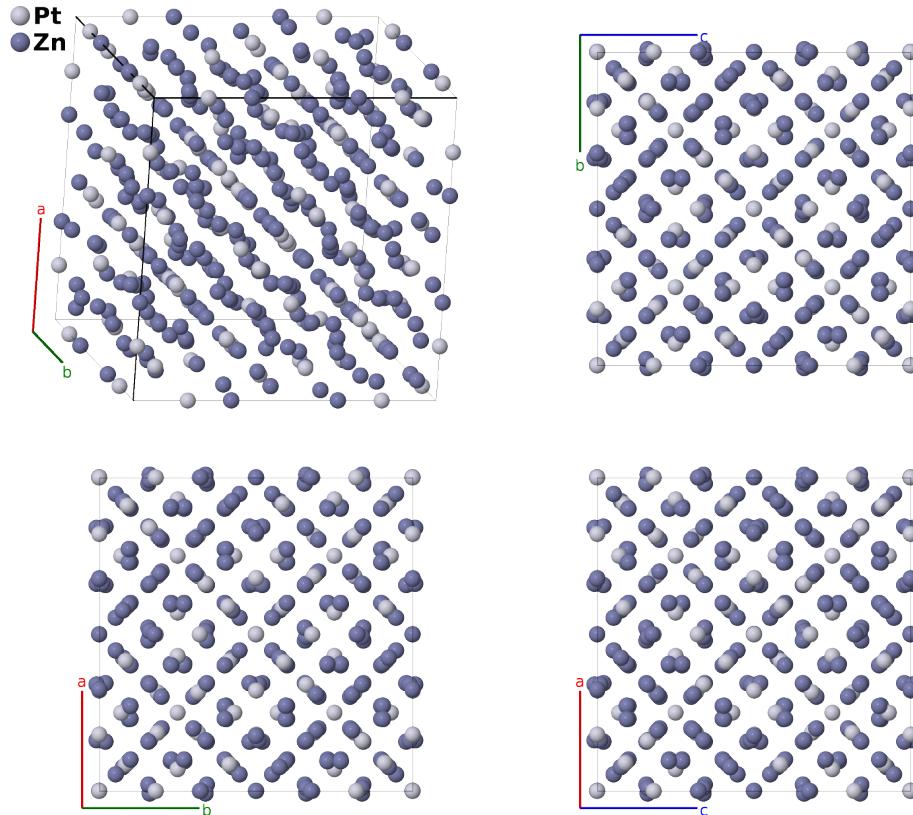


Pt₃Zn₁₀ Structure: A2B5_cF392_216_4efg_4ef4h-001

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<https://aflow.org/p/V17U>

https://aflow.org/p/A2B5_cF392_216_4efg_4ef4h-001



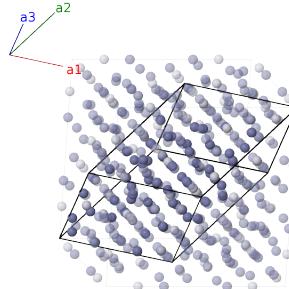
Prototype	Pt ₃ Zn ₁₀
AFLOW prototype label	A2B5_cF392_216_4efg_4ef4h-001
ICSD	105854
Pearson symbol	cF392
Space group number	216
Space group symbol	$F\bar{4}3m$
AFLOW prototype command	<code>aflow --proto=A2B5_cF392_216_4efg_4ef4h-001 --params=a,x₁,x₂,x₃,x₄,x₅,x₆,x₇,x₈,x₉,x₁₀,x₁₁,x₁₂,z₁₂,x₁₃,z₁₃,x₁₄,z₁₄,x₁₅,z₁₅</code>

- The site occupation in this structure is rather complicated:
 - In any unit cell, only one of the Pt-II/Zn-II sites is occupied.
 - The site we have labeled Pt-II is actually 50% platinum and 50% zinc.

