

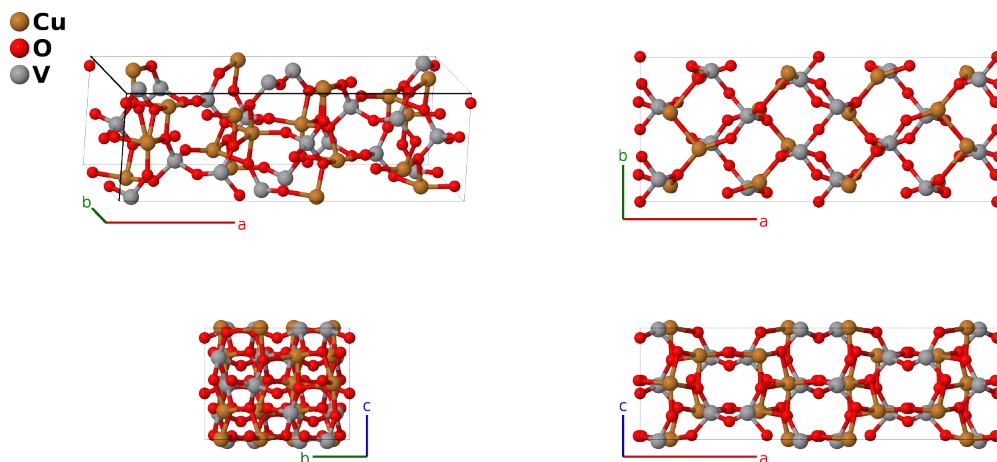
# Blossite ( $\alpha$ -Cu<sub>2</sub>V<sub>2</sub>O<sub>7</sub>) Structure: A2B7C2\_oF88\_43\_b\_a3b\_b-001

This structure originally had the label A2B7C2\_oF88\_43\_b\_a3b\_b. Calls to that address will be redirected here.

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<https://afLOW.org/p/D9YZ>

[https://afLOW.org/p/A2B7C2\\_oF88\\_43\\_b\\_a3b\\_b-001](https://afLOW.org/p/A2B7C2_oF88_43_b_a3b_b-001)



<b>Prototype</b>	Cu <sub>2</sub> O <sub>7</sub> V <sub>2</sub>
<b>AFLOW prototype label</b>	A2B7C2_oF88_43_b_a3b_b-001
<b>Mineral name</b>	blossite
<b>ICSD</b>	1831
<b>Pearson symbol</b>	oF88
<b>Space group number</b>	43
<b>Space group symbol</b>	<i>Fdd2</i>
<b>AFLOW prototype command</b>	<code>afLOW --proto=A2B7C2_oF88_43_b_a3b_b-001 --params=a, b/a, c/a, z<sub>1</sub>, x<sub>2</sub>, y<sub>2</sub>, z<sub>2</sub>, x<sub>3</sub>, y<sub>3</sub>, z<sub>3</sub>, x<sub>4</sub>, y<sub>4</sub>, z<sub>4</sub>, x<sub>5</sub>, y<sub>5</sub>, z<sub>5</sub>, x<sub>6</sub>, y<sub>6</sub>, z<sub>6</sub></code>

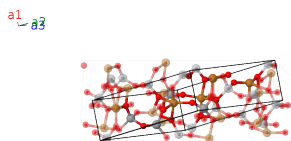
- This structure was given the name “blossite” by (Robinson, 1987).
- Space group *Fdd2* #43 does not fix the  $z = 0$  plane. We do this by setting  $z_2 = 3/4$  for the copper atom.

