

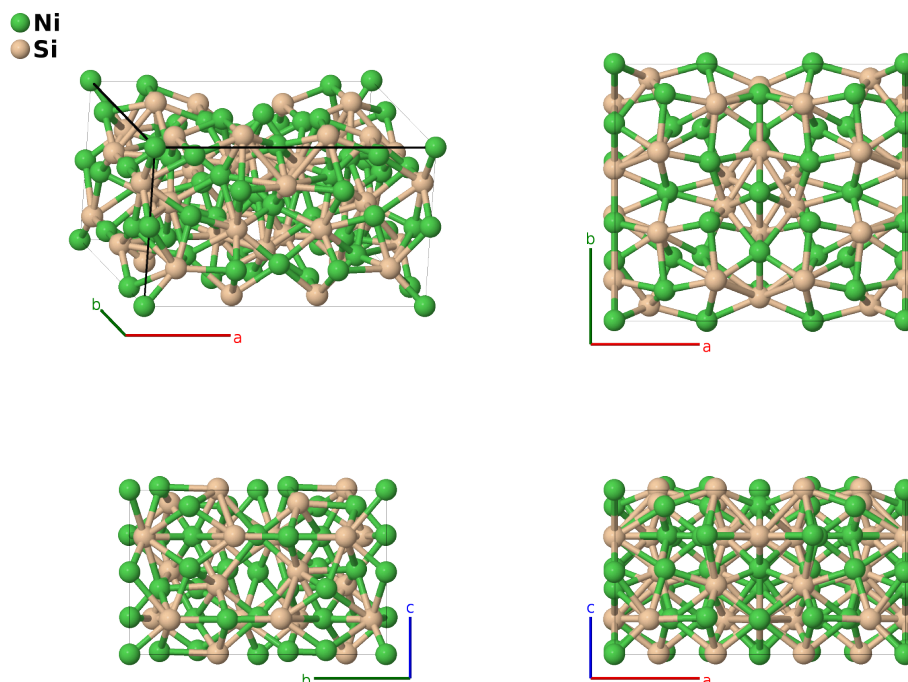
Ni₃Si₂ Structure: A3B2_oC80_36_4a4b_2a3b-001

This structure originally had the label A3B2_oC80_36_4a4b_2a3b. Calls to that address will be redirected here.

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<https://aflow.org/p/5H38>

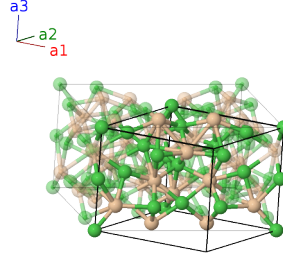
https://aflow.org/p/A3B2_oC80_36_4a4b_2a3b-001



Prototype	Ni ₃ Si ₂
AFLOW prototype label	A3B2_oC80_36_4a4b_2a3b-001
ICSD	43561
Pearson symbol	oC80
Space group number	36
Space group symbol	<i>Cmc</i> 2 ₁
AFLOW prototype command	<pre>aflow --proto=A3B2_oC80_36_4a4b_2a3b-001 --params=a, b/a, c/a, y1, z1, y2, z2, y3, z3, y4, z4, y5, z5, y6, z6, x7, y7, z7, x8, y8, z8, x9, y9, z9, x10, y10, z10, x11, y11, z11, x12, y12, z12, x13, y13, z13</pre>

Base-centered Orthorhombic primitive vectors

$$\begin{aligned}
\mathbf{a}_1 &= \frac{1}{2}a \hat{\mathbf{x}} - \frac{1}{2}b \hat{\mathbf{y}} \\
\mathbf{a}_2 &= \frac{1}{2}a \hat{\mathbf{x}} + \frac{1}{2}b \hat{\mathbf{y}} \\
\mathbf{a}_3 &= c \hat{\mathbf{z}}
\end{aligned}$$