- The sites we have labeled Zn-II and Zn-V are 8.333% platinum and 91.667% zinc.
- The Pt-V and Pt-VI sites are 2/3 platinum and 1/3 zinc.
- Accounting for all of this the nominal composition of the structure is approximately $\text{Pt}_3\text{Zn}_{10}$.
- This is an example of an F-cell γ -brass. (Mizutani, 2010)
- (Johansson, 1970) give the Wyckoff positions of the (24h) sites as xyy . The standard representation, used by AFLOW, is xyx , so we have swapped their x and y coordinates for these sites.

Face-centered Cubic primitive vectors

$$\begin{aligned}\mathbf{a}_1 &= \frac{1}{2}a\hat{\mathbf{y}} + \frac{1}{2}a\hat{\mathbf{z}} \\ \mathbf{a}_2 &= \frac{1}{2}a\hat{\mathbf{x}} + \frac{1}{2}a\hat{\mathbf{z}} \\ \mathbf{a}_3 &= \frac{1}{2}a\hat{\mathbf{x}} + \frac{1}{2}a\hat{\mathbf{y}}\end{aligned}$$



Basis vectors

	Lattice coordinates		Cartesian coordinates	Wyckoff position	Atom type
\mathbf{B}_1	$x_1 \mathbf{a}_1 + x_1 \mathbf{a}_2 + x_1 \mathbf{a}_3$	=	$ax_1 \hat{\mathbf{x}} + ax_1 \hat{\mathbf{y}} + ax_1 \hat{\mathbf{z}}$	(16e)	Pt I
\mathbf{B}_2	$x_1 \mathbf{a}_1 + x_1 \mathbf{a}_2 - 3x_1 \mathbf{a}_3$	=	$-ax_1 \hat{\mathbf{x}} - ax_1 \hat{\mathbf{y}} + ax_1 \hat{\mathbf{z}}$	(16e)	Pt I
\mathbf{B}_3	$x_1 \mathbf{a}_1 - 3x_1 \mathbf{a}_2 + x_1 \mathbf{a}_3$	=	$-ax_1 \hat{\mathbf{x}} + ax_1 \hat{\mathbf{y}} - ax_1 \hat{\mathbf{z}}$	(16e)	Pt I
\mathbf{B}_4	$-3x_1 \mathbf{a}_1 + x_1 \mathbf{a}_2 + x_1 \mathbf{a}_3$	=	$ax_1 \hat{\mathbf{x}} - ax_1 \hat{\mathbf{y}} - ax_1 \hat{\mathbf{z}}$	(16e)	Pt I
\mathbf{B}_5	$x_2 \mathbf{a}_1 + x_2 \mathbf{a}_2 + x_2 \mathbf{a}_3$	=	$ax_2 \hat{\mathbf{x}} + ax_2 \hat{\mathbf{y}} + ax_2 \hat{\mathbf{z}}$	(16e)	Pt II
\mathbf{B}_6	$x_2 \mathbf{a}_1 + x_2 \mathbf{a}_2 - 3x_2 \mathbf{a}_3$	=	$-ax_2 \hat{\mathbf{x}} - ax_2 \hat{\mathbf{y}} + ax_2 \hat{\mathbf{z}}$	(16e)	Pt II
\mathbf{B}_7	$x_2 \mathbf{a}_1 - 3x_2 \mathbf{a}_2 + x_2 \mathbf{a}_3$	=	$-ax_2 \hat{\mathbf{x}} + ax_2 \hat{\mathbf{y}} - ax_2 \hat{\mathbf{z}}$	(16e)	Pt II
\mathbf{B}_8	$-3x_2 \mathbf{a}_1 + x_2 \mathbf{a}_2 + x_2 \mathbf{a}_3$	=	$ax_2 \hat{\mathbf{x}} - ax_2 \hat{\mathbf{y}} - ax_2 \hat{\mathbf{z}}$	(16e)	Pt II