## Face-centered Orthorhombic primitive vectors

$$\mathbf{a}_1 = \frac{1}{2}b\hat{y} + \frac{1}{2}c\hat{z}$$

$$\mathbf{a}_2 = \frac{1}{2}a\hat{x} + \frac{1}{2}c\hat{z}$$

$$\mathbf{a}_3 = \frac{1}{2}a\hat{x} + \frac{1}{2}b\hat{y}$$



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**Basis vectors**

	Lattice coordinates		Cartesian coordinates	Wyckoff position	Atom type
$\mathbf{B}_1$	$= z_1 \mathbf{a}_1 + z_1 \mathbf{a}_2 - z_1 \mathbf{a}_3$	$=$	$cz_1 \hat{\mathbf{z}}$	(8a)	O I
$\mathbf{B}_2$	$= (z_1 + \frac{1}{4}) \mathbf{a}_1 + (z_1 + \frac{1}{4}) \mathbf{a}_2 -$ $(z_1 - \frac{1}{4}) \mathbf{a}_3$	$=$	$\frac{1}{4}a \hat{\mathbf{x}} + \frac{1}{4}b \hat{\mathbf{y}} + c(z_1 + \frac{1}{4}) \hat{\mathbf{z}}$	(8a)	O I
$\mathbf{B}_3$	$= (-x_2 + y_2 + z_2) \mathbf{a}_1 +$ $(x_2 - y_2 + z_2) \mathbf{a}_2 +$ $(x_2 + y_2 - z_2) \mathbf{a}_3$	$=$	$ax_2 \hat{\mathbf{x}} + by_2 \hat{\mathbf{y}} + cz_2 \hat{\mathbf{z}}$	(16b)	Cu I
$\mathbf{B}_4$	$= (x_2 - y_2 + z_2) \mathbf{a}_1 +$ $(-x_2 + y_2 + z_2) \mathbf{a}_2 -$ $(x_2 + y_2 + z_2) \mathbf{a}_3$	$=$	$-ax_2 \hat{\mathbf{x}} - by_2 \hat{\mathbf{y}} + cz_2 \hat{\mathbf{z}}$	(16b)	Cu I
$\mathbf{B}_5$	$= -(x_2 + y_2 - z_2 - \frac{1}{4}) \mathbf{a}_1 +$ $(x_2 + y_2 + z_2 + \frac{1}{4}) \mathbf{a}_2 +$ $(x_2 - y_2 - z_2 + \frac{1}{4}) \mathbf{a}_3$	$=$	$a(x_2 + \frac{1}{4}) \hat{\mathbf{x}} - b(y_2 - \frac{1}{4}) \hat{\mathbf{y}} + c(z_2 + \frac{1}{4}) \hat{\mathbf{z}}$	(16b)	Cu I
$\mathbf{B}_6$	$= (x_2 + y_2 + z_2 + \frac{1}{4}) \mathbf{a}_1 -$ $(x_2 + y_2 - z_2 - \frac{1}{4}) \mathbf{a}_2 -$ $(x_2 - y_2 + z_2 - \frac{1}{4}) \mathbf{a}_3$	$=$	$-a(x_2 - \frac{1}{4}) \hat{\mathbf{x}} + b(y_2 + \frac{1}{4}) \hat{\mathbf{y}} + c(z_2 + \frac{1}{4}) \hat{\mathbf{z}}$	(16b)	Cu I
$\mathbf{B}_7$	$= (-x_3 + y_3 + z_3) \mathbf{a}_1 +$ $(x_3 - y_3 + z_3) \mathbf{a}_2 +$ $(x_3 + y_3 - z_3) \mathbf{a}_3$	$=$	$ax_3 \hat{\mathbf{x}} + by_3 \hat{\mathbf{y}} + cz_3 \hat{\mathbf{z}}$	(16b)	O II
$\mathbf{B}_8$	$= (x_3 - y_3 + z_3) \mathbf{a}_1 +$ $(-x_3 + y_3 + z_3) \mathbf{a}_2 -$ $(x_3 + y_3 + z_3) \mathbf{a}_3$	$=$	$-ax_3 \hat{\mathbf{x}} - by_3 \hat{\mathbf{y}} + cz_3 \hat{\mathbf{z}}$	(16b)	O II
