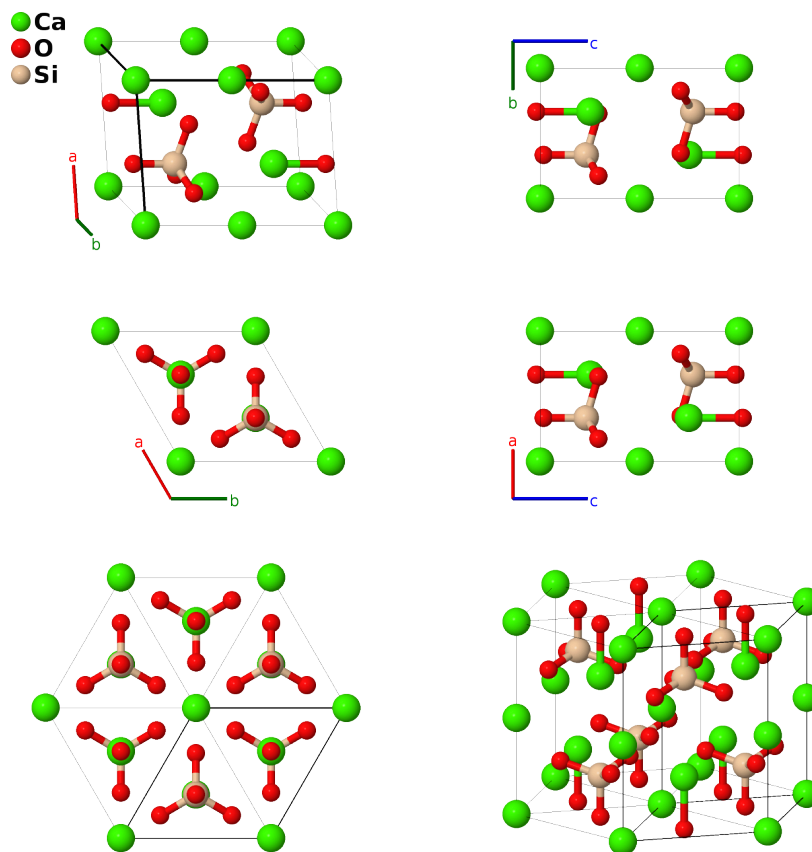


Trigonal α -Ca₂SiO₄ Structure: A2B4C_hP14_164_abd_di_d-001

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<https://aflow.org/p/DBUP>

https://aflow.org/p/A2B4C_hP14_164_abd_di_d-001



Prototype	Ca ₂ O ₄ Si
AFLOW prototype label	A2B4C_hP14_164_abd_di_d-001
ICSD	182052
Pearson symbol	hP14
Space group number	164
Space group symbol	$P\bar{3}m1$
AFLOW prototype command	<code>aflow --proto=A2B4C_hP14_164_abd_di_d-001 --params=a, c/a, z₃, z₄, z₅, x₆, z₆</code>

- Ca₂SiO₄ exists in a variety of structures (Mumme, 1996; Yamnova, 2011):
 - hexagonal α -Ca₂SiO₄, stable above 1445°C. There is some dispute as to whether this occurs in a

* trigonal, space group $P\bar{3}m1$ #164 structure (shown here) or a

* disordered hexagonal, space group $P6_3/mmc$ #194 structure.

– orthorhombic α_H '-Ca₂SiO₄, stable in the range 1160 – 1425°C,

– orthorhombic α_L '-Ca₂SiO₄, stable in the range 690 – 1160°C,

– monoclinic β -Ca₂SiO₄, stable in the range 500 – 690°C and found in nature as the metastable mineral larnite, and

– γ -Ca₂SiO₄, stable below 500°C, in the olivine ($S1_2$) structure.

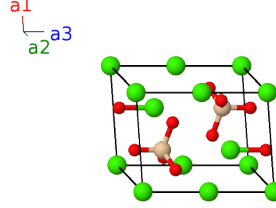
- The ICSD entry for this structure is from (Eysel, 1970). The atomic positions are significantly different than those given in (Mumme, 1996), but we have no ICSD entry from that paper.