\mathbf{B}_9	$x_3 \mathbf{a}_1 + x_3 \mathbf{a}_2 + x_3 \mathbf{a}_3$	=	$ax_3 \hat{\mathbf{x}} + ax_3 \hat{\mathbf{y}} + ax_3 \hat{\mathbf{z}}$	(16e)	Pt III
\mathbf{B}_{10}	$x_3 \mathbf{a}_1 + x_3 \mathbf{a}_2 - 3x_3 \mathbf{a}_3$	=	$-ax_3 \hat{\mathbf{x}} - ax_3 \hat{\mathbf{y}} + ax_3 \hat{\mathbf{z}}$	(16e)	Pt III
\mathbf{B}_{11}	$x_3 \mathbf{a}_1 - 3x_3 \mathbf{a}_2 + x_3 \mathbf{a}_3$	=	$-ax_3 \hat{\mathbf{x}} + ax_3 \hat{\mathbf{y}} - ax_3 \hat{\mathbf{z}}$	(16e)	Pt III
\mathbf{B}_{12}	$-3x_3 \mathbf{a}_1 + x_3 \mathbf{a}_2 + x_3 \mathbf{a}_3$	=	$ax_3 \hat{\mathbf{x}} - ax_3 \hat{\mathbf{y}} - ax_3 \hat{\mathbf{z}}$	(16e)	Pt III
\mathbf{B}_{13}	$x_4 \mathbf{a}_1 + x_4 \mathbf{a}_2 + x_4 \mathbf{a}_3$	=	$ax_4 \hat{\mathbf{x}} + ax_4 \hat{\mathbf{y}} + ax_4 \hat{\mathbf{z}}$	(16e)	Pt IV
\mathbf{B}_{14}	$x_4 \mathbf{a}_1 + x_4 \mathbf{a}_2 - 3x_4 \mathbf{a}_3$	=	$-ax_4 \hat{\mathbf{x}} - ax_4 \hat{\mathbf{y}} + ax_4 \hat{\mathbf{z}}$	(16e)	Pt IV
\mathbf{B}_{15}	$x_4 \mathbf{a}_1 - 3x_4 \mathbf{a}_2 + x_4 \mathbf{a}_3$	=	$-ax_4 \hat{\mathbf{x}} + ax_4 \hat{\mathbf{y}} - ax_4 \hat{\mathbf{z}}$	(16e)	Pt IV
\mathbf{B}_{16}	$-3x_4 \mathbf{a}_1 + x_4 \mathbf{a}_2 + x_4 \mathbf{a}_3$	=	$ax_4 \hat{\mathbf{x}} - ax_4 \hat{\mathbf{y}} - ax_4 \hat{\mathbf{z}}$	(16e)	Pt IV
\mathbf{B}_{17}	$x_5 \mathbf{a}_1 + x_5 \mathbf{a}_2 + x_5 \mathbf{a}_3$	=	$ax_5 \hat{\mathbf{x}} + ax_5 \hat{\mathbf{y}} + ax_5 \hat{\mathbf{z}}$	(16e)	Zn I
\mathbf{B}_{18}	$x_5 \mathbf{a}_1 + x_5 \mathbf{a}_2 - 3x_5 \mathbf{a}_3$	=	$-ax_5 \hat{\mathbf{x}} - ax_5 \hat{\mathbf{y}} + ax_5 \hat{\mathbf{z}}$	(16e)	Zn I
\mathbf{B}_{19}	$x_5 \mathbf{a}_1 - 3x_5 \mathbf{a}_2 + x_5 \mathbf{a}_3$	=	$-ax_5 \hat{\mathbf{x}} + ax_5 \hat{\mathbf{y}} - ax_5 \hat{\mathbf{z}}$	(16e)	Zn I
\mathbf{B}_{20}	$-3x_5 \mathbf{a}_1 + x_5 \mathbf{a}_2 + x_5 \mathbf{a}_3$	=	$ax_5 \hat{\mathbf{x}} - ax_5 \hat{\mathbf{y}} - ax_5 \hat{\mathbf{z}}$	(16e)	Zn I
\mathbf{B}_{21}	$x_6 \mathbf{a}_1 + x_6 \mathbf{a}_2 + x_6 \mathbf{a}_3$	=	$ax_6 \hat{\mathbf{x}} + ax_6 \hat{\mathbf{y}} + ax_6 \hat{\mathbf{z}}$	(16e)	Zn II
\mathbf{B}_{22}	$x_6 \mathbf{a}_1 + x_6 \mathbf{a}_2 - 3x_6 \mathbf{a}_3$	=	$-ax_6 \hat{\mathbf{x}} - ax_6 \hat{\mathbf{y}} + ax_6 \hat{\mathbf{z}}$	(16e)	Zn II

