

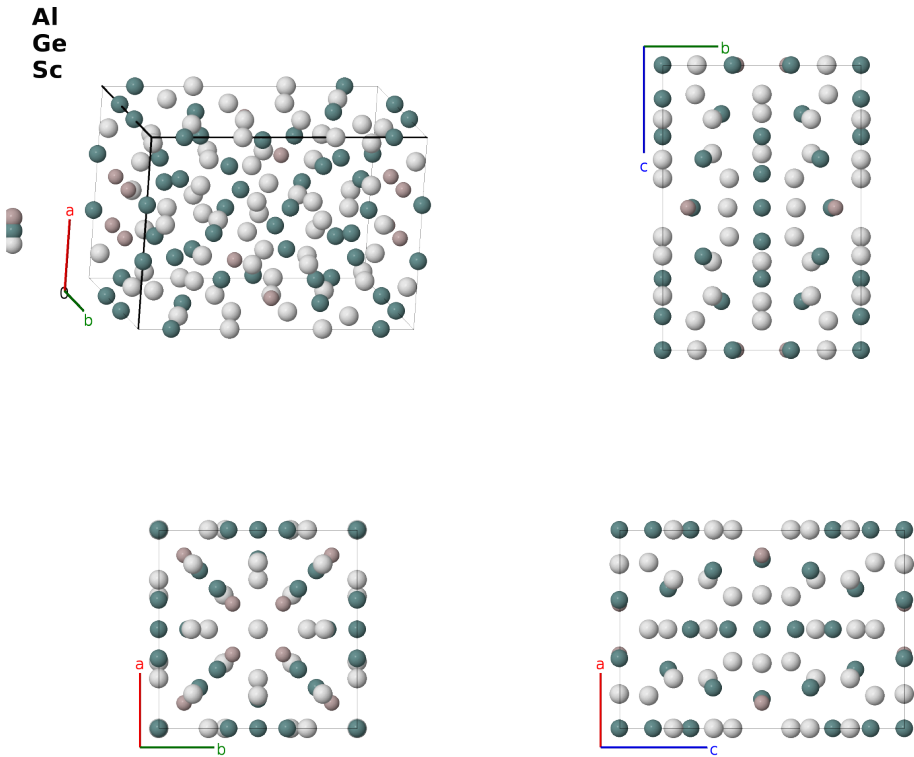
Sc₁₁Al₂Ge₈ Structure: A2B8C11_tI84_139_h_deim_eh2n-001

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<https://aflow.org/prototype-encyclopedia/DVM5>

https://aflow.org/prototype-encyclopedia/A2B8C11_tI84_139_h_deim_eh2n-001



Prototype	Al ₂ Ge ₈ Sc ₁₁
AFLOW prototype label	A2B8C11_tI84_139_h_deim_eh2n-001
ICSD	184236
CCDC	1693480
Pearson symbol	tI84
Space group number	139
Space group symbol	I4/mmm
AFLOW prototype command	<code>aflow --proto=A2B8C11_tI84_139_h_deim_eh2n-001</code> <code>--params=a, c/a, z₂, z₃, x₄, x₅, x₆, x₇, z₇, y₈, z₈, y₉, z₉</code>

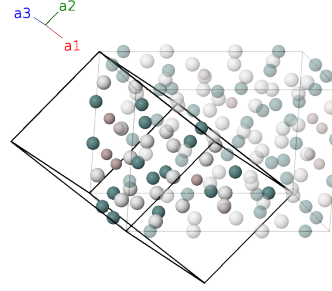
Other compounds with this structure

$\text{Er}_{11}\text{Al}_2\text{Ge}_8$, $\text{Gd}_{11}\text{In}_2\text{Ge}_8$, $\text{Yb}_{11}\text{Sn}_2\text{Bi}_8$

- This is a ternary form of $\text{Ho}_{11}\text{Ge}_{10}$. The ICSD lists all these compounds using the $\text{Ho}_{11}\text{Ge}_{10}$ prototype. We arbitrarily chose $\text{Sc}_{11}\text{Al}_2\text{Ge}_8$ as the prototype.
- $\text{Tb}_{11}\text{Si}_4\text{In}_6$ is a second ternary form of $\text{Ho}_{11}\text{Ge}_{10}$.
- The AFLOW standard labeling algorithm shifts the origin by $(0.5\ a, 0.5\ b, 0)$, moving the Ge III atom from the published (8j) Wyckoff position to (8i).