Basis vectors

	Lattice coordinates		Cartesian coordinates	Wyckoff position	Atom type
\mathbf{B}_1	$= -y_1 \mathbf{a}_1 + y_1 \mathbf{a}_2 + z_1 \mathbf{a}_3$	$=$	$by_1 \hat{\mathbf{y}} + cz_1 \hat{\mathbf{z}}$	(4a)	Ni I
\mathbf{B}_2	$= y_1 \mathbf{a}_1 - y_1 \mathbf{a}_2 + (z_1 + \frac{1}{2}) \mathbf{a}_3$	$=$	$-by_1 \hat{\mathbf{y}} + c(z_1 + \frac{1}{2}) \hat{\mathbf{z}}$	(4a)	Ni I
\mathbf{B}_3	$= -y_2 \mathbf{a}_1 + y_2 \mathbf{a}_2 + z_2 \mathbf{a}_3$	$=$	$by_2 \hat{\mathbf{y}} + cz_2 \hat{\mathbf{z}}$	(4a)	Ni II
\mathbf{B}_4	$= y_2 \mathbf{a}_1 - y_2 \mathbf{a}_2 + (z_2 + \frac{1}{2}) \mathbf{a}_3$	$=$	$-by_2 \hat{\mathbf{y}} + c(z_2 + \frac{1}{2}) \hat{\mathbf{z}}$	(4a)	Ni II
\mathbf{B}_5	$= -y_3 \mathbf{a}_1 + y_3 \mathbf{a}_2 + z_3 \mathbf{a}_3$	$=$	$by_3 \hat{\mathbf{y}} + cz_3 \hat{\mathbf{z}}$	(4a)	Ni III
\mathbf{B}_6	$= y_3 \mathbf{a}_1 - y_3 \mathbf{a}_2 + (z_3 + \frac{1}{2}) \mathbf{a}_3$	$=$	$-by_3 \hat{\mathbf{y}} + c(z_3 + \frac{1}{2}) \hat{\mathbf{z}}$	(4a)	Ni III
\mathbf{B}_7	$= -y_4 \mathbf{a}_1 + y_4 \mathbf{a}_2 + z_4 \mathbf{a}_3$	$=$	$by_4 \hat{\mathbf{y}} + cz_4 \hat{\mathbf{z}}$	(4a)	Ni IV
\mathbf{B}_8	$= y_4 \mathbf{a}_1 - y_4 \mathbf{a}_2 + (z_4 + \frac{1}{2}) \mathbf{a}_3$	$=$	$-by_4 \hat{\mathbf{y}} + c(z_4 + \frac{1}{2}) \hat{\mathbf{z}}$	(4a)	Ni IV
\mathbf{B}_9	$= -y_5 \mathbf{a}_1 + y_5 \mathbf{a}_2 + z_5 \mathbf{a}_3$	$=$	$by_5 \hat{\mathbf{y}} + cz_5 \hat{\mathbf{z}}$	(4a)	Si I
\mathbf{B}_{10}	$= y_5 \mathbf{a}_1 - y_5 \mathbf{a}_2 + (z_5 + \frac{1}{2}) \mathbf{a}_3$	$=$	$-by_5 \hat{\mathbf{y}} + c(z_5 + \frac{1}{2}) \hat{\mathbf{z}}$	(4a)	Si I
\mathbf{B}_{11}	$= -y_6 \mathbf{a}_1 + y_6 \mathbf{a}_2 + z_6 \mathbf{a}_3$	$=$	$by_6 \hat{\mathbf{y}} + cz_6 \hat{\mathbf{z}}$	(4a)	Si II
\mathbf{B}_{12}	$= y_6 \mathbf{a}_1 - y_6 \mathbf{a}_2 + (z_6 + \frac{1}{2}) \mathbf{a}_3$	$=$	$-by_6 \hat{\mathbf{y}} + c(z_6 + \frac{1}{2}) \hat{\mathbf{z}}$	(4a)	Si II
