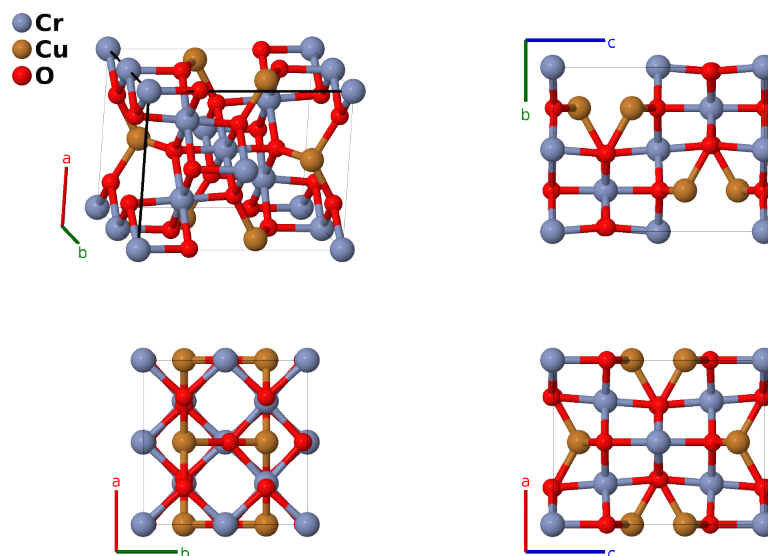


CuCr₂O₄ Structure: A2BC4_tI28_141_c_b_h-001

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<https://aflow.org/p/763J>

https://aflow.org/p/A2BC4_tI28_141_c_b_h-001



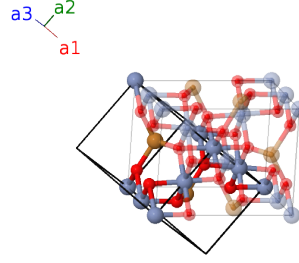
Prototype	Cr ₂ CuO ₄
AFLOW prototype label	A2BC4_tI28_141_c_b_h-001
ICSD	84378
Pearson symbol	tI28
Space group number	141
Space group symbol	<i>I</i> 4 ₁ / <i>amd</i>
AFLOW prototype command	<code>aflow --proto=A2BC4_tI28_141_c_b_h-001 --params=a, c/a, y₃, z₃</code>

Other compounds with this structure

CdMn₂O₄, CoMn₂O₄, CuMn₂O₄, FeCr₂S₄, GeCo₂O₄, MgMn₂O₄, NiCr₂O₄, ZnMn₂O₄

- This is a tetragonal distortion of the spinel (*H*1₁) structure.

Body-centered Tetragonal primitive vectors



$$\begin{aligned}\mathbf{a}_1 &= -\frac{1}{2}a\hat{\mathbf{x}} + \frac{1}{2}a\hat{\mathbf{y}} + \frac{1}{2}c\hat{\mathbf{z}} \\ \mathbf{a}_2 &= \frac{1}{2}a\hat{\mathbf{x}} - \frac{1}{2}a\hat{\mathbf{y}} + \frac{1}{2}c\hat{\mathbf{z}} \\ \mathbf{a}_3 &= \frac{1}{2}a\hat{\mathbf{x}} + \frac{1}{2}a\hat{\mathbf{y}} - \frac{1}{2}c\hat{\mathbf{z}}\end{aligned}$$

