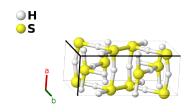
H₂S (170 GPa) Structure: A2B_oC24_64_2f_f-001

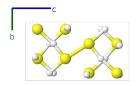
This structure originally had the label A2B_oC24_64_2f_f. Calls to that address will be redirected here.

Cite this page as: D. Hicks, M. J. Mehl, E. Gossett, C. Toher, O. Levy, R. M. Hanson, G. Hart, and S. Curtarolo, *The AFLOW Library of Crystallographic Prototypes: Part 2*, Comput. Mater. Sci. **161**, S1 (2019). doi: 10.1016/j.commatsci.2018.10.043

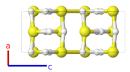
https://aflow.org/p/7FZR

https://aflow.org/p/A2B_oC24_64_2f_f-001









Prototype H_2S

AFLOW prototype label A2B_oC24_64_2f_f-001

ICSD none
Pearson symbol oC24
Space group number 64

Space group symbol Cmce

AFLOW prototype command aflow --proto=A2B_oC24_64_2f_f-001

--params= $a, b/a, c/a, y_1, z_1, y_2, z_2, y_3, z_3$

- This structure was found by first-principles electronic structure calculations and is predicted to be the stable structure of H_2S for pressures > 140 GPa. At 160 GPa it is predicted to be a conventional superconductor with an approximate transition temperature of 80K, however it is unlikely that this is the crystal structure of the 190K superconductor, which is probably the H_3S structure (Bernstein, 2005).
- The data presented here was computed at 170 GPa.

Base-centered Orthorhombic primitive vectors



$$\mathbf{a_1} = \frac{1}{2}a\,\hat{\mathbf{x}} - \frac{1}{2}b\,\hat{\mathbf{y}}$$

$$\mathbf{a_2} = \frac{1}{2}a\,\hat{\mathbf{x}} + \frac{1}{2}b\,\hat{\mathbf{y}}$$

$$\mathbf{a_3} = c\,\hat{\mathbf{z}}$$



Basis vectors

		Lattice coordinates		Cartesian coordinates	Wyckoff position	Atom type
${\bf B_1}$	=	$-y_1\mathbf{a}_1 + y_1\mathbf{a}_2 + z_1\mathbf{a}_3$	=	$by_1\hat{\mathbf{y}}+cz_1\hat{\mathbf{z}}$	(8f)	ΗΙ
$\mathbf{B_2}$	=	$\left(y_1 + \frac{1}{2}\right) \mathbf{a}_1 - \left(y_1 - \frac{1}{2}\right) \mathbf{a}_2 + \left(z_1 + \frac{1}{2}\right) \mathbf{a}_3$	=	$\frac{1}{2}a\hat{\mathbf{x}} - by_1\hat{\mathbf{y}} + c\left(z_1 + \frac{1}{2}\right)\hat{\mathbf{z}}$	(8f)	ΗΙ
B_3	=	$-\left(y_{1}-\frac{1}{2}\right) \mathbf{a}_{1}+\left(y_{1}+\frac{1}{2}\right) \mathbf{a}_{2}-\left(z_{1}-\frac{1}{2}\right) \mathbf{a}_{3}$	=	$\frac{1}{2}a\hat{\mathbf{x}} + by_1\hat{\mathbf{y}} - c\left(z_1 - \frac{1}{2}\right)\hat{\mathbf{z}}$	(8f)	ΗΙ
${f B_4}$	=	$y_1 \mathbf{a}_1 - y_1 \mathbf{a}_2 - z_1 \mathbf{a}_3$	=	$-by_1\mathbf{\hat{y}}-cz_1\mathbf{\hat{z}}$	(8f)	ΗΙ
${f B_5}$	=	$-y_2\mathbf{a}_1+y_2\mathbf{a}_2+z_2\mathbf{a}_3$	=	$by_2\mathbf{\hat{y}}+cz_2\mathbf{\hat{z}}$	(8f)	ΗII
B_{6}	=	$\left(y_2 + \frac{1}{2}\right) \mathbf{a}_1 - \left(y_2 - \frac{1}{2}\right) \mathbf{a}_2 + \left(z_2 + \frac{1}{2}\right) \mathbf{a}_3$	=	$\frac{1}{2}a\hat{\mathbf{x}} - by_2\hat{\mathbf{y}} + c\left(z_2 + \frac{1}{2}\right)\hat{\mathbf{z}}$	(8f)	ΗII
B_7	=	$-\left(y_2 - \frac{1}{2}\right) \mathbf{a}_1 + \left(y_2 + \frac{1}{2}\right) \mathbf{a}_2 - \left(z_2 - \frac{1}{2}\right) \mathbf{a}_3$	=	$\frac{1}{2}a\hat{\mathbf{x}} + by_2\hat{\mathbf{y}} - c\left(z_2 - \frac{1}{2}\right)\hat{\mathbf{z}}$	(8f)	H II
B_8	=	$y_2\mathbf{a}_1 - y_2\mathbf{a}_2 - z_2\mathbf{a}_3$	=	$-by_2\mathbf{\hat{y}}-cz_2\mathbf{\hat{z}}$	(8f)	ΗII
B_9	=	$-y_3\mathbf{a}_1+y_3\mathbf{a}_2+z_3\mathbf{a}_3$	=	$by_3\mathbf{\hat{y}}+cz_3\mathbf{\hat{z}}$	(8f)	SI
B_{10}	=	$\left(y_3 + \frac{1}{2}\right) \mathbf{a}_1 - \left(y_3 - \frac{1}{2}\right) \mathbf{a}_2 + \left(z_3 + \frac{1}{2}\right) \mathbf{a}_3$	=	$\frac{1}{2}a\hat{\mathbf{x}} - by_3\hat{\mathbf{y}} + c\left(z_3 + \frac{1}{2}\right)\hat{\mathbf{z}}$	(8f)	SI
B_{11}	=	$-\left(y_3 - \frac{1}{2}\right) \mathbf{a}_1 + \left(y_3 + \frac{1}{2}\right) \mathbf{a}_2 - \left(z_3 - \frac{1}{2}\right) \mathbf{a}_3$	=	$\frac{1}{2}a\hat{\mathbf{x}} + by_3\hat{\mathbf{y}} - c\left(z_3 - \frac{1}{2}\right)\hat{\mathbf{z}}$	(8f)	SI
$\mathbf{B_{12}}$	=	$y_3 \mathbf{a}_1 - y_3 \mathbf{a}_2 - z_3 \mathbf{a}_3$	=	$-by_3\mathbf{\hat{y}}-cz_3\mathbf{\hat{z}}$	(8f)	SI

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