$\mathbf{B}_{23} =$	$x_6 \mathbf{a}_1 - 3x_6 \mathbf{a}_2 + x_6 \mathbf{a}_3$	$=$	$-ax_6 \hat{\mathbf{x}} + ax_6 \hat{\mathbf{y}} - ax_6 \hat{\mathbf{z}}$	(16e)	Zn II
$\mathbf{B}_{24} =$	$-3x_6 \mathbf{a}_1 + x_6 \mathbf{a}_2 + x_6 \mathbf{a}_3$	$=$	$ax_6 \hat{\mathbf{x}} - ax_6 \hat{\mathbf{y}} - ax_6 \hat{\mathbf{z}}$	(16e)	Zn II
$\mathbf{B}_{25} =$	$x_7 \mathbf{a}_1 + x_7 \mathbf{a}_2 + x_7 \mathbf{a}_3$	$=$	$ax_7 \hat{\mathbf{x}} + ax_7 \hat{\mathbf{y}} + ax_7 \hat{\mathbf{z}}$	(16e)	Zn III
$\mathbf{B}_{26} =$	$x_7 \mathbf{a}_1 + x_7 \mathbf{a}_2 - 3x_7 \mathbf{a}_3$	$=$	$-ax_7 \hat{\mathbf{x}} - ax_7 \hat{\mathbf{y}} + ax_7 \hat{\mathbf{z}}$	(16e)	Zn III
$\mathbf{B}_{27} =$	$x_7 \mathbf{a}_1 - 3x_7 \mathbf{a}_2 + x_7 \mathbf{a}_3$	$=$	$-ax_7 \hat{\mathbf{x}} + ax_7 \hat{\mathbf{y}} - ax_7 \hat{\mathbf{z}}$	(16e)	Zn III
$\mathbf{B}_{28} =$	$-3x_7 \mathbf{a}_1 + x_7 \mathbf{a}_2 + x_7 \mathbf{a}_3$	$=$	$ax_7 \hat{\mathbf{x}} - ax_7 \hat{\mathbf{y}} - ax_7 \hat{\mathbf{z}}$	(16e)	Zn III
$\mathbf{B}_{29} =$	$x_8 \mathbf{a}_1 + x_8 \mathbf{a}_2 + x_8 \mathbf{a}_3$	$=$	$ax_8 \hat{\mathbf{x}} + ax_8 \hat{\mathbf{y}} + ax_8 \hat{\mathbf{z}}$	(16e)	Zn IV
$\mathbf{B}_{30} =$	$x_8 \mathbf{a}_1 + x_8 \mathbf{a}_2 - 3x_8 \mathbf{a}_3$	$=$	$-ax_8 \hat{\mathbf{x}} - ax_8 \hat{\mathbf{y}} + ax_8 \hat{\mathbf{z}}$	(16e)	Zn IV
$\mathbf{B}_{31} =$	$x_8 \mathbf{a}_1 - 3x_8 \mathbf{a}_2 + x_8 \mathbf{a}_3$	$=$	$-ax_8 \hat{\mathbf{x}} + ax_8 \hat{\mathbf{y}} - ax_8 \hat{\mathbf{z}}$	(16e)	Zn IV
$\mathbf{B}_{32} =$	$-3x_8 \mathbf{a}_1 + x_8 \mathbf{a}_2 + x_8 \mathbf{a}_3$	$=$	$ax_8 \hat{\mathbf{x}} - ax_8 \hat{\mathbf{y}} - ax_8 \hat{\mathbf{z}}$	(16e)	Zn IV
$\mathbf{B}_{33} =$	$-x_9 \mathbf{a}_1 + x_9 \mathbf{a}_2 + x_9 \mathbf{a}_3$	$=$	$ax_9 \hat{\mathbf{x}}$	(24f)	Pt V
$\mathbf{B}_{34} =$	$x_9 \mathbf{a}_1 - x_9 \mathbf{a}_2 - x_9 \mathbf{a}_3$	$=$	$-ax_9 \hat{\mathbf{x}}$	(24f)	Pt V
$\mathbf{B}_{35} =$	$x_9 \mathbf{a}_1 - x_9 \mathbf{a}_2 + x_9 \mathbf{a}_3$	$=$	$ax_9 \hat{\mathbf{y}}$	(24f)	Pt V
