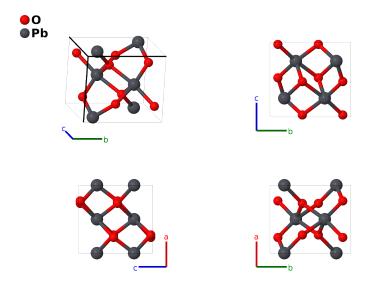
α -PbO₂ Structure: A2B_oP12_60_d_c-003

This structure originally had the label A2B_oP12_60_d_c. Calls to that address will be redirected here.

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https://aflow.org/p/9BKR

 $https://aflow.org/p/A2B_oP12_60_d_c-003$



Prototype O_2Pb

AFLOW prototype label A2B_oP12_60_d_c-003

ICSD 32691
Pearson symbol oP12
Space group number 60

Space group symbol Pbcn

AFLOW prototype command aflow --proto=A2B_oP12_60_d_c-003 --params= $a, b/a, c/a, y_1, x_2, y_2, z_2$

Other compounds with this structure

(Ti, Zr)O₂ (srilankite)

- (Hill, 1982) states the Pb site is only 49% occupied, so stoichiometrically this compound is closer to PbO₄. On the other hand, the ICSD entry gives lists 98% occupation, which is in better agreement with the claimed stoichiometry.
- This structure has the same AFLOW label as ζ-Fe₂N, but in that case the nitrogen site is fully occupied. The structures are generated by the same symmetry operations with different sets of parameters (--params) specified in their corresponding CIF files.

Simple Orthorhombic primitive vectors



$$\mathbf{a_1} = a\,\hat{\mathbf{x}}$$

$$\mathbf{a_2} = b\,\hat{\mathbf{y}}$$

$$\mathbf{a_3} = c \, \hat{\mathbf{z}}$$



Basis vectors

		Lattice coordinates		Cartesian coordinates	Wyckoff position	$\begin{array}{c} \text{Atom} \\ \text{type} \end{array}$
$\mathbf{B_1}$	=	$y_1{f a}_2+rac{1}{4}{f a}_3$	=	$by_1\mathbf{\hat{y}} + frac{1}{4}c\mathbf{\hat{z}}$	(4c)	Pb I
$\mathbf{B_2}$	=	$\frac{1}{2}\mathbf{a}_1 - \left(y_1 - \frac{1}{2}\right)\mathbf{a}_2 + \frac{3}{4}\mathbf{a}_3$	=	$\frac{1}{2}a\hat{\mathbf{x}} - b\left(y_1 - \frac{1}{2}\right)\hat{\mathbf{y}} + \frac{3}{4}c\hat{\mathbf{z}}$	(4c)	Pb I
$\mathbf{B_3}$	=	$-y_1{f a}_2+rac{3}{4}{f a}_3$	=	$-by_1\mathbf{\hat{y}}+rac{3}{4}c\mathbf{\hat{z}}$	(4c)	Pb I
$\mathbf{B_4}$	=	$\frac{1}{2}\mathbf{a}_1 + \left(y_1 + \frac{1}{2}\right)\mathbf{a}_2 + \frac{1}{4}\mathbf{a}_3$	=	$\frac{1}{2}a\hat{\mathbf{x}} + b\left(y_1 + \frac{1}{2}\right)\hat{\mathbf{y}} + \frac{1}{4}c\hat{\mathbf{z}}$	(4c)	Pb I
${f B_5}$	=	$x_2 \mathbf{a}_1 + y_2 \mathbf{a}_2 + z_2 \mathbf{a}_3$	=	$ax_2\mathbf{\hat{x}} + by_2\mathbf{\hat{y}} + cz_2\mathbf{\hat{z}}$	(8d)	ΟI
${f B_6}$	=	$-\left(x_2-\frac{1}{2}\right) \mathbf{a}_1 - \left(y_2-\frac{1}{2}\right) \mathbf{a}_2 +$	=	$-a\left(x_{2}-\frac{1}{2}\right) \hat{\mathbf{x}}-b\left(y_{2}-\frac{1}{2}\right) \hat{\mathbf{y}}+c\left(z_{2}+\frac{1}{2}\right) \hat{\mathbf{z}}$	(8d)	ΟI
		$\left(z_2+rac{1}{2} ight){f a}_3$				
$\mathbf{B_7}$	=	$-x_2\mathbf{a}_1 + y_2\mathbf{a}_2 - \left(z_2 - \frac{1}{2}\right)\mathbf{a}_3$	=	$-ax_2\mathbf{\hat{x}} + by_2\mathbf{\hat{y}} - c\left(z_2 - \frac{1}{2}\right)\mathbf{\hat{z}}$	(8d)	ΟI
${f B_8}$	=	$\left(x_2 + \frac{1}{2}\right) \mathbf{a}_1 - \left(y_2 - \frac{1}{2}\right) \mathbf{a}_2 - z_2 \mathbf{a}_3$	=	$a\left(x_{2}+\frac{1}{2}\right) \hat{\mathbf{x}}-b\left(y_{2}-\frac{1}{2}\right) \hat{\mathbf{y}}-cz_{2}\hat{\mathbf{z}}$	(8d)	ΟI
$\mathbf{B_9}$	=	$-x_2\mathbf{a}_1-y_2\mathbf{a}_2-z_2\mathbf{a}_3$	=	$-ax_2\mathbf{\hat{x}} - by_2\mathbf{\hat{y}} - cz_2\mathbf{\hat{z}}$	(8d)	ΟI
${f B_{10}}$	=	$(x_2 + \frac{1}{2}) \mathbf{a}_1 + (y_2 + \frac{1}{2}) \mathbf{a}_2 -$	=	$a\left(x_{2}+\frac{1}{2}\right) \hat{\mathbf{x}}+b\left(y_{2}+\frac{1}{2}\right) \hat{\mathbf{y}}-c\left(z_{2}-\frac{1}{2}\right) \hat{\mathbf{z}}$	(8d)	ΟI
		$\left(z_2-rac{1}{2} ight){f a}_3$				
$\mathbf{B_{11}}$	=	$x_2 \mathbf{a}_1 - y_2 \mathbf{a}_2 + \left(z_2 + \frac{1}{2}\right) \mathbf{a}_3$	=	$ax_2 \hat{\mathbf{x}} - by_2 \hat{\mathbf{y}} + c \left(z_2 + \frac{1}{2} \right) \hat{\mathbf{z}}$	(8d)	ΟI
$\mathbf{B_{12}}$	=	$-\left(x_2-\frac{1}{2}\right) \mathbf{a}_1+\left(y_2+\frac{1}{2}\right) \mathbf{a}_2+$	=	$-a\left(x_2-\frac{1}{2}\right)\hat{\mathbf{x}}+b\left(y_2+\frac{1}{2}\right)\hat{\mathbf{y}}+cz_2\hat{\mathbf{z}}$	(8d)	ΟI
		$z_2{f a}_3$				

References

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