\mathbf{B}_{13}	$= (x_7 - y_7) \mathbf{a}_1 + (x_7 + y_7) \mathbf{a}_2 + z_7 \mathbf{a}_3$	$=$	$ax_7 \hat{\mathbf{x}} + by_7 \hat{\mathbf{y}} + cz_7 \hat{\mathbf{z}}$	(8b)	Ni V
\mathbf{B}_{14}	$= -(x_7 - y_7) \mathbf{a}_1 - (x_7 + y_7) \mathbf{a}_2 + (z_7 + \frac{1}{2}) \mathbf{a}_3$	$=$	$-ax_7 \hat{\mathbf{x}} - by_7 \hat{\mathbf{y}} + c(z_7 + \frac{1}{2}) \hat{\mathbf{z}}$	(8b)	Ni V
\mathbf{B}_{15}	$= (x_7 + y_7) \mathbf{a}_1 + (x_7 - y_7) \mathbf{a}_2 + (z_7 + \frac{1}{2}) \mathbf{a}_3$	$=$	$ax_7 \hat{\mathbf{x}} - by_7 \hat{\mathbf{y}} + c(z_7 + \frac{1}{2}) \hat{\mathbf{z}}$	(8b)	Ni V
\mathbf{B}_{16}	$= -(x_7 + y_7) \mathbf{a}_1 - (x_7 - y_7) \mathbf{a}_2 + z_7 \mathbf{a}_3$	$=$	$-ax_7 \hat{\mathbf{x}} + by_7 \hat{\mathbf{y}} + cz_7 \hat{\mathbf{z}}$	(8b)	Ni V
\mathbf{B}_{17}	$= (x_8 - y_8) \mathbf{a}_1 + (x_8 + y_8) \mathbf{a}_2 + z_8 \mathbf{a}_3$	$=$	$ax_8 \hat{\mathbf{x}} + by_8 \hat{\mathbf{y}} + cz_8 \hat{\mathbf{z}}$	(8b)	Ni VI
\mathbf{B}_{18}	$= -(x_8 - y_8) \mathbf{a}_1 - (x_8 + y_8) \mathbf{a}_2 + (z_8 + \frac{1}{2}) \mathbf{a}_3$	$=$	$-ax_8 \hat{\mathbf{x}} - by_8 \hat{\mathbf{y}} + c(z_8 + \frac{1}{2}) \hat{\mathbf{z}}$	(8b)	Ni VI
\mathbf{B}_{19}	$= (x_8 + y_8) \mathbf{a}_1 + (x_8 - y_8) \mathbf{a}_2 + (z_8 + \frac{1}{2}) \mathbf{a}_3$	$=$	$ax_8 \hat{\mathbf{x}} - by_8 \hat{\mathbf{y}} + c(z_8 + \frac{1}{2}) \hat{\mathbf{z}}$	(8b)	Ni VI
\mathbf{B}_{20}	$= -(x_8 + y_8) \mathbf{a}_1 - (x_8 - y_8) \mathbf{a}_2 + z_8 \mathbf{a}_3$	$=$	$-ax_8 \hat{\mathbf{x}} + by_8 \hat{\mathbf{y}} + cz_8 \hat{\mathbf{z}}$	(8b)	Ni VI
\mathbf{B}_{21}	$= (x_9 - y_9) \mathbf{a}_1 + (x_9 + y_9) \mathbf{a}_2 + z_9 \mathbf{a}_3$	$=$	$ax_9 \hat{\mathbf{x}} + by_9 \hat{\mathbf{y}} + cz_9 \hat{\mathbf{z}}$	(8b)	Ni VII
\mathbf{B}_{22}	$= -(x_9 - y_9) \mathbf{a}_1 - (x_9 + y_9) \mathbf{a}_2 + (z_9 + \frac{1}{2}) \mathbf{a}_3$	$=$	$-ax_9 \hat{\mathbf{x}} - by_9 \hat{\mathbf{y}} + c(z_9 + \frac{1}{2}) \hat{\mathbf{z}}$	(8b)	Ni VII

