

# Rb<sub>2</sub>C<sub>2</sub>O<sub>4</sub>·H<sub>2</sub>O Structure:

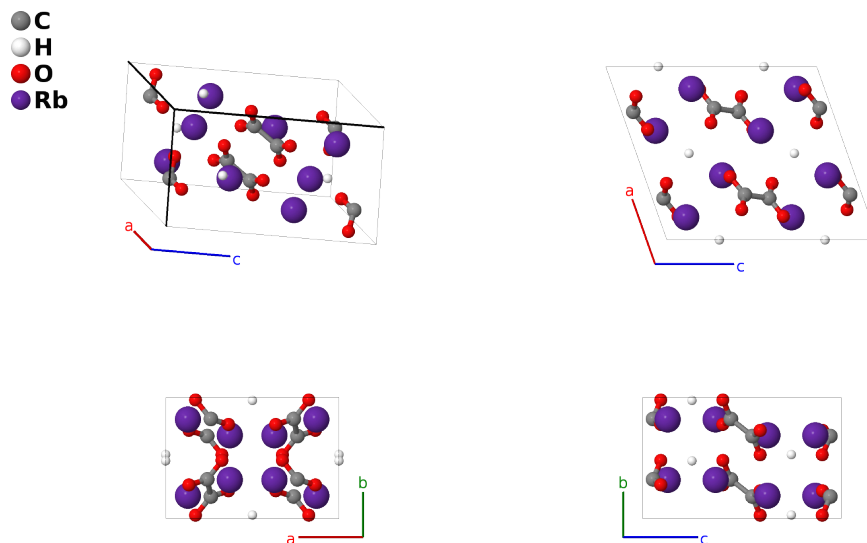
## A2BC4D2\_mC36\_15\_f\_e\_2f\_f-001

This structure originally had the label A2BC4D2\_mC36\_15\_f\_e\_2f\_f. Calls to that address will be redirected here.

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<https://aflow.org/p/RBDM>

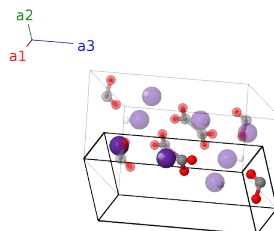
[https://aflow.org/p/A2BC4D2\\_mC36\\_15\\_f\\_e\\_2f\\_f-001](https://aflow.org/p/A2BC4D2_mC36_15_f_e_2f_f-001)



|                         |   |
|-------------------------|---|
| Prototype               | C <sub>2</sub> H <sub>2</sub> O <sub>5</sub> Rb <sub>2</sub>  |
| AFLOW prototype label   | A2BC4D2_mC36_15_f_e_2f_f-001  |
| CCDC                    | 1247457   |
| Pearson symbol          | mC36  |
| Space group number      | 15  |
| Space group symbol      | C2/c  |
| AFLOW prototype command | aflow --proto=A2BC4D2_mC36_15_f_e_2f_f-001<br>--params=a, b/a, c/a, β, y <sub>1</sub> , x <sub>2</sub> , y <sub>2</sub> , z <sub>2</sub> , x <sub>3</sub> , y <sub>3</sub> , z <sub>3</sub> , x <sub>4</sub> , y <sub>4</sub> , z <sub>4</sub> , x <sub>5</sub> , y <sub>5</sub> , z <sub>5</sub> |

### Base-centered Monoclinic primitive vectors

$$\begin{aligned} \mathbf{a}_1 &= \frac{1}{2}a \hat{\mathbf{x}} - \frac{1}{2}b \hat{\mathbf{y}} \\ \mathbf{a}_2 &= \frac{1}{2}a \hat{\mathbf{x}} + \frac{1}{2}b \hat{\mathbf{y}} \\ \mathbf{a}_3 &= c \cos \beta \hat{\mathbf{x}} + c \sin \beta \hat{\mathbf{z}} \end{aligned}$$



