

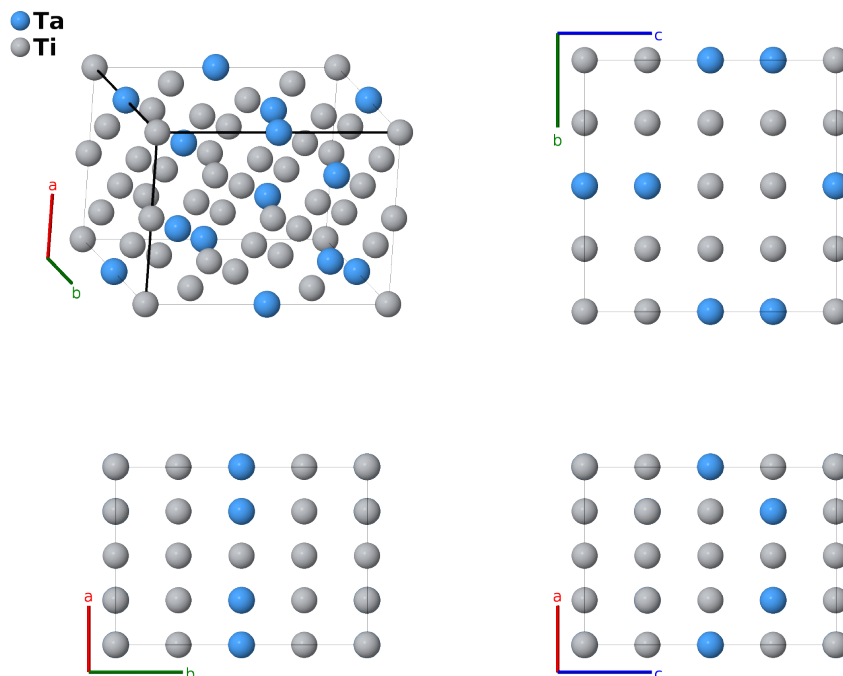
# Ta<sub>3</sub>Ti<sub>13</sub> (BCC SQS-16) Structure: A3B13\_oC32\_38\_ac\_a2bcdef-001

This structure originally had the label A3B13\_oC32\_38\_ac\_a2bcdef. Calls to that address will be redirected here.

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<https://afLOW.org/p/A2U8>

[https://afLOW.org/p/A3B13\\_oC32\\_38\\_ac\\_a2bcdef-001](https://afLOW.org/p/A3B13_oC32_38_ac_a2bcdef-001)



<b>Prototype</b>	Ta <sub>3</sub> Ti <sub>13</sub>
<b>AFLOW prototype label</b>	A3B13_oC32_38_ac_a2bcdef-001
<b>ICSD</b>	none
<b>Pearson symbol</b>	oC32
<b>Space group number</b>	38
<b>Space group symbol</b>	<i>Amm</i> 2
<b>AFLOW prototype command</b>	<code>afLOW --proto=A3B13_oC32_38_ac_a2bcdef-001 --params=a, b/a, c/a, z<sub>1</sub>, z<sub>2</sub>, z<sub>3</sub>, z<sub>4</sub>, x<sub>5</sub>, z<sub>5</sub>, x<sub>6</sub>, z<sub>6</sub>, y<sub>7</sub>, z<sub>7</sub>, y<sub>8</sub>, z<sub>8</sub>, x<sub>9</sub>, y<sub>9</sub>, z<sub>9</sub></code>

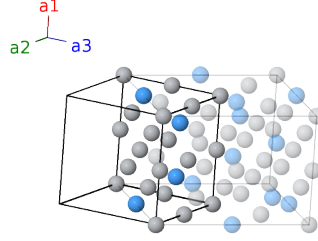
- This is a special quasirandom structure with 16 atoms per unit cell (SQS-16) for a bcc binary substitutional alloy A<sub>x</sub>B<sub>1-x</sub> (Jiang, 2004; Chakraborty, 2016)).
- Several compositions are available:
  - TaTi<sub>7</sub> (AB7\_hR16\_166\_c.c2h) ,

- Ta<sub>3</sub>Ti<sub>13</sub> (A3B13\_oC32\_38\_ac\_a2bcdef) (this structure),
- TaTi<sub>3</sub>-I (AB3\_mC32\_8\_4a\_12a) ,
- TaTi<sub>3</sub>-II (AB3\_mC32\_8\_4a\_4a4b) ,
- Ta<sub>5</sub>Ti<sub>11</sub> (A5B11\_mP16\_6\_2abc\_2a3b3c) ,
- Ta<sub>3</sub>Ti<sub>8</sub> (A3B5\_oC32\_38\_abce\_abcdef) ,
- TaTi (AB\_aP16\_2\_4i\_4i).

