

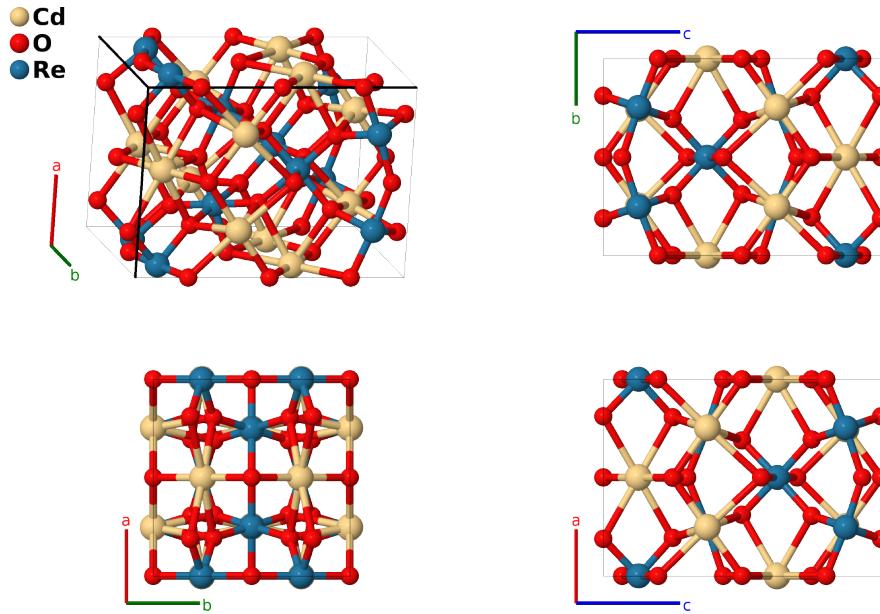
# Phase II Cd<sub>2</sub>Re<sub>2</sub>O<sub>7</sub> Structure: A2B7C2\_tI44\_119\_i\_acefgh\_i-001

This structure originally had the label A2B7C2\_tI44\_119\_i\_bdefgh\_i. Calls to that address will be redirected here.

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<https://aflow.org/p/AZDB>

[https://aflow.org/p/A2B7C2\\_tI44\\_119\\_i\\_acefgh\\_i-001](https://aflow.org/p/A2B7C2_tI44_119_i_acefgh_i-001)



<b>Prototype</b>	Cd <sub>2</sub> O <sub>7</sub> Re <sub>2</sub>
<b>AFLOW prototype label</b>	A2B7C2_tI44_119_i_acefgh_i-001
<b>ICSD</b>	none
<b>Pearson symbol</b>	tI44
<b>Space group number</b>	119
<b>Space group symbol</b>	$I\bar{4}m2$
<b>AFLOW prototype command</b>	<pre>aflow --proto=A2B7C2_tI44_119_i_acefgh_i-001 --params=a,c/a,z3,z4,x5,x6,x7,z8,x8,z8</pre>

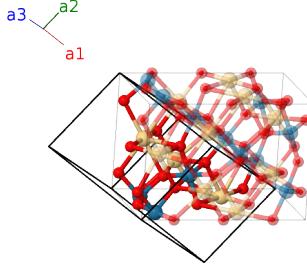
- Cd<sub>2</sub>Re<sub>2</sub>O<sub>7</sub> exhibits a number of phases. We will use the notation of (Kapcia, 2020) to describe them:
  - Phase I: Above 200K the system takes on the cubic pyrochlore ( $E8_1$ ) structure.
  - Phase II: in the range 120-200K the system is in the tetragonal  $I\bar{4}m2$  #119 structure. (this structure)
  - Phase III: in the range 80-120K the system is in the tetragonal  $I4_122$  #98 structure.
  - Phase IV: (Kapcia, 2020) did a first-principles study of this system and found that below 80K Phase III develops a soft phonon mode which transforms the system into an orthorhombic  $F222$  #22 structure.

