

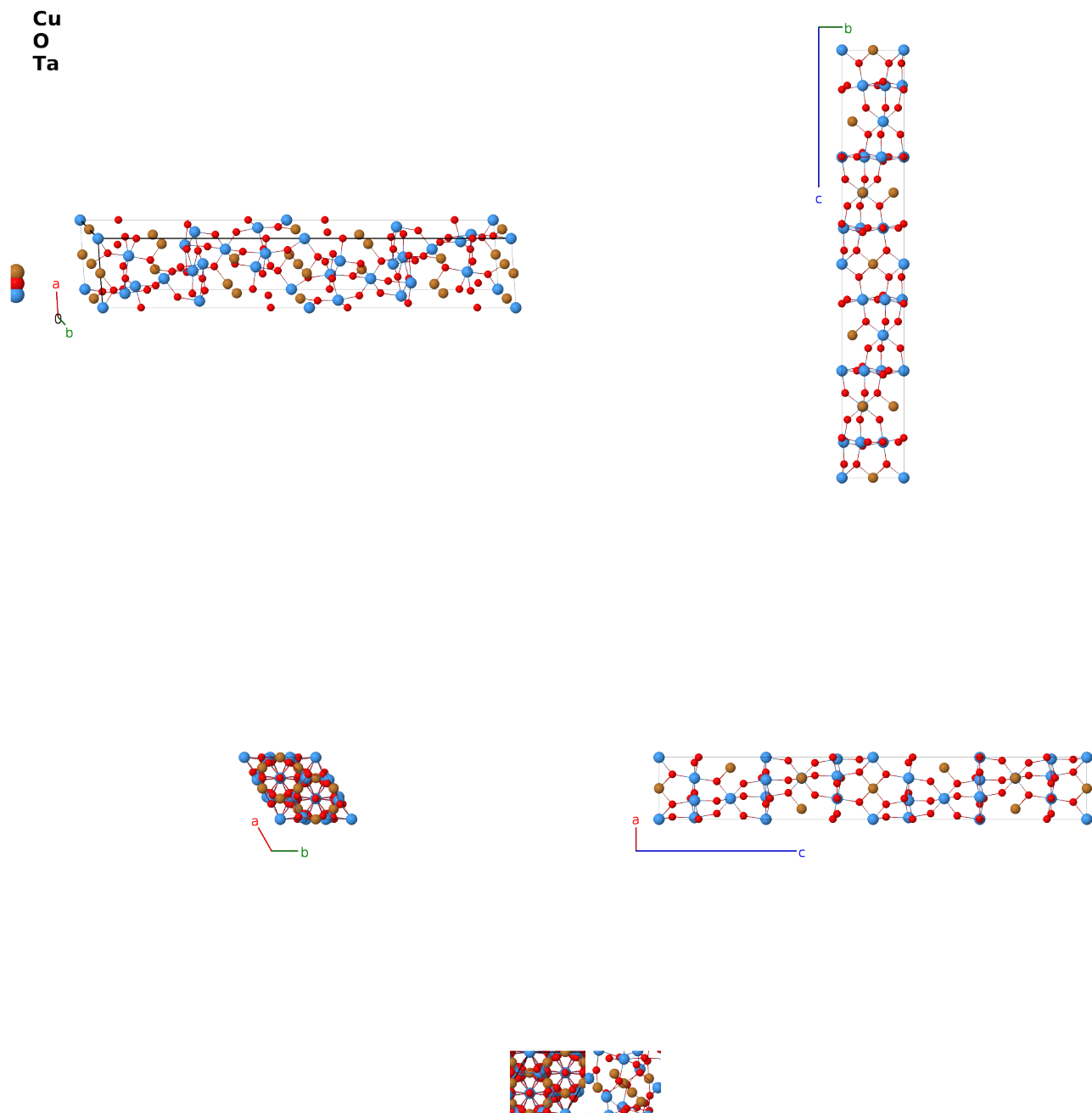
Cu₂Ta₄O₁₁ Structure: A3B11C4_hR36_167_d_cef_be-001

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<https://aflow.org/prototype-encyclopedia/AGLP>

https://aflow.org/prototype-encyclopedia/A3B11C4_hR36_167_d_cef_be-001



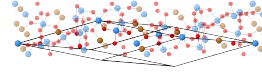
Prototype	Cu ₂ O ₁₁ Ta ₄
AFLOW prototype label	A3B11C4_hR36.167_d_cef_be-001
ICSD	194463
CCDC	1703148
Pearson symbol	hR36
Space group number	167
Space group symbol	$R\bar{3}c$
AFLOW prototype command	aflow --proto=A3B11C4_hR36.167_d_cef_be-001 --params= $a, c/a, x_2, x_4, x_5, x_6, y_6, z_6$

- Only two-thirds of the (6d) site are filled with copper atoms.

