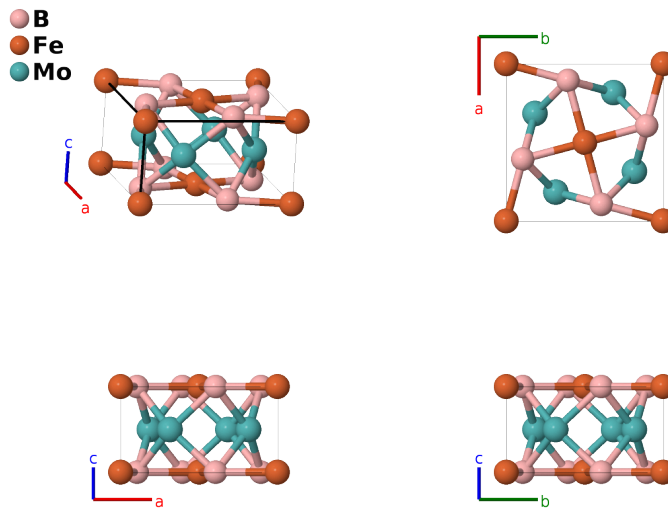


Mo₂FeB₂ Structure: A2BC2_tP10_127_g_a_h-002

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<https://aflow.org/p/5SWM>

https://aflow.org/p/A2BC2_tP10_127_g_a_h-002



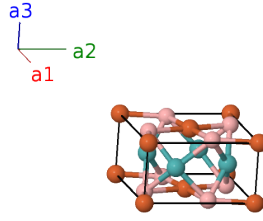
Prototype	B ₂ FeMo ₂
AFLOW prototype label	A2BC2_tP10_127_g_a_h-002
ICSD	5431
Pearson symbol	tP10
Space group number	127
Space group symbol	<i>P4/mbm</i>
AFLOW prototype command	<code>aflow --proto=A2BC2_tP10_127_g_a_h-002 --params=a,c/a,x₂,x₃</code>

Other compounds with this structure

Al₂CrB₂, Al₂FeB₂, Al₂NiB₂, Ce₂InPd₂, Dy₂CdPd₂, Dy₂InPd₂, Er₂CdPd₂, Er₂InPd₂, Gd₂CdPd₂, Gd₂InPd₂, Ho₂CdPd₂, Ho₂InNi₂, Ho₂InPd₂, La₂InCu₂, La₂InPd₂, Lu₂CdPd₂, Lu₂InPd₂, Mo₂CrB₂, Mo₂NiB₂, Nb₂FeB₂, Nd₂InPd₂, Ni₂SnZr₂, Pr₂CdPd₂, Pr₂InPd₂, Sm₂CdPd₂, Sm₂InPd₂, Ta₂FeB₂, Tb₂CdPd₂, Tb₂InPd₂, Th₂InPd₂, Ti₂CrB₂, Ti₂FeB₂, Ti₂NiB₂, Tm₂CdPd₂, Tm₂InCu₂, Tm₂InPd₂, U₂PbRh₂, Yb₂PbPt₂

- This is the ternary form of the Si₂U₃ (*D*5_a structure).

Simple Tetragonal primitive vectors



$$\begin{aligned}\mathbf{a}_1 &= a \hat{\mathbf{x}} \\ \mathbf{a}_2 &= a \hat{\mathbf{y}} \\ \mathbf{a}_3 &= c \hat{\mathbf{z}}\end{aligned}$$

Basis vectors

	Lattice coordinates		Cartesian coordinates	Wyckoff position	Atom type
\mathbf{B}_1	$= 0$	$=$	0	(2a)	Fe I
\mathbf{B}_2	$= \frac{1}{2} \mathbf{a}_1 + \frac{1}{2} \mathbf{a}_2$	$=$	$\frac{1}{2} a \hat{\mathbf{x}} + \frac{1}{2} a \hat{\mathbf{y}}$	(2a)	Fe I
\mathbf{B}_3	$= x_2 \mathbf{a}_1 + (x_2 + \frac{1}{2}) \mathbf{a}_2$	$=$	$ax_2 \hat{\mathbf{x}} + a(x_2 + \frac{1}{2}) \hat{\mathbf{y}}$	(4g)	B I
\mathbf{B}_4	$= -x_2 \mathbf{a}_1 - (x_2 - \frac{1}{2}) \mathbf{a}_2$	$=$	$-ax_2 \hat{\mathbf{x}} - a(x_2 - \frac{1}{2}) \hat{\mathbf{y}}$	(4g)	B I
\mathbf{B}_5	$= -(x_2 - \frac{1}{2}) \mathbf{a}_1 + x_2 \mathbf{a}_2$	$=$	$-a(x_2 - \frac{1}{2}) \hat{\mathbf{x}} + ax_2 \hat{\mathbf{y}}$	(4g)	B I
\mathbf{B}_6	$= (x_2 + \frac{1}{2}) \mathbf{a}_1 - x_2 \mathbf{a}_2$	$=$	$a(x_2 + \frac{1}{2}) \hat{\mathbf{x}} - ax_2 \hat{\mathbf{y}}$	(4g)	B I
\mathbf{B}_7	$= x_3 \mathbf{a}_1 + (x_3 + \frac{1}{2}) \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	$=$	$ax_3 \hat{\mathbf{x}} + a(x_3 + \frac{1}{2}) \hat{\mathbf{y}} + \frac{1}{2} c \hat{\mathbf{z}}$	(4h)	Mo I
\mathbf{B}_8	$= -x_3 \mathbf{a}_1 - (x_3 - \frac{1}{2}) \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	$=$	$-ax_3 \hat{\mathbf{x}} - a(x_3 - \frac{1}{2}) \hat{\mathbf{y}} + \frac{1}{2} c \hat{\mathbf{z}}$	(4h)	Mo I
\mathbf{B}_9	$= -(x_3 - \frac{1}{2}) \mathbf{a}_1 + x_3 \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	$=$	$-a(x_3 - \frac{1}{2}) \hat{\mathbf{x}} + ax_3 \hat{\mathbf{y}} + \frac{1}{2} c \hat{\mathbf{z}}$	(4h)	Mo I
\mathbf{B}_{10}	$= (x_3 + \frac{1}{2}) \mathbf{a}_1 - x_3 \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	$=$	$a(x_3 + \frac{1}{2}) \hat{\mathbf{x}} - ax_3 \hat{\mathbf{y}} + \frac{1}{2} c \hat{\mathbf{z}}$	(4h)	Mo I

References

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