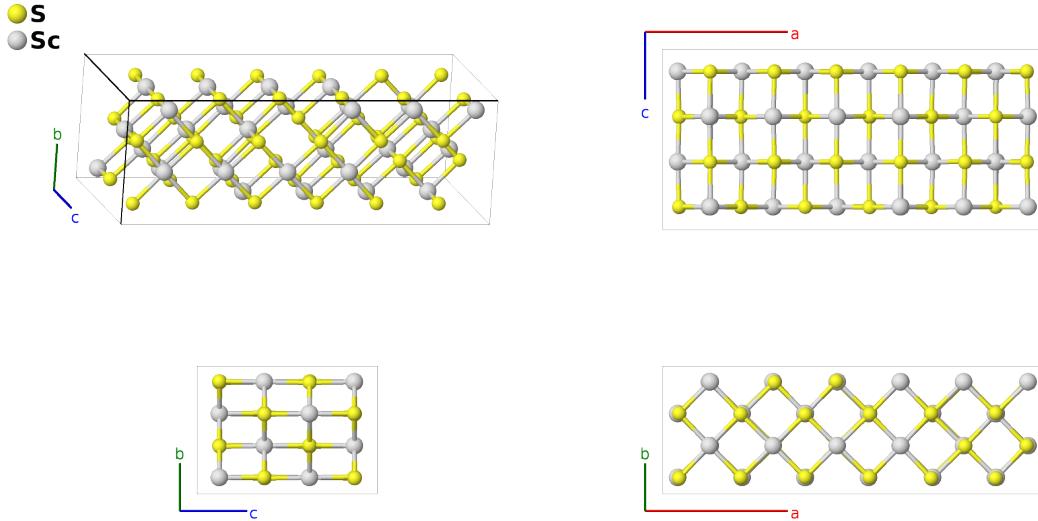


Sc₂S₃ Structure: A3B2_oF80_70_fh_2e-001

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<https://aflow.org/p/HQ18>

https://aflow.org/p/A3B2_oF80_70_fh_2e-001



Prototype	S ₃ Sc ₂
AFLOW prototype label	A3B2_oF80_70_fh_2e-001
ICSD	22236
Pearson symbol	oF80
Space group number	70
Space group symbol	Fddd
AFLOW prototype command	aflow --proto=A3B2_oF80_70_fh_2e-001 --params=a, b/a, c/a, x ₁ , x ₂ , y ₃ , x ₄ , y ₄ , z ₄

Other compounds with this structure

Dy₂Se₃, Dy₂Te₃, Eu₂Se₃, Eu₂Te₃, Lu₂Se₃, Sc₂Se₃, Y₂Se₃, Y₂Te₃, Yb₂Se₃

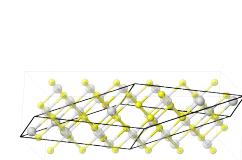
- This structure has been rotated from the orientation given by (Dismukes, 1964).