Rhombohedral primitive vectors

$$\begin{aligned}
\mathbf{a}_1 &= \frac{1}{2}a \hat{\mathbf{x}} - \frac{\sqrt{3}}{6}a \hat{\mathbf{y}} + \frac{1}{3}c \hat{\mathbf{z}} \\
\mathbf{a}_2 &= \frac{1}{\sqrt{3}}a \hat{\mathbf{y}} + \frac{1}{3}c \hat{\mathbf{z}} \\
\mathbf{a}_3 &= -\frac{1}{2}a \hat{\mathbf{x}} - \frac{\sqrt{3}}{6}a \hat{\mathbf{y}} + \frac{1}{3}c \hat{\mathbf{z}}
\end{aligned}$$

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Basis vectors

	Lattice coordinates		Cartesian coordinates	Wyckoff position	Atom type
$\mathbf{B}_1$	$=$	0	$=$	0	Ta I
$\mathbf{B}_2$	$=$	$\frac{1}{2} \mathbf{a}_1 + \frac{1}{2} \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	$=$	$\frac{1}{2}c \hat{\mathbf{z}}$	Ta I
$\mathbf{B}_3$	$=$	$x_2 \mathbf{a}_1 + x_2 \mathbf{a}_2 + x_2 \mathbf{a}_3$	$=$	$cx_2 \hat{\mathbf{z}}$	O I
$\mathbf{B}_4$	$=$	$-\left(x_2 - \frac{1}{2}\right) \mathbf{a}_1 - \left(x_2 - \frac{1}{2}\right) \mathbf{a}_2 - \left(x_2 - \frac{1}{2}\right) \mathbf{a}_3$	$=$	$-c \left(x_2 - \frac{1}{2}\right) \hat{\mathbf{z}}$	O I
$\mathbf{B}_5$	$=$	$-x_2 \mathbf{a}_1 - x_2 \mathbf{a}_2 - x_2 \mathbf{a}_3$	$=$	$-cx_2 \hat{\mathbf{z}}$	O I
$\mathbf{B}_6$	$=$	$\left(x_2 + \frac{1}{2}\right) \mathbf{a}_1 + \left(x_2 + \frac{1}{2}\right) \mathbf{a}_2 + \left(x_2 + \frac{1}{2}\right) \mathbf{a}_3$	$=$	$c \left(x_2 + \frac{1}{2}\right) \hat{\mathbf{z}}$	O I
$\mathbf{B}_7$	$=$	$\frac{1}{2} \mathbf{a}_1$	$=$	$\frac{1}{4}a \hat{\mathbf{x}} - \frac{\sqrt{3}}{12}a \hat{\mathbf{y}} + \frac{1}{6}c \hat{\mathbf{z}}$	Cu I
$\mathbf{B}_8$	$=$	$\frac{1}{2} \mathbf{a}_2$	$=$	$\frac{\sqrt{3}}{6}a \hat{\mathbf{y}} + \frac{1}{6}c \hat{\mathbf{z}}$	Cu I
$\mathbf{B}_9$	$=$	$\frac{1}{2} \mathbf{a}_3$	$=$	$-\frac{1}{4}a \hat{\mathbf{x}} - \frac{\sqrt{3}}{12}a \hat{\mathbf{y}} + \frac{1}{6}c \hat{\mathbf{z}}$	Cu I
$\mathbf{B}_{10}$	$=$	$\frac{1}{2} \mathbf{a}_1 + \frac{1}{2} \mathbf{a}_2$	$=$	$\frac{1}{4}a \hat{\mathbf{x}} + \frac{\sqrt{3}}{12}a \hat{\mathbf{y}} + \frac{1}{3}c \hat{\mathbf{z}}$	Cu I
$\mathbf{B}_{11}$	$=$	$\frac{1}{2} \mathbf{a}_1 + \frac{1}{2} \mathbf{a}_3$	$=$	$-\frac{\sqrt{3}}{6}a \hat{\mathbf{y}} + \frac{1}{3}c \hat{\mathbf{z}}$	Cu I
$\mathbf{B}_{12}$	$=$	$\frac{1}{2} \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	$=$	$-\frac{1}{4}a \hat{\mathbf{x}} + \frac{\sqrt{3}}{12}a \hat{\mathbf{y}} + \frac{1}{3}c \hat{\mathbf{z}}$	Cu I
$\mathbf{B}_{13}$	$=$	$x_4 \mathbf{a}_1 - \left(x_4 - \frac{1}{2}\right) \mathbf{a}_2 + \frac{1}{4} \mathbf{a}_3$	$=$	$\frac{1}{8}a (4x_4 - 1) \hat{\mathbf{x}} - \frac{\sqrt{3}}{8}a (4x_4 - 1) \hat{\mathbf{y}} + \frac{1}{4}c \hat{\mathbf{z}}$	O II