$$\begin{aligned}
\mathbf{B}_{23} &= \begin{pmatrix} (x_9 + y_9) \mathbf{a}_1 + (x_9 - y_9) \mathbf{a}_2 + \\ (z_9 + \frac{1}{2}) \mathbf{a}_3 \end{pmatrix} = ax_9 \hat{\mathbf{x}} - by_9 \hat{\mathbf{y}} + c(z_9 + \frac{1}{2}) \hat{\mathbf{z}} & (8b) & \text{Ni VII} \\
\mathbf{B}_{24} &= \begin{pmatrix} -(x_9 + y_9) \mathbf{a}_1 - (x_9 - y_9) \mathbf{a}_2 + \\ z_9 \mathbf{a}_3 \end{pmatrix} = -ax_9 \hat{\mathbf{x}} + by_9 \hat{\mathbf{y}} + cz_9 \hat{\mathbf{z}} & (8b) & \text{Ni VII} \\
\mathbf{B}_{25} &= \begin{pmatrix} (x_{10} - y_{10}) \mathbf{a}_1 + \\ (x_{10} + y_{10}) \mathbf{a}_2 + z_{10} \mathbf{a}_3 \end{pmatrix} = ax_{10} \hat{\mathbf{x}} + by_{10} \hat{\mathbf{y}} + cz_{10} \hat{\mathbf{z}} & (8b) & \text{Ni VIII} \\
\mathbf{B}_{26} &= \begin{pmatrix} -(x_{10} - y_{10}) \mathbf{a}_1 - \\ (x_{10} + y_{10}) \mathbf{a}_2 + (z_{10} + \frac{1}{2}) \mathbf{a}_3 \end{pmatrix} = -ax_{10} \hat{\mathbf{x}} - by_{10} \hat{\mathbf{y}} + c(z_{10} + \frac{1}{2}) \hat{\mathbf{z}} & (8b) & \text{Ni VIII} \\
\mathbf{B}_{27} &= \begin{pmatrix} (x_{10} + y_{10}) \mathbf{a}_1 + \\ (x_{10} - y_{10}) \mathbf{a}_2 + (z_{10} + \frac{1}{2}) \mathbf{a}_3 \end{pmatrix} = ax_{10} \hat{\mathbf{x}} - by_{10} \hat{\mathbf{y}} + c(z_{10} + \frac{1}{2}) \hat{\mathbf{z}} & (8b) & \text{Ni VIII} \\
\mathbf{B}_{28} &= \begin{pmatrix} -(x_{10} + y_{10}) \mathbf{a}_1 - \\ (x_{10} - y_{10}) \mathbf{a}_2 + z_{10} \mathbf{a}_3 \end{pmatrix} = -ax_{10} \hat{\mathbf{x}} + by_{10} \hat{\mathbf{y}} + cz_{10} \hat{\mathbf{z}} & (8b) & \text{Ni VIII} \\
\mathbf{B}_{29} &= \begin{pmatrix} (x_{11} - y_{11}) \mathbf{a}_1 + \\ (x_{11} + y_{11}) \mathbf{a}_2 + z_{11} \mathbf{a}_3 \end{pmatrix} = ax_{11} \hat{\mathbf{x}} + by_{11} \hat{\mathbf{y}} + cz_{11} \hat{\mathbf{z}} & (8b) & \text{Si III} \\
\mathbf{B}_{30} &= \begin{pmatrix} -(x_{11} - y_{11}) \mathbf{a}_1 - \\ (x_{11} + y_{11}) \mathbf{a}_2 + (z_{11} + \frac{1}{2}) \mathbf{a}_3 \end{pmatrix} = -ax_{11} \hat{\mathbf{x}} - by_{11} \hat{\mathbf{y}} + c(z_{11} + \frac{1}{2}) \hat{\mathbf{z}} & (8b) & \text{Si III} \\
\mathbf{B}_{31} &= \begin{pmatrix} (x_{11} + y_{11}) \mathbf{a}_1 + \\ (x_{11} - y_{11}) \mathbf{a}_2 + (z_{11} + \frac{1}{2}) \mathbf{a}_3 \end{pmatrix} = ax_{11} \hat{\mathbf{x}} - by_{11} \hat{\mathbf{y}} + c(z_{11} + \frac{1}{2}) \hat{\mathbf{z}} & (8b) & \text{Si III} \\