- There are many issues with all of these structures (Norman, 2020):
  - Phases II, III, and IV are all close to phase I. If we loosen the tolerance using AFLOW-SYM or FINDSYM the structures are seen to be equivalent to cubic pyrochlore.
  - Using the default tolerance, Phase II and Phase IV are equivalent.
- Data for the Phase II structure was taken at 160K.

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### Body-centered Tetragonal primitive vectors

$$\begin{aligned}\mathbf{a}_1 &= -\frac{1}{2}a\hat{\mathbf{x}} + \frac{1}{2}a\hat{\mathbf{y}} + \frac{1}{2}c\hat{\mathbf{z}} \\ \mathbf{a}_2 &= \frac{1}{2}a\hat{\mathbf{x}} - \frac{1}{2}a\hat{\mathbf{y}} + \frac{1}{2}c\hat{\mathbf{z}} \\ \mathbf{a}_3 &= \frac{1}{2}a\hat{\mathbf{x}} + \frac{1}{2}a\hat{\mathbf{y}} - \frac{1}{2}c\hat{\mathbf{z}}\end{aligned}$$




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### Basis vectors

	Lattice coordinates		Cartesian coordinates	Wyckoff position	Atom type
$\mathbf{B}_1$	= 0	=	0	(2a)	O I
$\mathbf{B}_2$	= $\frac{3}{4}\mathbf{a}_1 + \frac{1}{4}\mathbf{a}_2 + \frac{1}{2}\mathbf{a}_3$	=	$\frac{1}{2}a\hat{\mathbf{y}} + \frac{1}{4}c\hat{\mathbf{z}}$	(2c)	O II
$\mathbf{B}_3$	= $z_3\mathbf{a}_1 + z_3\mathbf{a}_2$	=	$cz_3\hat{\mathbf{z}}$	(4e)	O III
$\mathbf{B}_4$	= $-z_3\mathbf{a}_1 - z_3\mathbf{a}_2$	=	$-cz_3\hat{\mathbf{z}}$	(4e)	O III
$\mathbf{B}_5$	= $(z_4 + \frac{1}{2})\mathbf{a}_1 + z_4\mathbf{a}_2 + \frac{1}{2}\mathbf{a}_3$	=	$\frac{1}{2}a\hat{\mathbf{y}} + cz_4\hat{\mathbf{z}}$	(4f)	O IV
$\mathbf{B}_6$	= $-z_4\mathbf{a}_1 - (z_4 - \frac{1}{2})\mathbf{a}_2 + \frac{1}{2}\mathbf{a}_3$	=	$\frac{1}{2}a\hat{\mathbf{x}} - cz_4\hat{\mathbf{z}}$	(4f)	O IV
$\mathbf{B}_7$	= $x_5\mathbf{a}_1 + x_5\mathbf{a}_2 + 2x_5\mathbf{a}_3$	=	$ax_5\hat{\mathbf{x}} + ax_5\hat{\mathbf{y}}$	(8g)	O V
$\mathbf{B}_8$	= $-x_5\mathbf{a}_1 - x_5\mathbf{a}_2 - 2x_5\mathbf{a}_3$	=	$-ax_5\hat{\mathbf{x}} - ax_5\hat{\mathbf{y}}$	(8g)	O V
$\mathbf{B}_9$	= $-x_5\mathbf{a}_1 + x_5\mathbf{a}_2$	=	$ax_5\hat{\mathbf{x}} - ax_5\hat{\mathbf{y}}$	(8g)	O V
$\mathbf{B}_{10}$	= $x_5\mathbf{a}_1 - x_5\mathbf{a}_2$	=	$-ax_5\hat{\mathbf{x}} + ax_5\hat{\mathbf{y}}$	(8g)	O V