Body-centered Tetragonal primitive vectors

$$\begin{aligned}\mathbf{a}_1 &= -\frac{1}{2}a\hat{\mathbf{x}} + \frac{1}{2}a\hat{\mathbf{y}} + \frac{1}{2}c\hat{\mathbf{z}} \\ \mathbf{a}_2 &= \frac{1}{2}a\hat{\mathbf{x}} - \frac{1}{2}a\hat{\mathbf{y}} + \frac{1}{2}c\hat{\mathbf{z}} \\ \mathbf{a}_3 &= \frac{1}{2}a\hat{\mathbf{x}} + \frac{1}{2}a\hat{\mathbf{y}} - \frac{1}{2}c\hat{\mathbf{z}}\end{aligned}$$



Basis vectors

	Lattice coordinates		Cartesian coordinates	Wyckoff position	Atom type
$\mathbf{B}_1$	$= \frac{3}{4}\mathbf{a}_1 + \frac{1}{4}\mathbf{a}_2 + \frac{1}{2}\mathbf{a}_3$	$=$	$\frac{1}{2}a\hat{\mathbf{y}} + \frac{1}{4}c\hat{\mathbf{z}}$	(4d)	Ge I
$\mathbf{B}_2$	$= \frac{1}{4}\mathbf{a}_1 + \frac{3}{4}\mathbf{a}_2 + \frac{1}{2}\mathbf{a}_3$	$=$	$\frac{1}{2}a\hat{\mathbf{x}} + \frac{1}{4}c\hat{\mathbf{z}}$	(4d)	Ge I
$\mathbf{B}_3$	$= z_2\mathbf{a}_1 + z_2\mathbf{a}_2$	$=$	$cz_2\hat{\mathbf{z}}$	(4e)	Ge II
$\mathbf{B}_4$	$= -z_2\mathbf{a}_1 - z_2\mathbf{a}_2$	$=$	$-cz_2\hat{\mathbf{z}}$	(4e)	Ge II
$\mathbf{B}_5$	$= z_3\mathbf{a}_1 + z_3\mathbf{a}_2$	$=$	$cz_3\hat{\mathbf{z}}$	(4e)	Sc I
$\mathbf{B}_6$	$= -z_3\mathbf{a}_1 - z_3\mathbf{a}_2$	$=$	$-cz_3\hat{\mathbf{z}}$	(4e)	Sc I
$\mathbf{B}_7$	$= x_4\mathbf{a}_1 + x_4\mathbf{a}_2 + 2x_4\mathbf{a}_3$	$=$	$ax_4\hat{\mathbf{x}} + ax_4\hat{\mathbf{y}}$	(8h)	Al I
$\mathbf{B}_8$	$= -x_4\mathbf{a}_1 - x_4\mathbf{a}_2 - 2x_4\mathbf{a}_3$	$=$	$-ax_4\hat{\mathbf{x}} - ax_4\hat{\mathbf{y}}$	(8h)	Al I
$\mathbf{B}_9$	$= x_4\mathbf{a}_1 - x_4\mathbf{a}_2$	$=$	$-ax_4\hat{\mathbf{x}} + ax_4\hat{\mathbf{y}}$	(8h)	Al I
$\mathbf{B}_{10}$	$= -x_4\mathbf{a}_1 + x_4\mathbf{a}_2$	$=$	$ax_4\hat{\mathbf{x}} - ax_4\hat{\mathbf{y}}$	(8h)	Al I
$\mathbf{B}_{11}$	$= x_5\mathbf{a}_1 + x_5\mathbf{a}_2 + 2x_5\mathbf{a}_3$	$=$	$ax_5\hat{\mathbf{x}} + ax_5\hat{\mathbf{y}}$	(8h)	Sc II
$\mathbf{B}_{12}$	$= -x_5\mathbf{a}_1 - x_5\mathbf{a}_2 - 2x_5\mathbf{a}_3$	$=$	$-ax_5\hat{\mathbf{x}} - ax_5\hat{\mathbf{y}}$	(8h)	Sc II
$\mathbf{B}_{13}$	$= x_5\mathbf{a}_1 - x_5\mathbf{a}_2$	$=$	$-ax_5\hat{\mathbf{x}} + ax_5\hat{\mathbf{y}}$	(8h)	Sc II
$\mathbf{B}_{14}$	$= -x_5\mathbf{a}_1 + x_5\mathbf{a}_2$	$=$	$ax_5\hat{\mathbf{x}} - ax_5\hat{\mathbf{y}}$	(8h)	Sc II
$\mathbf{B}_{15}$	$= x_6\mathbf{a}_2 + x_6\mathbf{a}_3$	$=$	$ax_6\hat{\mathbf{x}}$	(8i)	Ge III
$\mathbf{B}_{16}$	$= -x_6\mathbf{a}_2 - x_6\mathbf{a}_3$	$=$	$-ax_6\hat{\mathbf{x}}$	(8i)	Ge III
$\mathbf{B}_{17}$	$= x_6\mathbf{a}_1 + x_6\mathbf{a}_3$	$=$	$ax_6\hat{\mathbf{y}}$	(8i)	Ge III
$\mathbf{B}_{18}$	$= -x_6\mathbf{a}_1 - x_6\mathbf{a}_3$	$=$	$-ax_6\hat{\mathbf{y}}$	(8i)	Ge III
$\mathbf{B}_{19}$	$= (x_7 + z_7)\mathbf{a}_1 + (x_7 + z_7)\mathbf{a}_2 + 2x_7\mathbf{a}_3$	$=$	$ax_7\hat{\mathbf{x}} + ax_7\hat{\mathbf{y}} + cz_7\hat{\mathbf{z}}$	(16m)	Ge IV