$\mathbf{B}_9$	$= -(x_3 + y_3 - z_3 - \frac{1}{4}) \mathbf{a}_1 +$ $(x_3 + y_3 + z_3 + \frac{1}{4}) \mathbf{a}_2 +$ $(x_3 - y_3 - z_3 + \frac{1}{4}) \mathbf{a}_3$	$=$	$a(x_3 + \frac{1}{4}) \hat{\mathbf{x}} - b(y_3 - \frac{1}{4}) \hat{\mathbf{y}} + c(z_3 + \frac{1}{4}) \hat{\mathbf{z}}$	(16b)	O II
$\mathbf{B}_{10}$	$= (x_3 + y_3 + z_3 + \frac{1}{4}) \mathbf{a}_1 -$ $(x_3 + y_3 - z_3 - \frac{1}{4}) \mathbf{a}_2 -$ $(x_3 - y_3 + z_3 - \frac{1}{4}) \mathbf{a}_3$	$=$	$-a(x_3 - \frac{1}{4}) \hat{\mathbf{x}} + b(y_3 + \frac{1}{4}) \hat{\mathbf{y}} + c(z_3 + \frac{1}{4}) \hat{\mathbf{z}}$	(16b)	O II
$\mathbf{B}_{11}$	$= (-x_4 + y_4 + z_4) \mathbf{a}_1 +$ $(x_4 - y_4 + z_4) \mathbf{a}_2 +$ $(x_4 + y_4 - z_4) \mathbf{a}_3$	$=$	$ax_4 \hat{\mathbf{x}} + by_4 \hat{\mathbf{y}} + cz_4 \hat{\mathbf{z}}$	(16b)	O III
$\mathbf{B}_{12}$	$= (x_4 - y_4 + z_4) \mathbf{a}_1 +$ $(-x_4 + y_4 + z_4) \mathbf{a}_2 -$ $(x_4 + y_4 + z_4) \mathbf{a}_3$	$=$	$-ax_4 \hat{\mathbf{x}} - by_4 \hat{\mathbf{y}} + cz_4 \hat{\mathbf{z}}$	(16b)	O III
$\mathbf{B}_{13}$	$= -(x_4 + y_4 - z_4 - \frac{1}{4}) \mathbf{a}_1 +$ $(x_4 + y_4 + z_4 + \frac{1}{4}) \mathbf{a}_2 +$ $(x_4 - y_4 - z_4 + \frac{1}{4}) \mathbf{a}_3$	$=$	$a(x_4 + \frac{1}{4}) \hat{\mathbf{x}} - b(y_4 - \frac{1}{4}) \hat{\mathbf{y}} + c(z_4 + \frac{1}{4}) \hat{\mathbf{z}}$	(16b)	O III
$\mathbf{B}_{14}$	$= (x_4 + y_4 + z_4 + \frac{1}{4}) \mathbf{a}_1 -$ $(x_4 + y_4 - z_4 - \frac{1}{4}) \mathbf{a}_2 -$ $(x_4 - y_4 + z_4 - \frac{1}{4}) \mathbf{a}_3$	$=$	$-a(x_4 - \frac{1}{4}) \hat{\mathbf{x}} + b(y_4 + \frac{1}{4}) \hat{\mathbf{y}} + c(z_4 + \frac{1}{4}) \hat{\mathbf{z}}$	(16b)	O III
$\mathbf{B}_{15}$	$= (-x_5 + y_5 + z_5) \mathbf{a}_1 +$ $(x_5 - y_5 + z_5) \mathbf{a}_2 +$ $(x_5 + y_5 - z_5) \mathbf{a}_3$	$=$	$ax_5 \hat{\mathbf{x}} + by_5 \hat{\mathbf{y}} + cz_5 \hat{\mathbf{z}}$	(16b)	O IV
$\mathbf{B}_{16}$	$= (x_5 - y_5 + z_5) \mathbf{a}_1 +$ $(-x_5 + y_5 + z_5) \mathbf{a}_2 -$ $(x_5 + y_5 + z_5) \mathbf{a}_3$	$=$	$-ax_5 \hat{\mathbf{x}} - by_5 \hat{\mathbf{y}} + cz_5 \hat{\mathbf{z}}$	(16b)	O IV