$\mathbf{B}_{14} =$	$\frac{1}{4} \mathbf{a}_1 + x_4 \mathbf{a}_2 - (x_4 - \frac{1}{2}) \mathbf{a}_3$	$=$	$\frac{1}{8} a (4x_4 - 1) \hat{\mathbf{x}} + \frac{\sqrt{3}}{8} a (4x_4 - 1) \hat{\mathbf{y}} + \frac{1}{4} c \hat{\mathbf{z}}$	(6e)	O II
$\mathbf{B}_{15} =$	$-(x_4 - \frac{1}{2}) \mathbf{a}_1 + \frac{1}{4} \mathbf{a}_2 + x_4 \mathbf{a}_3$	$=$	$-a (x_4 - \frac{1}{4}) \hat{\mathbf{x}} + \frac{1}{4} c \hat{\mathbf{z}}$	(6e)	O II
$\mathbf{B}_{16} =$	$-x_4 \mathbf{a}_1 + (x_4 + \frac{1}{2}) \mathbf{a}_2 + \frac{3}{4} \mathbf{a}_3$	$=$	$-\frac{1}{8} a (4x_4 + 3) \hat{\mathbf{x}} + \frac{\sqrt{3}}{24} a (12x_4 + 1) \hat{\mathbf{y}} + \frac{5}{12} c \hat{\mathbf{z}}$	(6e)	O II
$\mathbf{B}_{17} =$	$\frac{3}{4} \mathbf{a}_1 - x_4 \mathbf{a}_2 + (x_4 + \frac{1}{2}) \mathbf{a}_3$	$=$	$-\frac{1}{8} a (4x_4 - 1) \hat{\mathbf{x}} - \frac{\sqrt{3}}{24} a (12x_4 + 5) \hat{\mathbf{y}} + \frac{5}{12} c \hat{\mathbf{z}}$	(6e)	O II
$\mathbf{B}_{18} =$	$(x_4 + \frac{1}{2}) \mathbf{a}_1 + \frac{3}{4} \mathbf{a}_2 - x_4 \mathbf{a}_3$	$=$	$a (x_4 + \frac{1}{4}) \hat{\mathbf{x}} + \frac{\sqrt{3}}{6} a \hat{\mathbf{y}} + \frac{5}{12} c \hat{\mathbf{z}}$	(6e)	O II
$\mathbf{B}_{19} =$	$x_5 \mathbf{a}_1 - (x_5 - \frac{1}{2}) \mathbf{a}_2 + \frac{1}{4} \mathbf{a}_3$	$=$	$\frac{1}{8} a (4x_5 - 1) \hat{\mathbf{x}} - \frac{\sqrt{3}}{8} a (4x_5 - 1) \hat{\mathbf{y}} + \frac{1}{4} c \hat{\mathbf{z}}$	(6e)	Ta II
$\mathbf{B}_{20} =$	$\frac{1}{4} \mathbf{a}_1 + x_5 \mathbf{a}_2 - (x_5 - \frac{1}{2}) \mathbf{a}_3$	$=$	$\frac{1}{8} a (4x_5 - 1) \hat{\mathbf{x}} + \frac{\sqrt{3}}{8} a (4x_5 - 1) \hat{\mathbf{y}} + \frac{1}{4} c \hat{\mathbf{z}}$	(6e)	Ta II
$\mathbf{B}_{21} =$	$-(x_5 - \frac{1}{2}) \mathbf{a}_1 + \frac{1}{4} \mathbf{a}_2 + x_5 \mathbf{a}_3$	$=$	$-a (x_5 - \frac{1}{4}) \hat{\mathbf{x}} + \frac{1}{4} c \hat{\mathbf{z}}$	(6e)	Ta II
$\mathbf{B}_{22} =$	$-x_5 \mathbf{a}_1 + (x_5 + \frac{1}{2}) \mathbf{a}_2 + \frac{3}{4} \mathbf{a}_3$	$=$	$-\frac{1}{8} a (4x_5 + 3) \hat{\mathbf{x}} + \frac{\sqrt{3}}{24} a (12x_5 + 1) \hat{\mathbf{y}} + \frac{5}{12} c \hat{\mathbf{z}}$	(6e)	Ta II