$\mathbf{B}_{20}$	$= - (x_7 - z_7) \mathbf{a}_1 - (x_7 - z_7) \mathbf{a}_2 - 2x_7 \mathbf{a}_3$	$=$	$-ax_7 \hat{\mathbf{x}} - ax_7 \hat{\mathbf{y}} + cz_7 \hat{\mathbf{z}}$	(16m)	Ge IV
$\mathbf{B}_{21}$	$= (x_7 + z_7) \mathbf{a}_1 - (x_7 - z_7) \mathbf{a}_2$	$=$	$-ax_7 \hat{\mathbf{x}} + ax_7 \hat{\mathbf{y}} + cz_7 \hat{\mathbf{z}}$	(16m)	Ge IV
$\mathbf{B}_{22}$	$= - (x_7 - z_7) \mathbf{a}_1 + (x_7 + z_7) \mathbf{a}_2$	$=$	$ax_7 \hat{\mathbf{x}} - ax_7 \hat{\mathbf{y}} + cz_7 \hat{\mathbf{z}}$	(16m)	Ge IV
$\mathbf{B}_{23}$	$= (x_7 - z_7) \mathbf{a}_1 - (x_7 + z_7) \mathbf{a}_2$	$=$	$-ax_7 \hat{\mathbf{x}} + ax_7 \hat{\mathbf{y}} - cz_7 \hat{\mathbf{z}}$	(16m)	Ge IV
$\mathbf{B}_{24}$	$= - (x_7 + z_7) \mathbf{a}_1 + (x_7 - z_7) \mathbf{a}_2$	$=$	$ax_7 \hat{\mathbf{x}} - ax_7 \hat{\mathbf{y}} - cz_7 \hat{\mathbf{z}}$	(16m)	Ge IV
$\mathbf{B}_{25}$	$= (x_7 - z_7) \mathbf{a}_1 + (x_7 - z_7) \mathbf{a}_2 + 2x_7 \mathbf{a}_3$	$=$	$ax_7 \hat{\mathbf{x}} + ax_7 \hat{\mathbf{y}} - cz_7 \hat{\mathbf{z}}$	(16m)	Ge IV
$\mathbf{B}_{26}$	$= - (x_7 + z_7) \mathbf{a}_1 - (x_7 + z_7) \mathbf{a}_2 - 2x_7 \mathbf{a}_3$	$=$	$-ax_7 \hat{\mathbf{x}} - ax_7 \hat{\mathbf{y}} - cz_7 \hat{\mathbf{z}}$	(16m)	Ge IV
$\mathbf{B}_{27}$	$= (y_8 + z_8) \mathbf{a}_1 + z_8 \mathbf{a}_2 + y_8 \mathbf{a}_3$	$=$	$ay_8 \hat{\mathbf{y}} + cz_8 \hat{\mathbf{z}}$	(16n)	Sc III
$\mathbf{B}_{28}$	$= - (y_8 - z_8) \mathbf{a}_1 + z_8 \mathbf{a}_2 - y_8 \mathbf{a}_3$	$=$	$-ay_8 \hat{\mathbf{y}} + cz_8 \hat{\mathbf{z}}$	(16n)	Sc III
$\mathbf{B}_{29}$	$= z_8 \mathbf{a}_1 - (y_8 - z_8) \mathbf{a}_2 - y_8 \mathbf{a}_3$	$=$	$-ay_8 \hat{\mathbf{x}} + cz_8 \hat{\mathbf{z}}$	(16n)	Sc III
$\mathbf{B}_{30}$	$= z_8 \mathbf{a}_1 + (y_8 + z_8) \mathbf{a}_2 + y_8 \mathbf{a}_3$	$=$	$ay_8 \hat{\mathbf{x}} + cz_8 \hat{\mathbf{z}}$	(16n)	Sc III
$\mathbf{B}_{31}$	$= (y_8 - z_8) \mathbf{a}_1 - z_8 \mathbf{a}_2 + y_8 \mathbf{a}_3$	$=$	$ay_8 \hat{\mathbf{y}} - cz_8 \hat{\mathbf{z}}$	(16n)	Sc III