## Basis vectors

|                   | Lattice<br>coordinates  |     | Cartesian<br>coordinates  | Wyckoff<br>position | Atom<br>type |
|-------------------|---|-----|---|---------------------|--------------|
| $\mathbf{B}_1$    | $= -y_1 \mathbf{a}_1 + y_1 \mathbf{a}_2 + \frac{1}{4} \mathbf{a}_3$                         | $=$ | $\frac{1}{4}c \cos \beta \hat{\mathbf{x}} + by_1 \hat{\mathbf{y}} + \frac{1}{4}c \sin \beta \hat{\mathbf{z}}$                           | (4e)                | H I          |
| $\mathbf{B}_2$    | $= y_1 \mathbf{a}_1 - y_1 \mathbf{a}_2 + \frac{3}{4} \mathbf{a}_3$                          | $=$ | $\frac{3}{4}c \cos \beta \hat{\mathbf{x}} - by_1 \hat{\mathbf{y}} + \frac{3}{4}c \sin \beta \hat{\mathbf{z}}$                           | (4e)                | H I          |
| $\mathbf{B}_3$    | $= (x_2 - y_2) \mathbf{a}_1 + (x_2 + y_2) \mathbf{a}_2 + z_2 \mathbf{a}_3$                  | $=$ | $(ax_2 + cz_2 \cos \beta) \hat{\mathbf{x}} + by_2 \hat{\mathbf{y}} + cz_2 \sin \beta \hat{\mathbf{z}}$                                  | (8f)                | C I          |
| $\mathbf{B}_4$    | $= -(x_2 + y_2) \mathbf{a}_1 - (x_2 - y_2) \mathbf{a}_2 - (z_2 - \frac{1}{2}) \mathbf{a}_3$ | $=$ | $-(ax_2 + c(z_2 - \frac{1}{2}) \cos \beta) \hat{\mathbf{x}} + by_2 \hat{\mathbf{y}} - c(z_2 - \frac{1}{2}) \sin \beta \hat{\mathbf{z}}$ | (8f)                | C I          |
| $\mathbf{B}_5$    | $= -(x_2 - y_2) \mathbf{a}_1 - (x_2 + y_2) \mathbf{a}_2 - z_2 \mathbf{a}_3$                 | $=$ | $-(ax_2 + cz_2 \cos \beta) \hat{\mathbf{x}} - by_2 \hat{\mathbf{y}} - cz_2 \sin \beta \hat{\mathbf{z}}$                                 | (8f)                | C I          |
| $\mathbf{B}_6$    | $= (x_2 + y_2) \mathbf{a}_1 + (x_2 - y_2) \mathbf{a}_2 + (z_2 + \frac{1}{2}) \mathbf{a}_3$  | $=$ | $(ax_2 + c(z_2 + \frac{1}{2}) \cos \beta) \hat{\mathbf{x}} - by_2 \hat{\mathbf{y}} + c(z_2 + \frac{1}{2}) \sin \beta \hat{\mathbf{z}}$  | (8f)                | C I          |
| $\mathbf{B}_7$    | $= (x_3 - y_3) \mathbf{a}_1 + (x_3 + y_3) \mathbf{a}_2 + z_3 \mathbf{a}_3$                  | $=$ | $(ax_3 + cz_3 \cos \beta) \hat{\mathbf{x}} + by_3 \hat{\mathbf{y}} + cz_3 \sin \beta \hat{\mathbf{z}}$                                  | (8f)                | O I          |
| $\mathbf{B}_8$    | $= -(x_3 + y_3) \mathbf{a}_1 - (x_3 - y_3) \mathbf{a}_2 - (z_3 - \frac{1}{2}) \mathbf{a}_3$ | $=$ | $-(ax_3 + c(z_3 - \frac{1}{2}) \cos \beta) \hat{\mathbf{x}} + by_3 \hat{\mathbf{y}} - c(z_3 - \frac{1}{2}) \sin \beta \hat{\mathbf{z}}$ | (8f)                | O I          |
| $\mathbf{B}_9$    | $= -(x_3 - y_3) \mathbf{a}_1 - (x_3 + y_3) \mathbf{a}_2 - z_3 \mathbf{a}_3$                 | $=$ | $-(ax_3 + cz_3 \cos \beta) \hat{\mathbf{x}} - by_3 \hat{\mathbf{y}} - cz_3 \sin \beta \hat{\mathbf{z}}$                                 | (8f)                | O I          |