$$\mathbf{B}_{17} = \begin{matrix} -(x_5 + y_5 - z_5 - \frac{1}{4}) \mathbf{a}_1 + \\ (x_5 + y_5 + z_5 + \frac{1}{4}) \mathbf{a}_2 + \\ (x_5 - y_5 - z_5 + \frac{1}{4}) \mathbf{a}_3 \end{matrix} = a(x_5 + \frac{1}{4}) \hat{\mathbf{x}} - b(y_5 - \frac{1}{4}) \hat{\mathbf{y}} + c(z_5 + \frac{1}{4}) \hat{\mathbf{z}} \quad (16b) \quad \text{O IV}$$

$$\mathbf{B}_{18} = \begin{matrix} (x_5 + y_5 + z_5 + \frac{1}{4}) \mathbf{a}_1 - \\ (x_5 + y_5 - z_5 - \frac{1}{4}) \mathbf{a}_2 - \\ (x_5 - y_5 + z_5 - \frac{1}{4}) \mathbf{a}_3 \end{matrix} = -a(x_5 - \frac{1}{4}) \hat{\mathbf{x}} + b(y_5 + \frac{1}{4}) \hat{\mathbf{y}} + c(z_5 + \frac{1}{4}) \hat{\mathbf{z}} \quad (16b) \quad \text{O IV}$$

$$\mathbf{B}_{19} = \begin{matrix} (-x_6 + y_6 + z_6) \mathbf{a}_1 + \\ (x_6 - y_6 + z_6) \mathbf{a}_2 + \\ (x_6 + y_6 - z_6) \mathbf{a}_3 \end{matrix} = ax_6 \hat{\mathbf{x}} + by_6 \hat{\mathbf{y}} + cz_6 \hat{\mathbf{z}} \quad (16b) \quad \text{V I}$$

$$\mathbf{B}_{20} = \begin{matrix} (x_6 - y_6 + z_6) \mathbf{a}_1 + \\ (-x_6 + y_6 + z_6) \mathbf{a}_2 - \\ (x_6 + y_6 + z_6) \mathbf{a}_3 \end{matrix} = -ax_6 \hat{\mathbf{x}} - by_6 \hat{\mathbf{y}} + cz_6 \hat{\mathbf{z}} \quad (16b) \quad \text{V I}$$

$$\mathbf{B}_{21} = \begin{matrix} -(x_6 + y_6 - z_6 - \frac{1}{4}) \mathbf{a}_1 + \\ (x_6 + y_6 + z_6 + \frac{1}{4}) \mathbf{a}_2 + \\ (x_6 - y_6 - z_6 + \frac{1}{4}) \mathbf{a}_3 \end{matrix} = a(x_6 + \frac{1}{4}) \hat{\mathbf{x}} - b(y_6 - \frac{1}{4}) \hat{\mathbf{y}} + c(z_6 + \frac{1}{4}) \hat{\mathbf{z}} \quad (16b) \quad \text{V I}$$

$$\mathbf{B}_{22} = \begin{matrix} (x_6 + y_6 + z_6 + \frac{1}{4}) \mathbf{a}_1 - \\ (x_6 + y_6 - z_6 - \frac{1}{4}) \mathbf{a}_2 - \\ (x_6 - y_6 + z_6 - \frac{1}{4}) \mathbf{a}_3 \end{matrix} = -a(x_6 - \frac{1}{4}) \hat{\mathbf{x}} + b(y_6 + \frac{1}{4}) \hat{\mathbf{y}} + c(z_6 + \frac{1}{4}) \hat{\mathbf{z}} \quad (16b) \quad \text{V I}$$

## References

- [1] C. Calvo and R. Faggiani,  $\alpha$  *Cupric Divanadate*, *Acta Cryst.* **31**, 603–605 (1975), doi:10.1107/S0567740875003354.
- [2] P. D. Robinson, J. M. Hughs, and M. L. Malinconico, *Blossite*,  $\alpha$ - $\text{Cu}_2^{2+}\text{V}_2^{5+}\text{O}_7$ , *an new fumarolic sublimate from Izalco volcano, El Salvador*, *Am. Mineral.* **72**, 397–400 (1987).

## Found in

- [1] R. T. Downs and M. Hall-Wallace, *The American Mineralogist Crystal Structure Database*, *Am. Mineral.* **88**, 247–250 (2003).