbf{z}}$	(8j)	U I

References

- [1] L. G. Aksel'rud, Y. P. Yarmolyuk, and E. I. Gladyshevskii, *Crystal structure of the compound $U_2Co_3Si_5$* , Sov. Phys. Crystallogr. **22**, 492–493 (1997).