

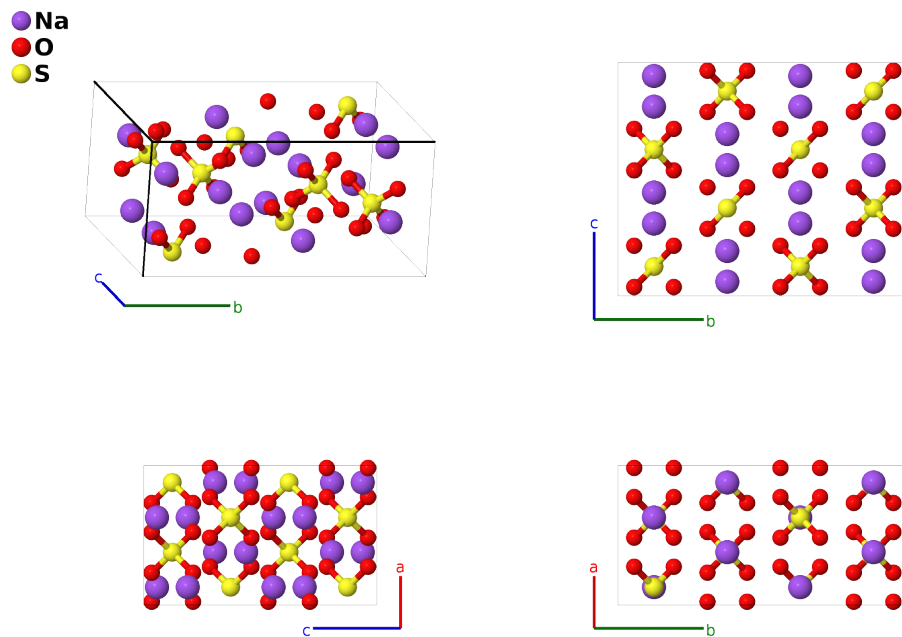
# Thenardite [Na<sub>2</sub>SO<sub>4</sub> (V), *H*1<sub>7</sub>] Structure: A2B4C\_oF56\_70\_e\_h\_a-001

This structure originally had the label A2B4C\_oF56\_70\_g\_h\_a. Calls to that address will be redirected here.

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<https://afLOW.org/p/8CBQ>

[https://afLOW.org/p/A2B4C\\_oF56\\_70\\_e\\_h\\_a-001](https://afLOW.org/p/A2B4C_oF56_70_e_h_a-001)



Prototype	Na <sub>2</sub> O <sub>4</sub> S
AFLOW prototype label	A2B4C_oF56_70_e_h_a-001
<i>Strukturbericht</i> designation	<i>H</i> 1 <sub>7</sub>
Mineral name	thenardite
ICSD	2895
Pearson symbol	oF56
Space group number	70
Space group symbol	<i>Fddd</i>
AFLOW prototype command	<code>afLOW --proto=A2B4C_oF56_70_e_h_a-001 --params=a, b/a, c/a, x<sub>2</sub>, x<sub>3</sub>, y<sub>3</sub>, z<sub>3</sub></code>

## Other compounds with this structure

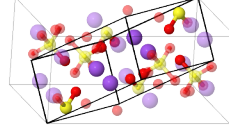
Ag<sub>2</sub>SO<sub>4</sub>, Cr<sub>2</sub>SO<sub>4</sub>

- $\text{Na}_2\text{SO}_4$  has eight known anhydrous phases. The thenardite phase is “reported to be stable between 32°C and about 180°C” (Nord, 1973), however the data reported here was taken on synthetic thenardite at 25°C.

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### Face-centered Orthorhombic primitive vectors

$$\begin{aligned}\mathbf{a}_1 &= \frac{1}{2}b\hat{\mathbf{y}} + \frac{1}{2}c\hat{\mathbf{z}} \\ \mathbf{a}_2 &= \frac{1}{2}a\hat{\mathbf{x}} + \frac{1}{2}c\hat{\mathbf{z}} \\ \mathbf{a}_3 &= \frac{1}{2}a\hat{\mathbf{x}} + \frac{1}{2}b\hat{\mathbf{y}}\end{aligned}$$