Face-centered Orthorhombic primitive vectors

$$\mathbf{a}_1 = \frac{1}{2}b\hat{\mathbf{y}} + \frac{1}{2}c\hat{\mathbf{z}}$$

$$\mathbf{a}_2 = \frac{1}{2}a\hat{\mathbf{x}} + \frac{1}{2}c\hat{\mathbf{z}}$$

$$\mathbf{a}_3 = \frac{1}{2}a\hat{\mathbf{x}} + \frac{1}{2}b\hat{\mathbf{y}}$$



Basis vectors

	Lattice coordinates	Cartesian coordinates	Wyckoff position	Atom type
\mathbf{B}_1	$= -\left(x_1 - \frac{1}{4}\right) \mathbf{a}_1 + x_1 \mathbf{a}_2 + x_1 \mathbf{a}_3$	$= ax_1 \hat{\mathbf{x}} + \frac{1}{8}b \hat{\mathbf{y}} + \frac{1}{8}c \hat{\mathbf{z}}$	(16e)	Sc I
\mathbf{B}_2	$= x_1 \mathbf{a}_1 - \left(x_1 - \frac{1}{4}\right) \mathbf{a}_2 - \left(x_1 - \frac{1}{4}\right) \mathbf{a}_3$	$= -a \left(x_1 - \frac{1}{4}\right) \hat{\mathbf{x}} + \frac{1}{8}b \hat{\mathbf{y}} + \frac{1}{8}c \hat{\mathbf{z}}$	(16e)	Sc I
\mathbf{B}_3	$= \left(x_1 + \frac{3}{4}\right) \mathbf{a}_1 - x_1 \mathbf{a}_2 - x_1 \mathbf{a}_3$	$= -ax_1 \hat{\mathbf{x}} + \frac{3}{8}b \hat{\mathbf{y}} + \frac{3}{8}c \hat{\mathbf{z}}$	(16e)	Sc I
\mathbf{B}_4	$= -x_1 \mathbf{a}_1 + \left(x_1 + \frac{3}{4}\right) \mathbf{a}_2 + \left(x_1 + \frac{3}{4}\right) \mathbf{a}_3$	$= a \left(x_1 + \frac{3}{4}\right) \hat{\mathbf{x}} + \frac{3}{8}b \hat{\mathbf{y}} + \frac{3}{8}c \hat{\mathbf{z}}$	(16e)	Sc I
\mathbf{B}_5	$= -\left(x_2 - \frac{1}{4}\right) \mathbf{a}_1 + x_2 \mathbf{a}_2 + x_2 \mathbf{a}_3$	$= ax_2 \hat{\mathbf{x}} + \frac{1}{8}b \hat{\mathbf{y}} + \frac{1}{8}c \hat{\mathbf{z}}$	(16e)	Sc II
\mathbf{B}_6	$= x_2 \mathbf{a}_1 - \left(x_2 - \frac{1}{4}\right) \mathbf{a}_2 - \left(x_2 - \frac{1}{4}\right) \mathbf{a}_3$	$= -a \left(x_2 - \frac{1}{4}\right) \hat{\mathbf{x}} + \frac{1}{8}b \hat{\mathbf{y}} + \frac{1}{8}c \hat{\mathbf{z}}$	(16e)	Sc II
\mathbf{B}_7	$= \left(x_2 + \frac{3}{4}\right) \mathbf{a}_1 - x_2 \mathbf{a}_2 - x_2 \mathbf{a}_3$	$= -ax_2 \hat{\mathbf{x}} + \frac{3}{8}b \hat{\mathbf{y}} + \frac{3}{8}c \hat{\mathbf{z}}$	(16e)	Sc II
\mathbf{B}_8	$= -x_2 \mathbf{a}_1 + \left(x_2 + \frac{3}{4}\right) \mathbf{a}_2 + \left(x_2 + \frac{3}{4}\right) \mathbf{a}_3$	$= a \left(x_2 + \frac{3}{4}\right) \hat{\mathbf{x}} + \frac{3}{8}b \hat{\mathbf{y}} + \frac{3}{8}c \hat{\mathbf{z}}$	(16e)	Sc II
\mathbf{B}_9	$= y_3 \mathbf{a}_1 - \left(y_3 - \frac{1}{4}\right) \mathbf{a}_2 + y_3 \mathbf{a}_3$	$= \frac{1}{8}a \hat{\mathbf{x}} + by_3 \hat{\mathbf{y}} + \frac{1}{8}c \hat{\mathbf{z}}$	(16f)	S I
\mathbf{B}_{10}	$= -\left(y_3 - \frac{1}{4}\right) \mathbf{a}_1 + y_3 \mathbf{a}_2 - \left(y_3 - \frac{1}{4}\right) \mathbf{a}_3$	$= \frac{1}{8}a \hat{\mathbf{x}} - b \left(y_3 - \frac{1}{4}\right) \hat{\mathbf{y}} + \frac{1}{8}c \hat{\mathbf{z}}$	(16f)	S I