$\mathbf{B}_{36} =$	$-x_9 \mathbf{a}_1 + x_9 \mathbf{a}_2 - x_9 \mathbf{a}_3$	$=$	$-ax_9 \hat{\mathbf{y}}$	(24f)	Pt V
$\mathbf{B}_{37} =$	$x_9 \mathbf{a}_1 + x_9 \mathbf{a}_2 - x_9 \mathbf{a}_3$	$=$	$ax_9 \hat{\mathbf{z}}$	(24f)	Pt V
$\mathbf{B}_{38} =$	$-x_9 \mathbf{a}_1 - x_9 \mathbf{a}_2 + x_9 \mathbf{a}_3$	$=$	$-ax_9 \hat{\mathbf{z}}$	(24f)	Pt V
$\mathbf{B}_{39} =$	$-x_{10} \mathbf{a}_1 + x_{10} \mathbf{a}_2 + x_{10} \mathbf{a}_3$	$=$	$ax_{10} \hat{\mathbf{x}}$	(24f)	Zn V
$\mathbf{B}_{40} =$	$x_{10} \mathbf{a}_1 - x_{10} \mathbf{a}_2 - x_{10} \mathbf{a}_3$	$=$	$-ax_{10} \hat{\mathbf{x}}$	(24f)	Zn V
$\mathbf{B}_{41} =$	$x_{10} \mathbf{a}_1 - x_{10} \mathbf{a}_2 + x_{10} \mathbf{a}_3$	$=$	$ax_{10} \hat{\mathbf{y}}$	(24f)	Zn V
$\mathbf{B}_{42} =$	$-x_{10} \mathbf{a}_1 + x_{10} \mathbf{a}_2 - x_{10} \mathbf{a}_3$	$=$	$-ax_{10} \hat{\mathbf{y}}$	(24f)	Zn V
$\mathbf{B}_{43} =$	$x_{10} \mathbf{a}_1 + x_{10} \mathbf{a}_2 - x_{10} \mathbf{a}_3$	$=$	$ax_{10} \hat{\mathbf{z}}$	(24f)	Zn V
$\mathbf{B}_{44} =$	$-x_{10} \mathbf{a}_1 - x_{10} \mathbf{a}_2 + x_{10} \mathbf{a}_3$	$=$	$-ax_{10} \hat{\mathbf{z}}$	(24f)	Zn V
$\mathbf{B}_{45} =$	$-(x_{11} - \frac{1}{2}) \mathbf{a}_1 + x_{11} \mathbf{a}_2 + x_{11} \mathbf{a}_3$	$=$	$ax_{11} \hat{\mathbf{x}} + \frac{1}{4}a \hat{\mathbf{y}} + \frac{1}{4}a \hat{\mathbf{z}}$	(24g)	Pt VI
$\mathbf{B}_{46} =$	$x_{11} \mathbf{a}_1 - (x_{11} - \frac{1}{2}) \mathbf{a}_2 - (x_{11} - \frac{1}{2}) \mathbf{a}_3$	$=$	$-a(x_{11} - \frac{1}{2}) \hat{\mathbf{x}} + \frac{1}{4}a \hat{\mathbf{y}} + \frac{1}{4}a \hat{\mathbf{z}}$	(24g)	Pt VI
$\mathbf{B}_{47} =$	$x_{11} \mathbf{a}_1 - (x_{11} - \frac{1}{2}) \mathbf{a}_2 + x_{11} \mathbf{a}_3$	$=$	$\frac{1}{4}a \hat{\mathbf{x}} + ax_{11} \hat{\mathbf{y}} + \frac{1}{4}a \hat{\mathbf{z}}$	(24g)	Pt VI
$\mathbf{B}_{48} =$	$-(x_{11} - \frac{1}{2}) \mathbf{a}_1 + x_{11} \mathbf{a}_2 - (x_{11} - \frac{1}{2}) \mathbf{a}_3$	$=$	$\frac{1}{4}a \hat{\mathbf{x}} - a(x_{11} - \frac{1}{2}) \hat{\mathbf{y}} + \frac{1}{4}a \hat{\mathbf{z}}$	(24g)	Pt VI
