

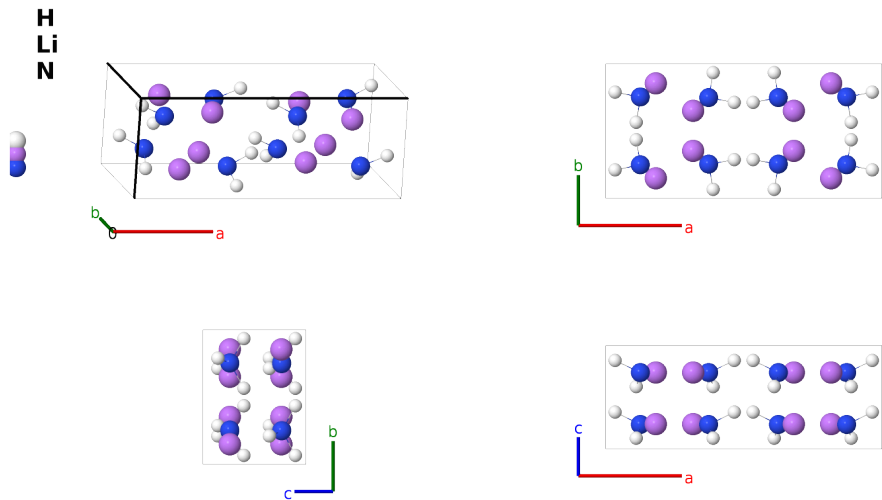
β -LiNH₂ (*Iba*2) Structure: A2BC_oI32_45_2c_c_c-001

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<https://aflow.org/prototype-encyclopedia/ZBD3>

https://aflow.org/prototype-encyclopedia/A2BC_oI32_45_2c_c_c-001

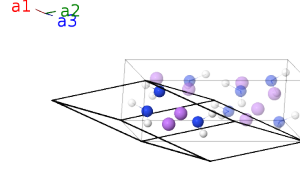


Prototype	H ₂ LiN
AFLOW prototype label	A2BC_oI32_45_2c_c_c-001
ICSD	116487
CCDC	2273728
Pearson symbol	oI32
Space group number	45
Space group symbol	<i>Iba</i> 2
AFLOW prototype command	<code>aflow --proto=A2BC_oI32_45_2c_c_c-001</code> <code>--params=a, b/a, c/a, x₁, y₁, z₁, x₂, y₂, z₂, x₃, y₃, z₃, x₄, y₄, z₄</code>

- Under pressure LiNH₂ has at least three phases (Yamawaki, 2014): tetragonal α -LiNiH₂, or Phase I, the ground state, stable up to 10GPa.
- Monoclinic Phase II, stable between 10 and 13 GPa.
- β -LiNH₂, or Phase III, is stable above 13 GPa. The structure is very uncertain. (Yamawaki, 2014) discuss two possible structures: orthorhombic space group *Pccn* #56 and body-centered orthorhombic space group *Iba*2 #45 (this structure).

Body-centered Orthorhombic primitive vectors

$$\begin{aligned}\mathbf{a}_1 &= -\frac{1}{2}a \hat{\mathbf{x}} + \frac{1}{2}b \hat{\mathbf{y}} + \frac{1}{2}c \hat{\mathbf{z}} \\ \mathbf{a}_2 &= \frac{1}{2}a \hat{\mathbf{x}} - \frac{1}{2}b \hat{\mathbf{y}} + \frac{1}{2}c \hat{\mathbf{z}} \\ \mathbf{a}_3 &= \frac{1}{2}a \hat{\mathbf{x}} + \frac{1}{2}b \hat{\mathbf{y}} - \frac{1}{2}c \hat{\mathbf{z}}\end{aligned}$$