\mathbf{B}_{11}	$= -y_3 \mathbf{a}_1 + \left(y_3 + \frac{3}{4}\right) \mathbf{a}_2 - y_3 \mathbf{a}_3$	$= \frac{3}{8}a \hat{\mathbf{x}} - by_3 \hat{\mathbf{y}} + \frac{3}{8}c \hat{\mathbf{z}}$	(16f)	S I
\mathbf{B}_{12}	$= \left(y_3 + \frac{3}{4}\right) \mathbf{a}_1 - y_3 \mathbf{a}_2 + \left(y_3 + \frac{3}{4}\right) \mathbf{a}_3$	$= \frac{3}{8}a \hat{\mathbf{x}} + b \left(y_3 + \frac{3}{4}\right) \hat{\mathbf{y}} + \frac{3}{8}c \hat{\mathbf{z}}$	(16f)	S I
\mathbf{B}_{13}	$= (-x_4 + y_4 + z_4) \mathbf{a}_1 + (x_4 - y_4 + z_4) \mathbf{a}_2 + (x_4 + y_4 - z_4) \mathbf{a}_3$	$= ax_4 \hat{\mathbf{x}} + by_4 \hat{\mathbf{y}} + cz_4 \hat{\mathbf{z}}$	(32h)	S II
\mathbf{B}_{14}	$= (x_4 - y_4 + z_4) \mathbf{a}_1 + (-x_4 + y_4 + z_4) \mathbf{a}_2 - (x_4 + y_4 + z_4 - \frac{1}{2}) \mathbf{a}_3$	$= -a \left(x_4 - \frac{1}{4}\right) \hat{\mathbf{x}} - b \left(y_4 - \frac{1}{4}\right) \hat{\mathbf{y}} + cz_4 \hat{\mathbf{z}}$	(32h)	S II
\mathbf{B}_{15}	$= (x_4 + y_4 - z_4) \mathbf{a}_1 - (x_4 + y_4 + z_4 - \frac{1}{2}) \mathbf{a}_2 + (-x_4 + y_4 + z_4) \mathbf{a}_3$	$= -a \left(x_4 - \frac{1}{4}\right) \hat{\mathbf{x}} + by_4 \hat{\mathbf{y}} - c \left(z_4 - \frac{1}{4}\right) \hat{\mathbf{z}}$	(32h)	S II
\mathbf{B}_{16}	$= -(x_4 + y_4 + z_4 - \frac{1}{2}) \mathbf{a}_1 + (x_4 + y_4 - z_4) \mathbf{a}_2 + (x_4 - y_4 + z_4) \mathbf{a}_3$	$= ax_4 \hat{\mathbf{x}} - b \left(y_4 - \frac{1}{4}\right) \hat{\mathbf{y}} - c \left(z_4 - \frac{1}{4}\right) \hat{\mathbf{z}}$	(32h)	S II
\mathbf{B}_{17}	$= (x_4 - y_4 - z_4) \mathbf{a}_1 - (x_4 - y_4 + z_4) \mathbf{a}_2 - (x_4 + y_4 - z_4) \mathbf{a}_3$	$= -ax_4 \hat{\mathbf{x}} - by_4 \hat{\mathbf{y}} - cz_4 \hat{\mathbf{z}}$	(32h)	S II
\mathbf{B}_{18}	$= -(x_4 - y_4 + z_4) \mathbf{a}_1 + (x_4 - y_4 - z_4) \mathbf{a}_2 + (x_4 + y_4 + z_4 + \frac{1}{2}) \mathbf{a}_3$	$= a \left(x_4 + \frac{1}{4}\right) \hat{\mathbf{x}} + b \left(y_4 + \frac{1}{4}\right) \hat{\mathbf{y}} - cz_4 \hat{\mathbf{z}}$	(32h)	S II
\mathbf{B}_{19}	$= -(x_4 + y_4 - z_4) \mathbf{a}_1 + (x_4 + y_4 + z_4 + \frac{1}{2}) \mathbf{a}_2 + (x_4 - y_4 - z_4) \mathbf{a}_3$	$= a \left(x_4 + \frac{1}{4}\right) \hat{\mathbf{x}} - by_4 \hat{\mathbf{y}} + c \left(z_4 + \frac{1}{4}\right) \hat{\mathbf{z}}$	(32h)	S II
\mathbf{B}_{20}	$= (x_4 + y_4 + z_4 + \frac{1}{2}) \mathbf{a}_1 - (x_4 + y_4 - z_4) \mathbf{a}_2 - (x_4 - y_4 + z_4) \mathbf{a}_3$	$= -ax_4 \hat{\mathbf{x}} + b \left(y_4 + \frac{1}{4}\right) \hat{\mathbf{y}} + c \left(z_4 + \frac{1}{4}\right) \hat{\mathbf{z}}$	(32h)	S II

References

- [1] J. P. Dismukes and J. G. White, *The Preparation, Properties, and Crystal Structures of Some Scandium Sulfides in the Range Sc_2S_3 - ScS* , Inorg. Chem. **3**, 1220–1228 (1964), doi:10.1021/ic50019a004.