$\mathbf{B}_{23} =$	$\frac{3}{4} \mathbf{a}_1 - x_5 \mathbf{a}_2 + (x_5 + \frac{1}{2}) \mathbf{a}_3$	$=$	$-\frac{1}{8} a (4x_5 - 1) \hat{\mathbf{x}} - \frac{\sqrt{3}}{24} a (12x_5 + 5) \hat{\mathbf{y}} + \frac{5}{12} c \hat{\mathbf{z}}$	(6e)	Ta II
$\mathbf{B}_{24} =$	$(x_5 + \frac{1}{2}) \mathbf{a}_1 + \frac{3}{4} \mathbf{a}_2 - x_5 \mathbf{a}_3$	$=$	$a (x_5 + \frac{1}{4}) \hat{\mathbf{x}} + \frac{\sqrt{3}}{6} a \hat{\mathbf{y}} + \frac{5}{12} c \hat{\mathbf{z}}$	(6e)	Ta II
$\mathbf{B}_{25} =$	$x_6 \mathbf{a}_1 + y_6 \mathbf{a}_2 + z_6 \mathbf{a}_3$	$=$	$\frac{1}{2} a (x_6 - z_6) \hat{\mathbf{x}} - \frac{\sqrt{3}}{6} a (x_6 - 2y_6 + z_6) \hat{\mathbf{y}} + \frac{1}{3} c (x_6 + y_6 + z_6) \hat{\mathbf{z}}$	(12f)	O III
$\mathbf{B}_{26} =$	$z_6 \mathbf{a}_1 + x_6 \mathbf{a}_2 + y_6 \mathbf{a}_3$	$=$	$-\frac{1}{2} a (y_6 - z_6) \hat{\mathbf{x}} + \frac{\sqrt{3}}{6} a (2x_6 - y_6 - z_6) \hat{\mathbf{y}} + \frac{1}{3} c (x_6 + y_6 + z_6) \hat{\mathbf{z}}$	(12f)	O III
$\mathbf{B}_{27} =$	$y_6 \mathbf{a}_1 + z_6 \mathbf{a}_2 + x_6 \mathbf{a}_3$	$=$	$-\frac{1}{2} a (x_6 - y_6) \hat{\mathbf{x}} - \frac{\sqrt{3}}{6} a (x_6 + y_6 - 2z_6) \hat{\mathbf{y}} + \frac{1}{3} c (x_6 + y_6 + z_6) \hat{\mathbf{z}}$	(12f)	O III
$\mathbf{B}_{28} =$	$-(z_6 - \frac{1}{2}) \mathbf{a}_1 - (y_6 - \frac{1}{2}) \mathbf{a}_2 - (x_6 - \frac{1}{2}) \mathbf{a}_3$	$=$	$\frac{1}{2} a (x_6 - z_6) \hat{\mathbf{x}} + \frac{\sqrt{3}}{6} a (x_6 - 2y_6 + z_6) \hat{\mathbf{y}} - \frac{1}{6} c (2x_6 + 2y_6 + 2z_6 - 3) \hat{\mathbf{z}}$	(12f)	O III
$\mathbf{B}_{29} =$	$-(y_6 - \frac{1}{2}) \mathbf{a}_1 - (x_6 - \frac{1}{2}) \mathbf{a}_2 - (z_6 - \frac{1}{2}) \mathbf{a}_3$	$=$	$-\frac{1}{2} a (y_6 - z_6) \hat{\mathbf{x}} - \frac{\sqrt{3}}{6} a (2x_6 - y_6 - z_6) \hat{\mathbf{y}} - \frac{1}{6} c (2x_6 + 2y_6 + 2z_6 - 3) \hat{\mathbf{z}}$	(12f)	O III
$\mathbf{B}_{30} =$	$-(x_6 - \frac{1}{2}) \mathbf{a}_1 - (z_6 - \frac{1}{2}) \mathbf{a}_2 - (y_6 - \frac{1}{2}) \mathbf{a}_3$	$=$	$-\frac{1}{2} a (x_6 - y_6) \hat{\mathbf{x}} + \frac{\sqrt{3}}{6} a (x_6 + y_6 - 2z_6) \hat{\mathbf{y}} - \frac{1}{6} c (2x_6 + 2y_6 + 2z_6 - 3) \hat{\mathbf{z}}$	(12f)	O III