Basis vectors

	Lattice coordinates		Cartesian coordinates	Wyckoff position	Atom type
$\mathbf{B}_1$	$= (y_1 + z_1) \mathbf{a}_1 + (x_1 + z_1) \mathbf{a}_2 + (x_1 + y_1) \mathbf{a}_3$	$=$	$ax_1 \hat{\mathbf{x}} + by_1 \hat{\mathbf{y}} + cz_1 \hat{\mathbf{z}}$	(8c)	H I
$\mathbf{B}_2$	$= -(y_1 - z_1) \mathbf{a}_1 - (x_1 - z_1) \mathbf{a}_2 - (x_1 + y_1) \mathbf{a}_3$	$=$	$-ax_1 \hat{\mathbf{x}} - by_1 \hat{\mathbf{y}} + cz_1 \hat{\mathbf{z}}$	(8c)	H I
$\mathbf{B}_3$	$= (-y_1 + z_1 + \frac{1}{2}) \mathbf{a}_1 + (x_1 + z_1 + \frac{1}{2}) \mathbf{a}_2 + (x_1 - y_1) \mathbf{a}_3$	$=$	$ax_1 \hat{\mathbf{x}} - by_1 \hat{\mathbf{y}} + c(z_1 + \frac{1}{2}) \hat{\mathbf{z}}$	(8c)	H I
$\mathbf{B}_4$	$= (y_1 + z_1 + \frac{1}{2}) \mathbf{a}_1 + (-x_1 + z_1 + \frac{1}{2}) \mathbf{a}_2 - (x_1 - y_1) \mathbf{a}_3$	$=$	$-ax_1 \hat{\mathbf{x}} + by_1 \hat{\mathbf{y}} + c(z_1 + \frac{1}{2}) \hat{\mathbf{z}}$	(8c)	H I
$\mathbf{B}_5$	$= (y_2 + z_2) \mathbf{a}_1 + (x_2 + z_2) \mathbf{a}_2 + (x_2 + y_2) \mathbf{a}_3$	$=$	$ax_2 \hat{\mathbf{x}} + by_2 \hat{\mathbf{y}} + cz_2 \hat{\mathbf{z}}$	(8c)	H II
$\mathbf{B}_6$	$= -(y_2 - z_2) \mathbf{a}_1 - (x_2 - z_2) \mathbf{a}_2 - (x_2 + y_2) \mathbf{a}_3$	$=$	$-ax_2 \hat{\mathbf{x}} - by_2 \hat{\mathbf{y}} + cz_2 \hat{\mathbf{z}}$	(8c)	H II
$\mathbf{B}_7$	$= (-y_2 + z_2 + \frac{1}{2}) \mathbf{a}_1 + (x_2 + z_2 + \frac{1}{2}) \mathbf{a}_2 + (x_2 - y_2) \mathbf{a}_3$	$=$	$ax_2 \hat{\mathbf{x}} - by_2 \hat{\mathbf{y}} + c(z_2 + \frac{1}{2}) \hat{\mathbf{z}}$	(8c)	H II
$\mathbf{B}_8$	$= (y_2 + z_2 + \frac{1}{2}) \mathbf{a}_1 + (-x_2 + z_2 + \frac{1}{2}) \mathbf{a}_2 - (x_2 - y_2) \mathbf{a}_3$	$=$	$-ax_2 \hat{\mathbf{x}} + by_2 \hat{\mathbf{y}} + c(z_2 + \frac{1}{2}) \hat{\mathbf{z}}$	(8c)	H II
$\mathbf{B}_9$	$= (y_3 + z_3) \mathbf{a}_1 + (x_3 + z_3) \mathbf{a}_2 + (x_3 + y_3) \mathbf{a}_3$	$=$	$ax_3 \hat{\mathbf{x}} + by_3 \hat{\mathbf{y}} + cz_3 \hat{\mathbf{z}}$	(8c)	Li I
$\mathbf{B}_{10}$	$= -(y_3 - z_3) \mathbf{a}_1 - (x_3 - z_3) \mathbf{a}_2 - (x_3 + y_3) \mathbf{a}_3$	$=$	$-ax_3 \hat{\mathbf{x}} - by_3 \hat{\mathbf{y}} + cz_3 \hat{\mathbf{z}}$	(8c)	Li I
$\mathbf{B}_{11}$	$= (-y_3 + z_3 + \frac{1}{2}) \mathbf{a}_1 + (x_3 + z_3 + \frac{1}{2}) \mathbf{a}_2 + (x_3 - y_3) \mathbf{a}_3$	$=$	$ax_3 \hat{\mathbf{x}} - by_3 \hat{\mathbf{y}} + c(z_3 + \frac{1}{2}) \hat{\mathbf{z}}$	(8c)	Li I
$\mathbf{B}_{12}$	$= (y_3 + z_3 + \frac{1}{2}) \mathbf{a}_1 + (-x_3 + z_3 + \frac{1}{2}) \mathbf{a}_2 - (x_3 - y_3) \mathbf{a}_3$	$=$	$-ax_3 \hat{\mathbf{x}} + by_3 \hat{\mathbf{y}} + c(z_3 + \frac{1}{2}) \hat{\mathbf{z}}$	(8c)	Li I
$\mathbf{B}_{13}$	$= (y_4 + z_4) \mathbf{a}_1 + (x_4 + z_4) \mathbf{a}_2 + (x_4 + y_4) \mathbf{a}_3$	$=$	$ax_4 \hat{\mathbf{x}} + by_4 \hat{\mathbf{y}} + cz_4 \hat{\mathbf{z}}$	(8c)	N I
$\mathbf{B}_{14}$	$= -(y_4 - z_4) \mathbf{a}_1 - (x_4 - z_4) \mathbf{a}_2 - (x_4 + y_4) \mathbf{a}_3$	$=$	$-ax_4 \hat{\mathbf{x}} - by_4 \hat{\mathbf{y}} + cz_4 \hat{\mathbf{z}}$	(8c)	N I
$\mathbf{B}_{15}$	$= (-y_4 + z_4 + \frac{1}{2}) \mathbf{a}_1 + (x_4 + z_4 + \frac{1}{2}) \mathbf{a}_2 + (x_4 - y_4) \mathbf{a}_3$	$=$	$ax_4 \hat{\mathbf{x}} - by_4 \hat{\mathbf{y}} + c(z_4 + \frac{1}{2}) \hat{\mathbf{z}}$	(8c)	N I
$\mathbf{B}_{16}$	$= (y_4 + z_4 + \frac{1}{2}) \mathbf{a}_1 + (-x_4 + z_4 + \frac{1}{2}) \mathbf{a}_2 - (x_4 - y_4) \mathbf{a}_3$	$=$	$-ax_4 \hat{\mathbf{x}} + by_4 \hat{\mathbf{y}} + c(z_4 + \frac{1}{2}) \hat{\mathbf{z}}$	(8c)	N I

References

- [1] H. Yamawaki, H. Fujihisa, Y. Gotoh, and S. Nakano, *Structure of Intermediate Phase II of LiNH_2 under High Pressure*, J. Phys. Chem. B **118**, 9991–9996 (2014), doi:10.1021/jp505133q.

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