$\mathbf{B}_{49} =$	$x_{11} \mathbf{a}_1 + x_{11} \mathbf{a}_2 - (x_{11} - \frac{1}{2}) \mathbf{a}_3$	$=$	$\frac{1}{4}a \hat{\mathbf{x}} + \frac{1}{4}a \hat{\mathbf{y}} + ax_{11} \hat{\mathbf{z}}$	(24g)	Pt VI
$\mathbf{B}_{50} =$	$-(x_{11} - \frac{1}{2}) \mathbf{a}_1 - (x_{11} - \frac{1}{2}) \mathbf{a}_2 + x_{11} \mathbf{a}_3$	$=$	$\frac{1}{4}a \hat{\mathbf{x}} + \frac{1}{4}a \hat{\mathbf{y}} - a(x_{11} - \frac{1}{2}) \hat{\mathbf{z}}$	(24g)	Pt VI
$\mathbf{B}_{51} =$	$z_{12} \mathbf{a}_1 + z_{12} \mathbf{a}_2 + (2x_{12} - z_{12}) \mathbf{a}_3$	$=$	$az_{12} \hat{\mathbf{x}} + az_{12} \hat{\mathbf{y}} + az_{12} \hat{\mathbf{z}}$	(48h)	Zn VI
$\mathbf{B}_{52} =$	$z_{12} \mathbf{a}_1 + z_{12} \mathbf{a}_2 - (2x_{12} + z_{12}) \mathbf{a}_3$	$=$	$-az_{12} \hat{\mathbf{x}} - az_{12} \hat{\mathbf{y}} + az_{12} \hat{\mathbf{z}}$	(48h)	Zn VI
$\mathbf{B}_{53} =$	$(2x_{12} - z_{12}) \mathbf{a}_1 - (2x_{12} + z_{12}) \mathbf{a}_2 + z_{12} \mathbf{a}_3$	$=$	$-az_{12} \hat{\mathbf{x}} + az_{12} \hat{\mathbf{y}} - az_{12} \hat{\mathbf{z}}$	(48h)	Zn VI
$\mathbf{B}_{54} =$	$-(2x_{12} + z_{12}) \mathbf{a}_1 + (2x_{12} - z_{12}) \mathbf{a}_2 + z_{12} \mathbf{a}_3$	$=$	$az_{12} \hat{\mathbf{x}} - az_{12} \hat{\mathbf{y}} - az_{12} \hat{\mathbf{z}}$	(48h)	Zn VI
$\mathbf{B}_{55} =$	$(2x_{12} - z_{12}) \mathbf{a}_1 + z_{12} \mathbf{a}_2 + z_{12} \mathbf{a}_3$	$=$	$az_{12} \hat{\mathbf{x}} + az_{12} \hat{\mathbf{y}} + az_{12} \hat{\mathbf{z}}$	(48h)	Zn VI
$\mathbf{B}_{56} =$	$-(2x_{12} + z_{12}) \mathbf{a}_1 + z_{12} \mathbf{a}_2 + z_{12} \mathbf{a}_3$	$=$	$az_{12} \hat{\mathbf{x}} - az_{12} \hat{\mathbf{y}} - az_{12} \hat{\mathbf{z}}$	(48h)	Zn VI
$\mathbf{B}_{57} =$	$z_{12} \mathbf{a}_1 + (2x_{12} - z_{12}) \mathbf{a}_2 - (2x_{12} + z_{12}) \mathbf{a}_3$	$=$	$-az_{12} \hat{\mathbf{x}} - az_{12} \hat{\mathbf{y}} + az_{12} \hat{\mathbf{z}}$	(48h)	Zn VI
$\mathbf{B}_{58} =$	$z_{12} \mathbf{a}_1 - (2x_{12} + z_{12}) \mathbf{a}_2 + (2x_{12} - z_{12}) \mathbf{a}_3$	$=$	$-az_{12} \hat{\mathbf{x}} + az_{12} \hat{\mathbf{y}} - az_{12} \hat{\mathbf{z}}$	(48h)	Zn VI