Trigonal (Hexagonal) primitive vectors

$$\mathbf{a}_1 = \frac{1}{2}a \hat{\mathbf{x}} - \frac{\sqrt{3}}{2}a \hat{\mathbf{y}}$$

$$\mathbf{a}_2 = \frac{1}{2}a \hat{\mathbf{x}} + \frac{\sqrt{3}}{2}a \hat{\mathbf{y}}$$

$$\mathbf{a}_3 = c \hat{\mathbf{z}}$$



Basis vectors

	Lattice coordinates		Cartesian coordinates	Wyckoff position	Atom type
\mathbf{B}_1	=	0	=	0	(1a) Ca I
\mathbf{B}_2	=	$\frac{1}{2} \mathbf{a}_3$	=	$\frac{1}{2} c \hat{\mathbf{z}}$	(1b) Ca II
\mathbf{B}_3	=	$\frac{1}{3} \mathbf{a}_1 + \frac{2}{3} \mathbf{a}_2 + z_3 \mathbf{a}_3$	=	$\frac{1}{2} a \hat{\mathbf{x}} + \frac{\sqrt{3}}{6} a \hat{\mathbf{y}} + cz_3 \hat{\mathbf{z}}$	(2d) Ca III
\mathbf{B}_4	=	$\frac{2}{3} \mathbf{a}_1 + \frac{1}{3} \mathbf{a}_2 - z_3 \mathbf{a}_3$	=	$\frac{1}{2} a \hat{\mathbf{x}} - \frac{\sqrt{3}}{6} a \hat{\mathbf{y}} - cz_3 \hat{\mathbf{z}}$	(2d) Ca III
\mathbf{B}_5	=	$\frac{1}{3} \mathbf{a}_1 + \frac{2}{3} \mathbf{a}_2 + z_4 \mathbf{a}_3$	=	$\frac{1}{2} a \hat{\mathbf{x}} + \frac{\sqrt{3}}{6} a \hat{\mathbf{y}} + cz_4 \hat{\mathbf{z}}$	(2d) O I
\mathbf{B}_6	=	$\frac{2}{3} \mathbf{a}_1 + \frac{1}{3} \mathbf{a}_2 - z_4 \mathbf{a}_3$	=	$\frac{1}{2} a \hat{\mathbf{x}} - \frac{\sqrt{3}}{6} a \hat{\mathbf{y}} - cz_4 \hat{\mathbf{z}}$	(2d) O I
\mathbf{B}_7	=	$\frac{1}{3} \mathbf{a}_1 + \frac{2}{3} \mathbf{a}_2 + z_5 \mathbf{a}_3$	=	$\frac{1}{2} a \hat{\mathbf{x}} + \frac{\sqrt{3}}{6} a \hat{\mathbf{y}} + cz_5 \hat{\mathbf{z}}$	(2d) Si I
\mathbf{B}_8	=	$\frac{2}{3} \mathbf{a}_1 + \frac{1}{3} \mathbf{a}_2 - z_5 \mathbf{a}_3$	=	$\frac{1}{2} a \hat{\mathbf{x}} - \frac{\sqrt{3}}{6} a \hat{\mathbf{y}} - cz_5 \hat{\mathbf{z}}$	(2d) Si I
\mathbf{B}_9	=	$x_6 \mathbf{a}_1 - x_6 \mathbf{a}_2 + z_6 \mathbf{a}_3$	=	$-\sqrt{3}ax_6 \hat{\mathbf{y}} + cz_6 \hat{\mathbf{z}}$	(6i) O II
\mathbf{B}_{10}	=	$x_6 \mathbf{a}_1 + 2x_6 \mathbf{a}_2 + z_6 \mathbf{a}_3$	=	$\frac{3}{2}ax_6 \hat{\mathbf{x}} + \frac{\sqrt{3}}{2}ax_6 \hat{\mathbf{y}} + cz_6 \hat{\mathbf{z}}$	(6i) O II
\mathbf{B}_{11}	=	$-2x_6 \mathbf{a}_1 - x_6 \mathbf{a}_2 + z_6 \mathbf{a}_3$	=	$-\frac{3}{2}ax_6 \hat{\mathbf{x}} + \frac{\sqrt{3}}{2}ax_6 \hat{\mathbf{y}} + cz_6 \hat{\mathbf{z}}$	(6i) O II
\mathbf{B}_{12}	=	$-x_6 \mathbf{a}_1 + x_6 \mathbf{a}_2 - z_6 \mathbf{a}_3$	=	$\sqrt{3}ax_6 \hat{\mathbf{y}} - cz_6 \hat{\mathbf{z}}$	(6i) O II
\mathbf{B}_{13}	=	$2x_6 \mathbf{a}_1 + x_6 \mathbf{a}_2 - z_6 \mathbf{a}_3$	=	$\frac{3}{2}ax_6 \hat{\mathbf{x}} - \frac{\sqrt{3}}{2}ax_6 \hat{\mathbf{y}} - cz_6 \hat{\mathbf{z}}$	(6i) O II
\mathbf{B}_{14}	=	$-x_6 \mathbf{a}_1 - 2x_6 \mathbf{a}_2 - z_6 \mathbf{a}_3$	=	$-\frac{3}{2}ax_6 \hat{\mathbf{x}} - \frac{\sqrt{3}}{2}ax_6 \hat{\mathbf{y}} - cz_6 \hat{\mathbf{z}}$	(6i) O II

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