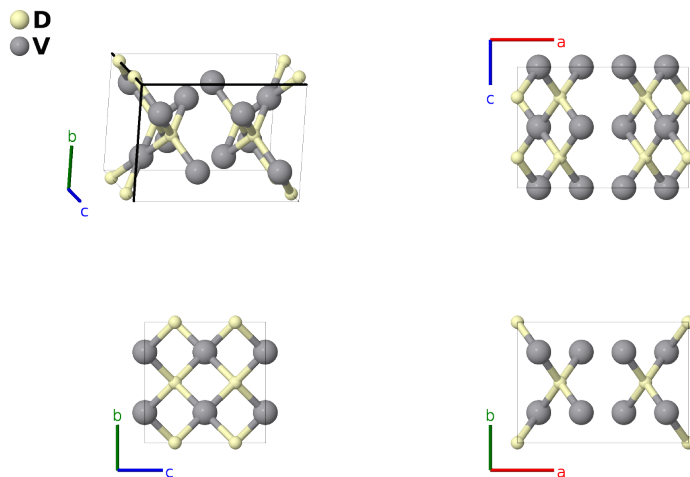


δ -V₄D₃ Structure: A3B4_oP14_49_ej_2q-001

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<https://afLOW.org/p/6B3F>

https://afLOW.org/p/A3B4_oP14_49_ej_2q-001

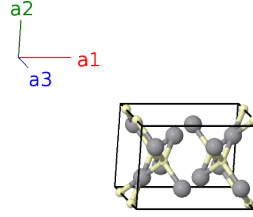


Prototype	H ₃ V ₄
AFLOW prototype label	A3B4_oP14_49_ej_2q-001
ICSD	42434
Pearson symbol	oP14
Space group number	49
Space group symbol	<i>Pccm</i>
AFLOW prototype command	<code>afLOW --proto=A3B4_oP14_49_ej_2q-001 --params=a, b/a, c/a, x₂, x₃, y₃, x₄, y₄</code>

- δ -V₄D₃ is the only completely ordered structure in the Vanadium-Hydrogen/Deuterium system (Asano, 1973). Even then, the deuterium sites are only 98% occupied.
- The data for this structure was obtained at 88K.
- While (Asano, 1973) placed this in space group *Pcc2* #27, (Cenzual, 1991) showed that the published coordinates placed the system in space group *Pccm* #49.

Simple Orthorhombic primitive vectors

$$\begin{aligned}\mathbf{a}_1 &= a \hat{\mathbf{x}} \\ \mathbf{a}_2 &= b \hat{\mathbf{y}} \\ \mathbf{a}_3 &= c \hat{\mathbf{z}}\end{aligned}$$



Basis vectors

	Lattice coordinates		Cartesian coordinates	Wyckoff position	Atom type
\mathbf{B}_1	$= \frac{1}{4} \mathbf{a}_3$	$=$	$\frac{1}{4} c \hat{\mathbf{z}}$	(2e)	D I
\mathbf{B}_2	$= \frac{3}{4} \mathbf{a}_3$	$=$	$\frac{3}{4} c \hat{\mathbf{z}}$	(2e)	D I
\mathbf{B}_3	$= x_2 \mathbf{a}_1 + \frac{1}{2} \mathbf{a}_2 + \frac{1}{4} \mathbf{a}_3$	$=$	$ax_2 \hat{\mathbf{x}} + \frac{1}{2} b \hat{\mathbf{y}} + \frac{1}{4} c \hat{\mathbf{z}}$	(4j)	D II
\mathbf{B}_4	$= -x_2 \mathbf{a}_1 + \frac{1}{2} \mathbf{a}_2 + \frac{1}{4} \mathbf{a}_3$	$=$	$-ax_2 \hat{\mathbf{x}} + \frac{1}{2} b \hat{\mathbf{y}} + \frac{1}{4} c \hat{\mathbf{z}}$	(4j)	D II
\mathbf{B}_5	$= -x_2 \mathbf{a}_1 + \frac{1}{2} \mathbf{a}_2 + \frac{3}{4} \mathbf{a}_3$	$=$	$-ax_2 \hat{\mathbf{x}} + \frac{1}{2} b \hat{\mathbf{y}} + \frac{3}{4} c \hat{\mathbf{z}}$	(4j)	D II
\mathbf{B}_6	$= x_2 \mathbf{a}_1 + \frac{1}{2} \mathbf{a}_2 + \frac{3}{4} \mathbf{a}_3$	$=$	$ax_2 \hat{\mathbf{x}} + \frac{1}{2} b \hat{\mathbf{y}} + \frac{3}{4} c \hat{\mathbf{z}}$	(4j)	D II
\mathbf{B}_7	$= x_3 \mathbf{a}_1 + y_3 \mathbf{a}_2$	$=$	$ax_3 \hat{\mathbf{x}} + by_3 \hat{\mathbf{y}}$	(4q)	V I
\mathbf{B}_8	$= -x_3 \mathbf{a}_1 - y_3 \mathbf{a}_2$	$=$	$-ax_3 \hat{\mathbf{x}} - by_3 \hat{\mathbf{y}}$	(4q)	V I
\mathbf{B}_9	$= -x_3 \mathbf{a}_1 + y_3 \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	$=$	$-ax_3 \hat{\mathbf{x}} + by_3 \hat{\mathbf{y}} + \frac{1}{2} c \hat{\mathbf{z}}$	(4q)	V I
\mathbf{B}_{10}	$= x_3 \mathbf{a}_1 - y_3 \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	$=$	$ax_3 \hat{\mathbf{x}} - by_3 \hat{\mathbf{y}} + \frac{1}{2} c \hat{\mathbf{z}}$	(4q)	V I
\mathbf{B}_{11}	$= x_4 \mathbf{a}_1 + y_4 \mathbf{a}_2$	$=$	$ax_4 \hat{\mathbf{x}} + by_4 \hat{\mathbf{y}}$	(4q)	V II
\mathbf{B}_{12}	$= -x_4 \mathbf{a}_1 - y_4 \mathbf{a}_2$	$=$	$-ax_4 \hat{\mathbf{x}} - by_4 \hat{\mathbf{y}}$	(4q)	V II
\mathbf{B}_{13}	$= -x_4 \mathbf{a}_1 + y_4 \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	$=$	$-ax_4 \hat{\mathbf{x}} + by_4 \hat{\mathbf{y}} + \frac{1}{2} c \hat{\mathbf{z}}$	(4q)	V II
\mathbf{B}_{14}	$= x_4 \mathbf{a}_1 - y_4 \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	$=$	$ax_4 \hat{\mathbf{x}} - by_4 \hat{\mathbf{y}} + \frac{1}{2} c \hat{\mathbf{z}}$	(4q)	V II

References

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