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### Basis vectors

	Lattice coordinates		Cartesian coordinates	Wyckoff position	Atom type
$\mathbf{B}_1$	$= \frac{1}{8}\mathbf{a}_1 + \frac{1}{8}\mathbf{a}_2 + \frac{1}{8}\mathbf{a}_3$	$=$	$\frac{1}{8}a\hat{\mathbf{x}} + \frac{1}{8}b\hat{\mathbf{y}} + \frac{1}{8}c\hat{\mathbf{z}}$	(8a)	S I
$\mathbf{B}_2$	$= \frac{7}{8}\mathbf{a}_1 + \frac{7}{8}\mathbf{a}_2 + \frac{7}{8}\mathbf{a}_3$	$=$	$\frac{7}{8}a\hat{\mathbf{x}} + \frac{7}{8}b\hat{\mathbf{y}} + \frac{7}{8}c\hat{\mathbf{z}}$	(8a)	S I
$\mathbf{B}_3$	$= -(x_2 - \frac{1}{4})\mathbf{a}_1 + x_2\mathbf{a}_2 + x_2\mathbf{a}_3$	$=$	$ax_2\hat{\mathbf{x}} + \frac{1}{8}b\hat{\mathbf{y}} + \frac{1}{8}c\hat{\mathbf{z}}$	(16e)	Na I
$\mathbf{B}_4$	$= x_2\mathbf{a}_1 - (x_2 - \frac{1}{4})\mathbf{a}_2 - (x_2 - \frac{1}{4})\mathbf{a}_3$	$=$	$-a(x_2 - \frac{1}{4})\hat{\mathbf{x}} + \frac{1}{8}b\hat{\mathbf{y}} + \frac{1}{8}c\hat{\mathbf{z}}$	(16e)	Na I
$\mathbf{B}_5$	$= (x_2 + \frac{3}{4})\mathbf{a}_1 - x_2\mathbf{a}_2 - x_2\mathbf{a}_3$	$=$	$-ax_2\hat{\mathbf{x}} + \frac{3}{8}b\hat{\mathbf{y}} + \frac{3}{8}c\hat{\mathbf{z}}$	(16e)	Na I
$\mathbf{B}_6$	$= -x_2\mathbf{a}_1 + (x_2 + \frac{3}{4})\mathbf{a}_2 + (x_2 + \frac{3}{4})\mathbf{a}_3$	$=$	$a(x_2 + \frac{3}{4})\hat{\mathbf{x}} + \frac{3}{8}b\hat{\mathbf{y}} + \frac{3}{8}c\hat{\mathbf{z}}$	(16e)	Na I
$\mathbf{B}_7$	$= (-x_3 + y_3 + z_3)\mathbf{a}_1 + (x_3 - y_3 + z_3)\mathbf{a}_2 + (x_3 + y_3 - z_3)\mathbf{a}_3$	$=$	$ax_3\hat{\mathbf{x}} + by_3\hat{\mathbf{y}} + cz_3\hat{\mathbf{z}}$	(32h)	O I
$\mathbf{B}_8$	$= (x_3 - y_3 + z_3)\mathbf{a}_1 + (-x_3 + y_3 + z_3)\mathbf{a}_2 - (x_3 + y_3 + z_3 - \frac{1}{2})\mathbf{a}_3$	$=$	$-a(x_3 - \frac{1}{4})\hat{\mathbf{x}} - b(y_3 - \frac{1}{4})\hat{\mathbf{y}} + cz_3\hat{\mathbf{z}}$	(32h)	O I
$\mathbf{B}_9$	$= (x_3 + y_3 - z_3)\mathbf{a}_1 - (x_3 + y_3 + z_3 - \frac{1}{2})\mathbf{a}_2 + (-x_3 + y_3 + z_3)\mathbf{a}_3$	$=$	$-a(x_3 - \frac{1}{4})\hat{\mathbf{x}} + by_3\hat{\mathbf{y}} - c(z_3 - \frac{1}{4})\hat{\mathbf{z}}$	(32h)	O I
$\mathbf{B}_{10}$	$= -(x_3 + y_3 + z_3 - \frac{1}{2})\mathbf{a}_1 + (x_3 + y_3 - z_3)\mathbf{a}_2 + (x_3 - y_3 + z_3)\mathbf{a}_3$	$=$	$ax_3\hat{\mathbf{x}} - b(y_3 - \frac{1}{4})\hat{\mathbf{y}} - c(z_3 - \frac{1}{4})\hat{\mathbf{z}}$	(32h)	O I
$\mathbf{B}_{11}$	$= (x_3 - y_3 - z_3)\mathbf{a}_1 - (x_3 - y_3 + z_3)\mathbf{a}_2 - (x_3 + y_3 - z_3)\mathbf{a}_3$	$=$	$-ax_3\hat{\mathbf{x}} - by_3\hat{\mathbf{y}} - cz_3\hat{\mathbf{z}}$	(32h)	O I
$\mathbf{B}_{12}$	$= -(x_3 - y_3 + z_3)\mathbf{a}_1 + (x_3 - y_3 - z_3)\mathbf{a}_2 + (x_3 + y_3 + z_3 + \frac{1}{2})\mathbf{a}_3$	$=$	$a(x_3 + \frac{1}{4})\hat{\mathbf{x}} + b(y_3 + \frac{1}{4})\hat{\mathbf{y}} - cz_3\hat{\mathbf{z}}$	(32h)	O I
$\mathbf{B}_{13}$	$= -(x_3 + y_3 - z_3)\mathbf{a}_1 + (x_3 + y_3 + z_3 + \frac{1}{2})\mathbf{a}_2 + (x_3 - y_3 - z_3)\mathbf{a}_3$	$=$	$a(x_3 + \frac{1}{4})\hat{\mathbf{x}} - by_3\hat{\mathbf{y}} + c(z_3 + \frac{1}{4})\hat{\mathbf{z}}$	(32h)	O I
$\mathbf{B}_{14}$	$= (x_3 + y_3 + z_3 + \frac{1}{2})\mathbf{a}_1 - (x_3 + y_3 - z_3)\mathbf{a}_2 - (x_3 - y_3 + z_3)\mathbf{a}_3$	$=$	$-ax_3\hat{\mathbf{x}} + b(y_3 + \frac{1}{4})\hat{\mathbf{y}} + c(z_3 + \frac{1}{4})\hat{\mathbf{z}}$	(32h)	O I

## References

- [1] A. C. Nord, *Refinement of the Crystal Structure of Thenardite  $\text{Na}_2\text{SO}_4$  (V)*, Acta Chem. Scand. **27**, 814–822 (1973).