Basis vectors

	Lattice coordinates		Cartesian coordinates	Wyckoff position	Atom type
\mathbf{B}_1	$= \frac{5}{8}\mathbf{a}_1 + \frac{3}{8}\mathbf{a}_2 + \frac{1}{4}\mathbf{a}_3$	$=$	$\frac{1}{4}a\hat{\mathbf{y}} + \frac{3}{8}c\hat{\mathbf{z}}$	(4b)	Cu I
\mathbf{B}_2	$= \frac{3}{8}\mathbf{a}_1 + \frac{5}{8}\mathbf{a}_2 + \frac{3}{4}\mathbf{a}_3$	$=$	$\frac{1}{2}a\hat{\mathbf{x}} + \frac{1}{4}a\hat{\mathbf{y}} + \frac{1}{8}c\hat{\mathbf{z}}$	(4b)	Cu I
\mathbf{B}_3	$= 0$	$=$	0	(8c)	Cr I
\mathbf{B}_4	$= \frac{1}{2}\mathbf{a}_1 + \frac{1}{2}\mathbf{a}_3$	$=$	$\frac{1}{2}a\hat{\mathbf{y}}$	(8c)	Cr I
\mathbf{B}_5	$= \frac{1}{2}\mathbf{a}_2$	$=$	$\frac{1}{4}a\hat{\mathbf{x}} - \frac{1}{4}a\hat{\mathbf{y}} + \frac{1}{4}c\hat{\mathbf{z}}$	(8c)	Cr I
\mathbf{B}_6	$= \frac{1}{2}\mathbf{a}_3$	$=$	$\frac{1}{4}a\hat{\mathbf{x}} + \frac{1}{4}a\hat{\mathbf{y}} - \frac{1}{4}c\hat{\mathbf{z}}$	(8c)	Cr I
\mathbf{B}_7	$= (y_3 + z_3)\mathbf{a}_1 + z_3\mathbf{a}_2 + y_3\mathbf{a}_3$	$=$	$ay_3\hat{\mathbf{y}} + cz_3\hat{\mathbf{z}}$	(16h)	O I
\mathbf{B}_8	$= (-y_3 + z_3 + \frac{1}{2})\mathbf{a}_1 + z_3\mathbf{a}_2 - (y_3 - \frac{1}{2})\mathbf{a}_3$	$=$	$-a(y_3 - \frac{1}{2})\hat{\mathbf{y}} + cz_3\hat{\mathbf{z}}$	(16h)	O I
\mathbf{B}_9	$= z_3\mathbf{a}_1 + (-y_3 + z_3 + \frac{1}{2})\mathbf{a}_2 - y_3\mathbf{a}_3$	$=$	$-a(y_3 - \frac{1}{4})\hat{\mathbf{x}} - \frac{1}{4}a\hat{\mathbf{y}} + c(z_3 + \frac{1}{4})\hat{\mathbf{z}}$	(16h)	O I
\mathbf{B}_{10}	$= z_3\mathbf{a}_1 + (y_3 + z_3)\mathbf{a}_2 + (y_3 + \frac{1}{2})\mathbf{a}_3$	$=$	$a(y_3 + \frac{1}{4})\hat{\mathbf{x}} + \frac{1}{4}a\hat{\mathbf{y}} + c(z_3 - \frac{1}{4})\hat{\mathbf{z}}$	(16h)	O I
\mathbf{B}_{11}	$= (y_3 - z_3 + \frac{1}{2})\mathbf{a}_1 - z_3\mathbf{a}_2 + (y_3 + \frac{1}{2})\mathbf{a}_3$	$=$	$a(y_3 + \frac{1}{2})\hat{\mathbf{y}} - cz_3\hat{\mathbf{z}}$	(16h)	O I
\mathbf{B}_{12}	$= -(y_3 + z_3)\mathbf{a}_1 - z_3\mathbf{a}_2 - y_3\mathbf{a}_3$	$=$	$-ay_3\hat{\mathbf{y}} - cz_3\hat{\mathbf{z}}$	(16h)	O I
\mathbf{B}_{13}	$= -z_3\mathbf{a}_1 + (y_3 - z_3 + \frac{1}{2})\mathbf{a}_2 + y_3\mathbf{a}_3$	$=$	$a(y_3 + \frac{1}{4})\hat{\mathbf{x}} - \frac{1}{4}a\hat{\mathbf{y}} - c(z_3 - \frac{1}{4})\hat{\mathbf{z}}$	(16h)	O I
\mathbf{B}_{14}	$= -z_3\mathbf{a}_1 - (y_3 + z_3)\mathbf{a}_2 - (y_3 - \frac{1}{2})\mathbf{a}_3$	$=$	$-a(y_3 - \frac{1}{4})\hat{\mathbf{x}} + \frac{1}{4}a\hat{\mathbf{y}} - c(z_3 + \frac{1}{4})\hat{\mathbf{z}}$	(16h)	O I

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