| $\mathbf{B}_{10}$ | $= (x_3 + y_3) \mathbf{a}_1 + (x_3 - y_3) \mathbf{a}_2 + (z_3 + \frac{1}{2}) \mathbf{a}_3$  | $=$ | $(ax_3 + c(z_3 + \frac{1}{2}) \cos \beta) \hat{\mathbf{x}} - by_3 \hat{\mathbf{y}} + c(z_3 + \frac{1}{2}) \sin \beta \hat{\mathbf{z}}$  | (8f)                | O I          |
| $\mathbf{B}_{11}$ | $= (x_4 - y_4) \mathbf{a}_1 + (x_4 + y_4) \mathbf{a}_2 + z_4 \mathbf{a}_3$                  | $=$ | $(ax_4 + cz_4 \cos \beta) \hat{\mathbf{x}} + by_4 \hat{\mathbf{y}} + cz_4 \sin \beta \hat{\mathbf{z}}$                                  | (8f)                | O II         |
| $\mathbf{B}_{12}$ | $= -(x_4 + y_4) \mathbf{a}_1 - (x_4 - y_4) \mathbf{a}_2 - (z_4 - \frac{1}{2}) \mathbf{a}_3$ | $=$ | $-(ax_4 + c(z_4 - \frac{1}{2}) \cos \beta) \hat{\mathbf{x}} + by_4 \hat{\mathbf{y}} - c(z_4 - \frac{1}{2}) \sin \beta \hat{\mathbf{z}}$ | (8f)                | O II         |
| $\mathbf{B}_{13}$ | $= -(x_4 - y_4) \mathbf{a}_1 - (x_4 + y_4) \mathbf{a}_2 - z_4 \mathbf{a}_3$                 | $=$ | $-(ax_4 + cz_4 \cos \beta) \hat{\mathbf{x}} - by_4 \hat{\mathbf{y}} - cz_4 \sin \beta \hat{\mathbf{z}}$                                 | (8f)                | O II         |
| $\mathbf{B}_{14}$ | $= (x_4 + y_4) \mathbf{a}_1 + (x_4 - y_4) \mathbf{a}_2 + (z_4 + \frac{1}{2}) \mathbf{a}_3$  | $=$ | $(ax_4 + c(z_4 + \frac{1}{2}) \cos \beta) \hat{\mathbf{x}} - by_4 \hat{\mathbf{y}} + c(z_4 + \frac{1}{2}) \sin \beta \hat{\mathbf{z}}$  | (8f)                | O II         |
| $\mathbf{B}_{15}$ | $= (x_5 - y_5) \mathbf{a}_1 + (x_5 + y_5) \mathbf{a}_2 + z_5 \mathbf{a}_3$                  | $=$ | $(ax_5 + cz_5 \cos \beta) \hat{\mathbf{x}} + by_5 \hat{\mathbf{y}} + cz_5 \sin \beta \hat{\mathbf{z}}$                                  | (8f)                | Rb I         |
| $\mathbf{B}_{16}$ | $= -(x_5 + y_5) \mathbf{a}_1 - (x_5 - y_5) \mathbf{a}_2 - (z_5 - \frac{1}{2}) \mathbf{a}_3$ | $=$ | $-(ax_5 + c(z_5 - \frac{1}{2}) \cos \beta) \hat{\mathbf{x}} + by_5 \hat{\mathbf{y}} - c(z_5 - \frac{1}{2}) \sin \beta \hat{\mathbf{z}}$ | (8f)                | Rb I         |
| $\mathbf{B}_{17}$ | $= -(x_5 - y_5) \mathbf{a}_1 - (x_5 + y_5) \mathbf{a}_2 - z_5 \mathbf{a}_3$                 | $=$ | $-(ax_5 + cz_5 \cos \beta) \hat{\mathbf{x}} - by_5 \hat{\mathbf{y}} - cz_5 \sin \beta \hat{\mathbf{z}}$                                 | (8f)                | Rb I         |
| $\mathbf{B}_{18}$ | $= (x_5 + y_5) \mathbf{a}_1 + (x_5 - y_5) \mathbf{a}_2 + (z_5 + \frac{1}{2}) \mathbf{a}_3$  | $=$ | $(ax_5 + c(z_5 + \frac{1}{2}) \cos \beta) \hat{\mathbf{x}} - by_5 \hat{\mathbf{y}} + c(z_5 + \frac{1}{2}) \sin \beta \hat{\mathbf{z}}$  | (8f)                | Rb I         |

## References

- [1] B. F. Pedersen, *The Crystal Structure of Rubidium. Oxalate Monohydrate,  $\text{Rb}_2\text{C}_2\text{O}_4 \cdot \text{H}_2\text{O}$* , Acta Chem. Scand. **19**, 1815–1818 (1965), doi:10.3891/acta.chem.scand.19-1815.