\mathbf{B}_{32} &= \begin{pmatrix} -(x_{11} + y_{11}) \mathbf{a}_1 - \\ (x_{11} - y_{11}) \mathbf{a}_2 + z_{11} \mathbf{a}_3 \end{pmatrix} = -ax_{11} \hat{\mathbf{x}} + by_{11} \hat{\mathbf{y}} + cz_{11} \hat{\mathbf{z}} & (8b) & \text{Si III} \\
\mathbf{B}_{33} &= \begin{pmatrix} (x_{12} - y_{12}) \mathbf{a}_1 + \\ (x_{12} + y_{12}) \mathbf{a}_2 + z_{12} \mathbf{a}_3 \end{pmatrix} = ax_{12} \hat{\mathbf{x}} + by_{12} \hat{\mathbf{y}} + cz_{12} \hat{\mathbf{z}} & (8b) & \text{Si IV} \\
\mathbf{B}_{34} &= \begin{pmatrix} -(x_{12} - y_{12}) \mathbf{a}_1 - \\ (x_{12} + y_{12}) \mathbf{a}_2 + (z_{12} + \frac{1}{2}) \mathbf{a}_3 \end{pmatrix} = -ax_{12} \hat{\mathbf{x}} - by_{12} \hat{\mathbf{y}} + c(z_{12} + \frac{1}{2}) \hat{\mathbf{z}} & (8b) & \text{Si IV} \\
\mathbf{B}_{35} &= \begin{pmatrix} (x_{12} + y_{12}) \mathbf{a}_1 + \\ (x_{12} - y_{12}) \mathbf{a}_2 + (z_{12} + \frac{1}{2}) \mathbf{a}_3 \end{pmatrix} = ax_{12} \hat{\mathbf{x}} - by_{12} \hat{\mathbf{y}} + c(z_{12} + \frac{1}{2}) \hat{\mathbf{z}} & (8b) & \text{Si IV} \\
\mathbf{B}_{36} &= \begin{pmatrix} -(x_{12} + y_{12}) \mathbf{a}_1 - \\ (x_{12} - y_{12}) \mathbf{a}_2 + z_{12} \mathbf{a}_3 \end{pmatrix} = -ax_{12} \hat{\mathbf{x}} + by_{12} \hat{\mathbf{y}} + cz_{12} \hat{\mathbf{z}} & (8b) & \text{Si IV} \\
\mathbf{B}_{37} &= \begin{pmatrix} (x_{13} - y_{13}) \mathbf{a}_1 + \\ (x_{13} + y_{13}) \mathbf{a}_2 + z_{13} \mathbf{a}_3 \end{pmatrix} = ax_{13} \hat{\mathbf{x}} + by_{13} \hat{\mathbf{y}} + cz_{13} \hat{\mathbf{z}} & (8b) & \text{Si V} \\
\mathbf{B}_{38} &= \begin{pmatrix} -(x_{13} - y_{13}) \mathbf{a}_1 - \\ (x_{13} + y_{13}) \mathbf{a}_2 + (z_{13} + \frac{1}{2}) \mathbf{a}_3 \end{pmatrix} = -ax_{13} \hat{\mathbf{x}} - by_{13} \hat{\mathbf{y}} + c(z_{13} + \frac{1}{2}) \hat{\mathbf{z}} & (8b) & \text{Si V} \\
\mathbf{B}_{39} &= \begin{pmatrix} (x_{13} + y_{13}) \mathbf{a}_1 + \\ (x_{13} - y_{13}) \mathbf{a}_2 + (z_{13} + \frac{1}{2}) \mathbf{a}_3 \end{pmatrix} = ax_{13} \hat{\mathbf{x}} - by_{13} \hat{\mathbf{y}} + c(z_{13} + \frac{1}{2}) \hat{\mathbf{z}} & (8b) & \text{Si V} \\
\mathbf{B}_{40} &= \begin{pmatrix} -(x_{13} + y_{13}) \mathbf{a}_1 - \\ (x_{13} - y_{13}) \mathbf{a}_2 + z_{13} \mathbf{a}_3 \end{pmatrix} = -ax_{13} \hat{\mathbf{x}} + by_{13} \hat{\mathbf{y}} + cz_{13} \hat{\mathbf{z}} & (8b) & \text{Si V}
\end{aligned}$$

References

- [1] G. Pilström, *The Crystal Structure of Ni₃Si₂ with some Notes on Ni₅Si₂*, Acta Chem. Scand. **15**, 893–902 (1961), doi:10.3891/acta.chem.scand.15-0893.