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### Base-centered Orthorhombic primitive vectors

$$\begin{aligned} \mathbf{a}_1 &= a \hat{\mathbf{x}} \\ \mathbf{a}_2 &= \frac{1}{2}b \hat{\mathbf{y}} - \frac{1}{2}c \hat{\mathbf{z}} \\ \mathbf{a}_3 &= \frac{1}{2}b \hat{\mathbf{y}} + \frac{1}{2}c \hat{\mathbf{z}} \end{aligned}$$




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### Basis vectors

	Lattice coordinates		Cartesian coordinates	Wyckoff position	Atom type
$\mathbf{B}_1$	$= -z_1 \mathbf{a}_2 + z_1 \mathbf{a}_3$	$=$	$cz_1 \hat{\mathbf{z}}$	(2a)	Ta I
$\mathbf{B}_2$	$= -z_2 \mathbf{a}_2 + z_2 \mathbf{a}_3$	$=$	$cz_2 \hat{\mathbf{z}}$	(2a)	Ti I
$\mathbf{B}_3$	$= \frac{1}{2} \mathbf{a}_1 - z_3 \mathbf{a}_2 + z_3 \mathbf{a}_3$	$=$	$\frac{1}{2}a \hat{\mathbf{x}} + cz_3 \hat{\mathbf{z}}$	(2b)	Ti II
$\mathbf{B}_4$	$= \frac{1}{2} \mathbf{a}_1 - z_4 \mathbf{a}_2 + z_4 \mathbf{a}_3$	$=$	$\frac{1}{2}a \hat{\mathbf{x}} + cz_4 \hat{\mathbf{z}}$	(2b)	Ti III
$\mathbf{B}_5$	$= x_5 \mathbf{a}_1 - z_5 \mathbf{a}_2 + z_5 \mathbf{a}_3$	$=$	$ax_5 \hat{\mathbf{x}} + cz_5 \hat{\mathbf{z}}$	(4c)	Ta II
$\mathbf{B}_6$	$= -x_5 \mathbf{a}_1 - z_5 \mathbf{a}_2 + z_5 \mathbf{a}_3$	$=$	$-ax_5 \hat{\mathbf{x}} + cz_5 \hat{\mathbf{z}}$	(4c)	Ta II
$\mathbf{B}_7$	$= x_6 \mathbf{a}_1 - z_6 \mathbf{a}_2 + z_6 \mathbf{a}_3$	$=$	$ax_6 \hat{\mathbf{x}} + cz_6 \hat{\mathbf{z}}$	(4c)	Ti IV
$\mathbf{B}_8$	$= -x_6 \mathbf{a}_1 - z_6 \mathbf{a}_2 + z_6 \mathbf{a}_3$	$=$	$-ax_6 \hat{\mathbf{x}} + cz_6 \hat{\mathbf{z}}$	(4c)	Ti IV
$\mathbf{B}_9$	$= (y_7 - z_7) \mathbf{a}_2 + (y_7 + z_7) \mathbf{a}_3$	$=$	$by_7 \hat{\mathbf{y}} + cz_7 \hat{\mathbf{z}}$	(4d)	Ti V
$\mathbf{B}_{10}$	$= -(y_7 + z_7) \mathbf{a}_2 - (y_7 - z_7) \mathbf{a}_3$	$=$	$-by_7 \hat{\mathbf{y}} + cz_7 \hat{\mathbf{z}}$	(4d)	Ti V
$\mathbf{B}_{11}$	$= \frac{1}{2} \mathbf{a}_1 + (y_8 - z_8) \mathbf{a}_2 + (y_8 + z_8) \mathbf{a}_3$	$=$	$\frac{1}{2}a \hat{\mathbf{x}} + by_8 \hat{\mathbf{y}} + cz_8 \hat{\mathbf{z}}$	(4e)	Ti VI
$\mathbf{B}_{12}$	$= \frac{1}{2} \mathbf{a}_1 - (y_8 + z_8) \mathbf{a}_2 - (y_8 - z_8) \mathbf{a}_3$	$=$	$\frac{1}{2}a \hat{\mathbf{x}} - by_8 \hat{\mathbf{y}} + cz_8 \hat{\mathbf{z}}$	(4e)	Ti VI
$\mathbf{B}_{13}$	$= x_9 \mathbf{a}_1 + (y_9 - z_9) \mathbf{a}_2 + (y_9 + z_9) \mathbf{a}_3$	$=$	$ax_9 \hat{\mathbf{x}} + by_9 \hat{\mathbf{y}} + cz_9 \hat{\mathbf{z}}$	(8f)	Ti VII
$\mathbf{B}_{14}$	$= -x_9 \mathbf{a}_1 - (y_9 + z_9) \mathbf{a}_2 - (y_9 - z_9) \mathbf{a}_3$	$=$	$-ax_9 \hat{\mathbf{x}} - by_9 \hat{\mathbf{y}} + cz_9 \hat{\mathbf{z}}$	(8f)	Ti VII
$\mathbf{B}_{15}$	$= x_9 \mathbf{a}_1 - (y_9 + z_9) \mathbf{a}_2 - (y_9 - z_9) \mathbf{a}_3$	$=$	$ax_9 \hat{\mathbf{x}} - by_9 \hat{\mathbf{y}} + cz_9 \hat{\mathbf{z}}$	(8f)	Ti VII
$\mathbf{B}_{16}$	$= -x_9 \mathbf{a}_1 + (y_9 - z_9) \mathbf{a}_2 + (y_9 + z_9) \mathbf{a}_3$	$=$	$-ax_9 \hat{\mathbf{x}} + by_9 \hat{\mathbf{y}} + cz_9 \hat{\mathbf{z}}$	(8f)	Ti VII

### References

- [1] C. Jiang, C. Wolverton, J. Sofo, L.-Q. Chen, and Z.-K. Liu, *First-principles study of binary bcc alloys using special quasirandom structures*, Phys. Rev. B **69**, 214202 (2004), doi:10.1103/PhysRevB.69.214202.

- [2] T. Chakraborty, J. Rogal, and R. Drautz, *Unraveling the composition dependence of the martensitic transformation temperature: A first-principles study of Ti-Ta alloys*, Phys. Rev. B **94**, 224104 (2016), doi:10.1103/PhysRevB.94.224104.