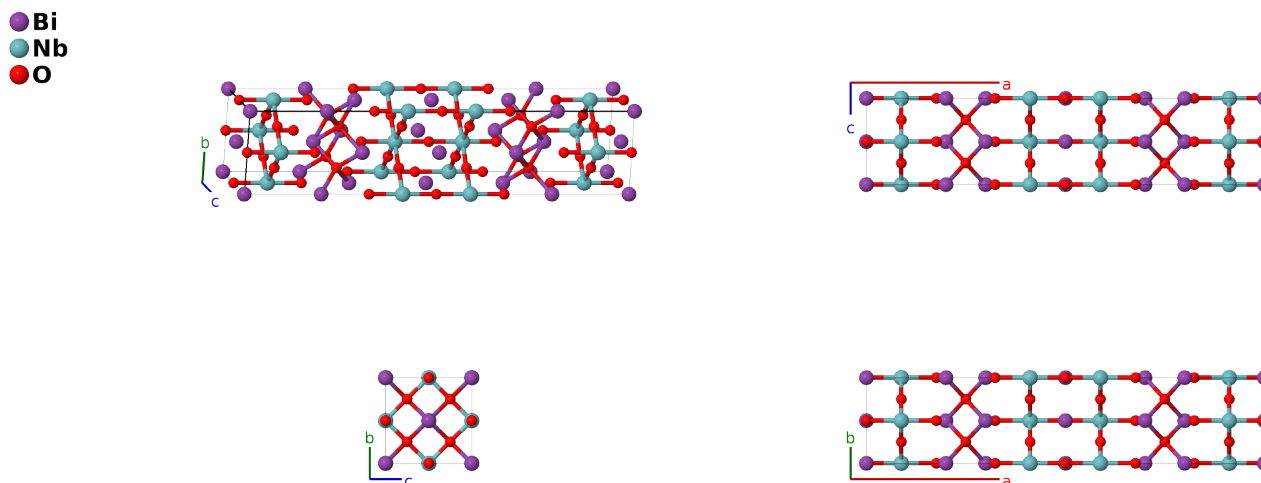


Orthorhombic $\text{Bi}_3\text{NbTiO}_9$ $m = 2$ Aurivillius Structure: A3B2C9_oF56_69_ag_g_bfgl-001

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<https://afLOW.org/p/FSA1>

https://afLOW.org/p/A3B2C9_oF56_69_ag_g_bfgl-001



Prototype	$\text{Bi}_3\text{Nb}_2\text{O}_9$
AFLOW prototype label	A3B2C9_oF56_69_ag_g_bfgl-001
ICSD	24734
Pearson symbol	oF56
Space group number	69
Space group symbol	$Fmmm$
AFLOW prototype command	<code>afLOW --proto=A3B2C9_oF56_69_ag_g_bfgl-001 --params=a, b/a, c/a, x4, x5, x6, x7</code>

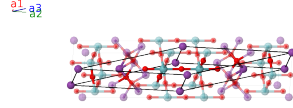
Other compounds with this structure

$\text{BaBi}_2\text{Nb}_2\text{O}_9$, $\text{CaBi}_2\text{Nb}_2\text{O}_9$, $\text{KBi}_2\text{Nb}_2\text{O}_9$, $\text{NaBi}_2\text{Nb}_2\text{O}_9$, $\text{PbBi}_2\text{Nb}_2\text{O}_9$, $\text{SrBi}_2\text{Nb}_2\text{O}_9$

- Aurivillius phases are layered tetragonal materials with composition $(\text{Me}'_2\text{O}_2)^{2+}(\text{Me}_{m-1}\text{R}_m\text{O}_{3m+1})^{2-}$ ($\text{Me}_{m-1}\text{Me}'_2\text{R}_m\text{O}_{3(m+1)}$), where Me and Me' are metals and R is a transition metal with a charge of +4 or +5. (Subbaro, 1962)
- This is the original structural determination by (Aurivillius, 1949). The niobium and titanium atoms equally occupy the same (8g) site. We have arbitrarily labeled this as “Nb.”
- Crystals such as $\text{BaBi}_2\text{Nb}_2\text{O}_9$ put the non-bismuth atom on the (4a) site, and the niobium site can be occupied by niobium, tantalum, and/or titanium. (Aurivillius, 1949)
- We have swapped Aurivillius's x - and z -axes.