$\mathbf{B}_{11}$	= $(x_6 + \frac{3}{4})\mathbf{a}_1 + (x_6 + \frac{1}{4})\mathbf{a}_2 + (2x_6 + \frac{1}{2})\mathbf{a}_3$	=	$ax_6\hat{\mathbf{x}} + a(x_6 + \frac{1}{2})\hat{\mathbf{y}} + \frac{1}{4}c\hat{\mathbf{z}}$	(8h)	O VI
$\mathbf{B}_{12}$	= $-(x_6 - \frac{3}{4})\mathbf{a}_1 - (x_6 - \frac{1}{4})\mathbf{a}_2 - (2x_6 - \frac{1}{2})\mathbf{a}_3$	=	$-ax_6\hat{\mathbf{x}} - a(x_6 - \frac{1}{2})\hat{\mathbf{y}} + \frac{1}{4}c\hat{\mathbf{z}}$	(8h)	O VI
$\mathbf{B}_{13}$	= $-(x_6 - \frac{3}{4})\mathbf{a}_1 + (x_6 + \frac{1}{4})\mathbf{a}_2 + \frac{1}{2}\mathbf{a}_3$	=	$ax_6\hat{\mathbf{x}} - a(x_6 - \frac{1}{2})\hat{\mathbf{y}} + \frac{1}{4}c\hat{\mathbf{z}}$	(8h)	O VI
$\mathbf{B}_{14}$	= $(x_6 + \frac{3}{4})\mathbf{a}_1 - (x_6 - \frac{1}{4})\mathbf{a}_2 + \frac{1}{2}\mathbf{a}_3$	=	$-ax_6\hat{\mathbf{x}} + a(x_6 + \frac{1}{2})\hat{\mathbf{y}} + \frac{1}{4}c\hat{\mathbf{z}}$	(8h)	O VI
$\mathbf{B}_{15}$	= $z_7\mathbf{a}_1 + (x_7 + z_7)\mathbf{a}_2 + x_7\mathbf{a}_3$	=	$ax_7\hat{\mathbf{x}} + cz_7\hat{\mathbf{z}}$	(8i)	Cd I
$\mathbf{B}_{16}$	= $z_7\mathbf{a}_1 - (x_7 - z_7)\mathbf{a}_2 - x_7\mathbf{a}_3$	=	$-ax_7\hat{\mathbf{x}} + cz_7\hat{\mathbf{z}}$	(8i)	Cd I
$\mathbf{B}_{17}$	= $-(x_7 + z_7)\mathbf{a}_1 - z_7\mathbf{a}_2 - x_7\mathbf{a}_3$	=	$-ax_7\hat{\mathbf{y}} - cz_7\hat{\mathbf{z}}$	(8i)	Cd I
$\mathbf{B}_{18}$	= $(x_7 - z_7)\mathbf{a}_1 - z_7\mathbf{a}_2 + x_7\mathbf{a}_3$	=	$ax_7\hat{\mathbf{y}} - cz_7\hat{\mathbf{z}}$	(8i)	Cd I
$\mathbf{B}_{19}$	= $z_8\mathbf{a}_1 + (x_8 + z_8)\mathbf{a}_2 + x_8\mathbf{a}_3$	=	$ax_8\hat{\mathbf{x}} + cz_8\hat{\mathbf{z}}$	(8i)	Re I
$\mathbf{B}_{20}$	= $z_8\mathbf{a}_1 - (x_8 - z_8)\mathbf{a}_2 - x_8\mathbf{a}_3$	=	$-ax_8\hat{\mathbf{x}} + cz_8\hat{\mathbf{z}}$	(8i)	Re I
$\mathbf{B}_{21}$	= $-(x_8 + z_8)\mathbf{a}_1 - z_8\mathbf{a}_2 - x_8\mathbf{a}_3$	=	$-ax_8\hat{\mathbf{y}} - cz_8\hat{\mathbf{z}}$	(8i)	Re I
$\mathbf{B}_{22}$	= $(x_8 - z_8)\mathbf{a}_1 - z_8\mathbf{a}_2 + x_8\mathbf{a}_3$	=	$ax_8\hat{\mathbf{y}} - cz_8\hat{\mathbf{z}}$	(8i)	Re I

## References

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