$\mathbf{B}_{31} =$	$-x_6 \mathbf{a}_1 - y_6 \mathbf{a}_2 - z_6 \mathbf{a}_3$	$=$	$-\frac{1}{2} a (x_6 - z_6) \hat{\mathbf{x}} + \frac{\sqrt{3}}{6} a (x_6 - 2y_6 + z_6) \hat{\mathbf{y}} - \frac{1}{3} c (x_6 + y_6 + z_6) \hat{\mathbf{z}}$	(12f)	O III
$\mathbf{B}_{32} =$	$-z_6 \mathbf{a}_1 - x_6 \mathbf{a}_2 - y_6 \mathbf{a}_3$	$=$	$\frac{1}{2} a (y_6 - z_6) \hat{\mathbf{x}} - \frac{\sqrt{3}}{6} a (2x_6 - y_6 - z_6) \hat{\mathbf{y}} - \frac{1}{3} c (x_6 + y_6 + z_6) \hat{\mathbf{z}}$	(12f)	O III
$\mathbf{B}_{33} =$	$-y_6 \mathbf{a}_1 - z_6 \mathbf{a}_2 - x_6 \mathbf{a}_3$	$=$	$\frac{1}{2} a (x_6 - y_6) \hat{\mathbf{x}} + \frac{\sqrt{3}}{6} a (x_6 + y_6 - 2z_6) \hat{\mathbf{y}} - \frac{1}{3} c (x_6 + y_6 + z_6) \hat{\mathbf{z}}$	(12f)	O III
$\mathbf{B}_{34} =$	$(z_6 + \frac{1}{2}) \mathbf{a}_1 + (y_6 + \frac{1}{2}) \mathbf{a}_2 + (x_6 + \frac{1}{2}) \mathbf{a}_3$	$=$	$-\frac{1}{2} a (x_6 - z_6) \hat{\mathbf{x}} - \frac{\sqrt{3}}{6} a (x_6 - 2y_6 + z_6) \hat{\mathbf{y}} + \frac{1}{6} c (2x_6 + 2y_6 + 2z_6 + 3) \hat{\mathbf{z}}$	(12f)	O III
$\mathbf{B}_{35} =$	$(y_6 + \frac{1}{2}) \mathbf{a}_1 + (x_6 + \frac{1}{2}) \mathbf{a}_2 + (z_6 + \frac{1}{2}) \mathbf{a}_3$	$=$	$\frac{1}{2} a (y_6 - z_6) \hat{\mathbf{x}} + \frac{\sqrt{3}}{6} a (2x_6 - y_6 - z_6) \hat{\mathbf{y}} + \frac{1}{6} c (2x_6 + 2y_6 + 2z_6 + 3) \hat{\mathbf{z}}$	(12f)	O III
$\mathbf{B}_{36} =$	$(x_6 + \frac{1}{2}) \mathbf{a}_1 + (z_6 + \frac{1}{2}) \mathbf{a}_2 + (y_6 + \frac{1}{2}) \mathbf{a}_3$	$=$	$\frac{1}{2} a (x_6 - y_6) \hat{\mathbf{x}} - \frac{\sqrt{3}}{6} a (x_6 + y_6 - 2z_6) \hat{\mathbf{y}} + \frac{1}{6} c (2x_6 + 2y_6 + 2z_6 + 3) \hat{\mathbf{z}}$	(12f)	O III

References

- [1] N. King, R. D. Sommer, P. Watkins-Curry, J. Y. Chan, and P. A. Maggard, *Synthesis, Structure, and Thermal Instability of the $\text{Cu}_2\text{Ta}_4\text{O}_{11}$ Phase*, *Crystal Growth & Design* **15**, 552–558 (2015), doi:10.1021/cg500987c.

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