Face-centered Orthorhombic primitive vectors

$$\begin{aligned}\mathbf{a}_1 &= \frac{1}{2}b\hat{\mathbf{y}} + \frac{1}{2}c\hat{\mathbf{z}} \\ \mathbf{a}_2 &= \frac{1}{2}a\hat{\mathbf{x}} + \frac{1}{2}c\hat{\mathbf{z}} \\ \mathbf{a}_3 &= \frac{1}{2}a\hat{\mathbf{x}} + \frac{1}{2}b\hat{\mathbf{y}}\end{aligned}$$



Basis vectors

	Lattice coordinates		Cartesian coordinates	Wyckoff position	Atom type
\mathbf{B}_1	$=$	0	$=$	0	(4a) Bi I
\mathbf{B}_2	$=$	$\frac{1}{2}\mathbf{a}_1 + \frac{1}{2}\mathbf{a}_2 + \frac{1}{2}\mathbf{a}_3$	$=$	$\frac{1}{2}a\hat{\mathbf{x}} + \frac{1}{2}b\hat{\mathbf{y}} + \frac{1}{2}c\hat{\mathbf{z}}$	(4b) O I
\mathbf{B}_3	$=$	$\frac{1}{4}\mathbf{a}_1 + \frac{1}{4}\mathbf{a}_2 + \frac{1}{4}\mathbf{a}_3$	$=$	$\frac{1}{4}a\hat{\mathbf{x}} + \frac{1}{4}b\hat{\mathbf{y}} + \frac{1}{4}c\hat{\mathbf{z}}$	(8f) O II
\mathbf{B}_4	$=$	$\frac{3}{4}\mathbf{a}_1 + \frac{3}{4}\mathbf{a}_2 + \frac{3}{4}\mathbf{a}_3$	$=$	$\frac{3}{4}a\hat{\mathbf{x}} + \frac{3}{4}b\hat{\mathbf{y}} + \frac{3}{4}c\hat{\mathbf{z}}$	(8f) O II
\mathbf{B}_5	$=$	$-x_4\mathbf{a}_1 + x_4\mathbf{a}_2 + x_4\mathbf{a}_3$	$=$	$ax_4\hat{\mathbf{x}}$	(8g) Bi II
\mathbf{B}_6	$=$	$x_4\mathbf{a}_1 - x_4\mathbf{a}_2 - x_4\mathbf{a}_3$	$=$	$-ax_4\hat{\mathbf{x}}$	(8g) Bi II
\mathbf{B}_7	$=$	$-x_5\mathbf{a}_1 + x_5\mathbf{a}_2 + x_5\mathbf{a}_3$	$=$	$ax_5\hat{\mathbf{x}}$	(8g) Nb I
\mathbf{B}_8	$=$	$x_5\mathbf{a}_1 - x_5\mathbf{a}_2 - x_5\mathbf{a}_3$	$=$	$-ax_5\hat{\mathbf{x}}$	(8g) Nb I
\mathbf{B}_9	$=$	$-x_6\mathbf{a}_1 + x_6\mathbf{a}_2 + x_6\mathbf{a}_3$	$=$	$ax_6\hat{\mathbf{x}}$	(8g) O III
\mathbf{B}_{10}	$=$	$x_6\mathbf{a}_1 - x_6\mathbf{a}_2 - x_6\mathbf{a}_3$	$=$	$-ax_6\hat{\mathbf{x}}$	(8g) O III
\mathbf{B}_{11}	$=$	$-(x_7 - \frac{1}{2})\mathbf{a}_1 + x_7\mathbf{a}_2 + x_7\mathbf{a}_3$	$=$	$ax_7\hat{\mathbf{x}} + \frac{1}{4}b\hat{\mathbf{y}} + \frac{1}{4}c\hat{\mathbf{z}}$	(16l) O IV
\mathbf{B}_{12}	$=$	$x_7\mathbf{a}_1 - (x_7 - \frac{1}{2})\mathbf{a}_2 - (x_7 - \frac{1}{2})\mathbf{a}_3$	$=$	$-a(x_7 - \frac{1}{2})\hat{\mathbf{x}} + \frac{1}{4}b\hat{\mathbf{y}} + \frac{1}{4}c\hat{\mathbf{z}}$	(16l) O IV
\mathbf{B}_{13}	$=$	$(x_7 + \frac{1}{2})\mathbf{a}_1 - x_7\mathbf{a}_2 - x_7\mathbf{a}_3$	$=$	$-ax_7\hat{\mathbf{x}} + \frac{1}{4}b\hat{\mathbf{y}} + \frac{1}{4}c\hat{\mathbf{z}}$	(16l) O IV
\mathbf{B}_{14}	$=$	$-x_7\mathbf{a}_1 + (x_7 + \frac{1}{2})\mathbf{a}_2 + (x_7 + \frac{1}{2})\mathbf{a}_3$	$=$	$a(x_7 + \frac{1}{2})\hat{\mathbf{x}} + \frac{1}{4}b\hat{\mathbf{y}} + \frac{1}{4}c\hat{\mathbf{z}}$	(16l) O IV

References

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