$\mathbf{B}_{32}$	$= - (y_8 + z_8) \mathbf{a}_1 - z_8 \mathbf{a}_2 - y_8 \mathbf{a}_3$	$=$	$-ay_8 \hat{\mathbf{y}} - cz_8 \hat{\mathbf{z}}$	(16n)	Sc III
$\mathbf{B}_{33}$	$= -z_8 \mathbf{a}_1 + (y_8 - z_8) \mathbf{a}_2 + y_8 \mathbf{a}_3$	$=$	$ay_8 \hat{\mathbf{x}} - cz_8 \hat{\mathbf{z}}$	(16n)	Sc III
$\mathbf{B}_{34}$	$= -z_8 \mathbf{a}_1 - (y_8 + z_8) \mathbf{a}_2 - y_8 \mathbf{a}_3$	$=$	$-ay_8 \hat{\mathbf{x}} - cz_8 \hat{\mathbf{z}}$	(16n)	Sc III
$\mathbf{B}_{35}$	$= (y_9 + z_9) \mathbf{a}_1 + z_9 \mathbf{a}_2 + y_9 \mathbf{a}_3$	$=$	$ay_9 \hat{\mathbf{y}} + cz_9 \hat{\mathbf{z}}$	(16n)	Sc IV
$\mathbf{B}_{36}$	$= - (y_9 - z_9) \mathbf{a}_1 + z_9 \mathbf{a}_2 - y_9 \mathbf{a}_3$	$=$	$-ay_9 \hat{\mathbf{y}} + cz_9 \hat{\mathbf{z}}$	(16n)	Sc IV
$\mathbf{B}_{37}$	$= z_9 \mathbf{a}_1 - (y_9 - z_9) \mathbf{a}_2 - y_9 \mathbf{a}_3$	$=$	$-ay_9 \hat{\mathbf{x}} + cz_9 \hat{\mathbf{z}}$	(16n)	Sc IV
$\mathbf{B}_{38}$	$= z_9 \mathbf{a}_1 + (y_9 + z_9) \mathbf{a}_2 + y_9 \mathbf{a}_3$	$=$	$ay_9 \hat{\mathbf{x}} + cz_9 \hat{\mathbf{z}}$	(16n)	Sc IV
$\mathbf{B}_{39}$	$= (y_9 - z_9) \mathbf{a}_1 - z_9 \mathbf{a}_2 + y_9 \mathbf{a}_3$	$=$	$ay_9 \hat{\mathbf{y}} - cz_9 \hat{\mathbf{z}}$	(16n)	Sc IV
$\mathbf{B}_{40}$	$= - (y_9 + z_9) \mathbf{a}_1 - z_9 \mathbf{a}_2 - y_9 \mathbf{a}_3$	$=$	$-ay_9 \hat{\mathbf{y}} - cz_9 \hat{\mathbf{z}}$	(16n)	Sc IV
$\mathbf{B}_{41}$	$= -z_9 \mathbf{a}_1 + (y_9 - z_9) \mathbf{a}_2 + y_9 \mathbf{a}_3$	$=$	$ay_9 \hat{\mathbf{x}} - cz_9 \hat{\mathbf{z}}$	(16n)	Sc IV
$\mathbf{B}_{42}$	$= -z_9 \mathbf{a}_1 - (y_9 + z_9) \mathbf{a}_2 - y_9 \mathbf{a}_3$	$=$	$-ay_9 \hat{\mathbf{x}} - cz_9 \hat{\mathbf{z}}$	(16n)	Sc IV

References

- [1] J. T. Zhao and E. Parthé, *Sc₁₁Al₂Ge₈, a ternary substitution variant of the tetragonal Ho₁₁Ge₁₀ type*, Acta Crystallogr. Sect. C **47**, 4–6 (1991), doi:10.1107/S0108270190007314.

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