B₈₉	$(2x_{15} - z_{15}) \mathbf{a}_1 -$ $(2x_{15} + z_{15}) \mathbf{a}_2 + z_{15} \mathbf{a}_3$	=	$-ax_{15} \hat{\mathbf{x}} + ax_{15} \hat{\mathbf{y}} - az_{15} \hat{\mathbf{z}}$	(48h)	Zn IX
B₉₀	$-(2x_{15} + z_{15}) \mathbf{a}_1 +$ $(2x_{15} - z_{15}) \mathbf{a}_2 + z_{15} \mathbf{a}_3$	=	$ax_{15} \hat{\mathbf{x}} - ax_{15} \hat{\mathbf{y}} - az_{15} \hat{\mathbf{z}}$	(48h)	Zn IX
B₉₁	$(2x_{15} - z_{15}) \mathbf{a}_1 + z_{15} \mathbf{a}_2 + z_{15} \mathbf{a}_3$	=	$az_{15} \hat{\mathbf{x}} + ax_{15} \hat{\mathbf{y}} + ax_{15} \hat{\mathbf{z}}$	(48h)	Zn IX
B₉₂	$-(2x_{15} + z_{15}) \mathbf{a}_1 + z_{15} \mathbf{a}_2 + z_{15} \mathbf{a}_3$	=	$az_{15} \hat{\mathbf{x}} - ax_{15} \hat{\mathbf{y}} - ax_{15} \hat{\mathbf{z}}$	(48h)	Zn IX
B₉₃	$z_{15} \mathbf{a}_1 + (2x_{15} - z_{15}) \mathbf{a}_2 -$ $(2x_{15} + z_{15}) \mathbf{a}_3$	=	$-az_{15} \hat{\mathbf{x}} - ax_{15} \hat{\mathbf{y}} + ax_{15} \hat{\mathbf{z}}$	(48h)	Zn IX
B₉₄	$z_{15} \mathbf{a}_1 - (2x_{15} + z_{15}) \mathbf{a}_2 +$ $(2x_{15} - z_{15}) \mathbf{a}_3$	=	$-az_{15} \hat{\mathbf{x}} + ax_{15} \hat{\mathbf{y}} - ax_{15} \hat{\mathbf{z}}$	(48h)	Zn IX
B₉₅	$z_{15} \mathbf{a}_1 + (2x_{15} - z_{15}) \mathbf{a}_2 + z_{15} \mathbf{a}_3$	=	$ax_{15} \hat{\mathbf{x}} + az_{15} \hat{\mathbf{y}} + ax_{15} \hat{\mathbf{z}}$	(48h)	Zn IX
B₉₆	$z_{15} \mathbf{a}_1 - (2x_{15} + z_{15}) \mathbf{a}_2 + z_{15} \mathbf{a}_3$	=	$-ax_{15} \hat{\mathbf{x}} + az_{15} \hat{\mathbf{y}} - ax_{15} \hat{\mathbf{z}}$	(48h)	Zn IX
B₉₇	$-(2x_{15} + z_{15}) \mathbf{a}_1 + z_{15} \mathbf{a}_2 +$ $(2x_{15} - z_{15}) \mathbf{a}_3$	=	$ax_{15} \hat{\mathbf{x}} - az_{15} \hat{\mathbf{y}} - ax_{15} \hat{\mathbf{z}}$	(48h)	Zn IX
B₉₈	$(2x_{15} - z_{15}) \mathbf{a}_1 + z_{15} \mathbf{a}_2 -$ $(2x_{15} + z_{15}) \mathbf{a}_3$	=	$-ax_{15} \hat{\mathbf{x}} - az_{15} \hat{\mathbf{y}} + ax_{15} \hat{\mathbf{z}}$	(48h)	Zn IX

References

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