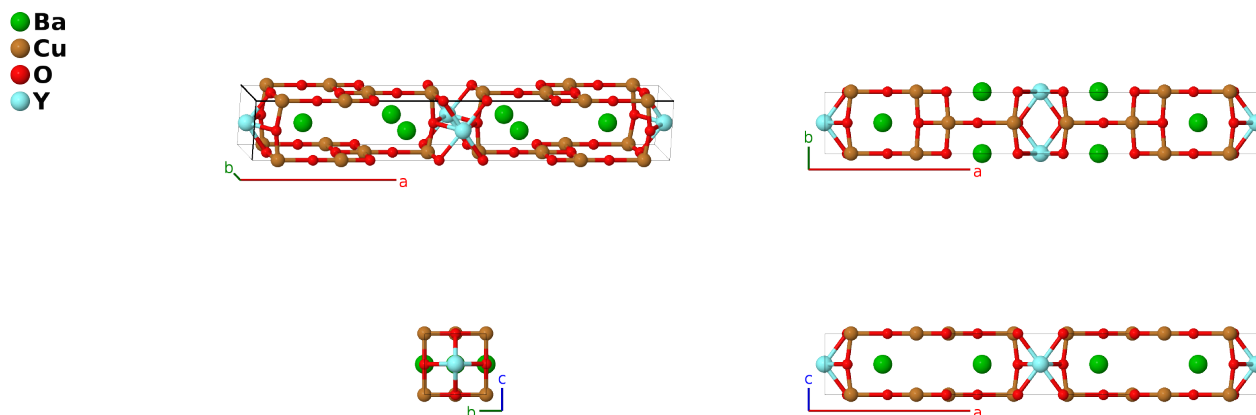


“124 Superconductor” (YBa₂Cu₄O₈) Structure: A2B4C8D_oC30_65_h_2g_3gh_c-001

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<https://afLOW.org/p/2EBJ>

https://afLOW.org/p/A2B4C8D_oC30_65_h_2g_3gh_c-001



Prototype	Ba ₂ Cu ₄ O ₈ Y
AFLOW prototype label	A2B4C8D_oC30_65_h_2g_3gh_c-001
ICSD	none
Pearson symbol	oC30
Space group number	65
Space group symbol	<i>Cmmm</i>
AFLOW prototype command	<code>afLOW --proto=A2B4C8D_oC30_65_h_2g_3gh_c-001 --params=a, b/a, c/a, x₂, x₃, x₄, x₅, x₆, x₇, x₈</code>

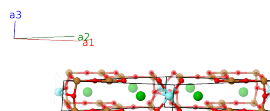
- Unlike most BCO-type superconductors, the stoichiometry of YBa₂Cu₄O₈ is fixed.
- We use the ambient pressure data from (Bordet, 1989) taken at room temperature.
- Although it is never explicitly stated by (Bordet, 1989), (Nelmes, 1990) notes that this data is given in the *Ammm* setting of space group #65, making the long axis in the *z*-direction. The standard orientation is *Cmmm*, and we use FINDSYM to rotate the structure, putting the long axis in the *x*-direction.

Base-centered Orthorhombic primitive vectors

$$\mathbf{a}_1 = \frac{1}{2}a \hat{x} - \frac{1}{2}b \hat{y}$$

$$\mathbf{a}_2 = \frac{1}{2}a \hat{x} + \frac{1}{2}b \hat{y}$$

$$\mathbf{a}_3 = c \hat{z}$$



Basis vectors

	Lattice coordinates		Cartesian coordinates	Wyckoff position	Atom type
\mathbf{B}_1	$=$	$\frac{1}{2} \mathbf{a}_1 + \frac{1}{2} \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	$=$	$\frac{1}{2}a \hat{\mathbf{x}} + \frac{1}{2}c \hat{\mathbf{z}}$	(2c) Y I
\mathbf{B}_2	$=$	$x_2 \mathbf{a}_1 + x_2 \mathbf{a}_2$	$=$	$ax_2 \hat{\mathbf{x}}$	(4g) Cu I
\mathbf{B}_3	$=$	$-x_2 \mathbf{a}_1 - x_2 \mathbf{a}_2$	$=$	$-ax_2 \hat{\mathbf{x}}$	(4g) Cu I
\mathbf{B}_4	$=$	$x_3 \mathbf{a}_1 + x_3 \mathbf{a}_2$	$=$	$ax_3 \hat{\mathbf{x}}$	(4g) Cu II
\mathbf{B}_5	$=$	$-x_3 \mathbf{a}_1 - x_3 \mathbf{a}_2$	$=$	$-ax_3 \hat{\mathbf{x}}$	(4g) Cu II
\mathbf{B}_6	$=$	$x_4 \mathbf{a}_1 + x_4 \mathbf{a}_2$	$=$	$ax_4 \hat{\mathbf{x}}$	(4g) O I
\mathbf{B}_7	$=$	$-x_4 \mathbf{a}_1 - x_4 \mathbf{a}_2$	$=$	$-ax_4 \hat{\mathbf{x}}$	(4g) O I
\mathbf{B}_8	$=$	$x_5 \mathbf{a}_1 + x_5 \mathbf{a}_2$	$=$	$ax_5 \hat{\mathbf{x}}$	(4g) O II
\mathbf{B}_9	$=$	$-x_5 \mathbf{a}_1 - x_5 \mathbf{a}_2$	$=$	$-ax_5 \hat{\mathbf{x}}$	(4g) O II
\mathbf{B}_{10}	$=$	$x_6 \mathbf{a}_1 + x_6 \mathbf{a}_2$	$=$	$ax_6 \hat{\mathbf{x}}$	(4g) O III
\mathbf{B}_{11}	$=$	$-x_6 \mathbf{a}_1 - x_6 \mathbf{a}_2$	$=$	$-ax_6 \hat{\mathbf{x}}$	(4g) O III
\mathbf{B}_{12}	$=$	$x_7 \mathbf{a}_1 + x_7 \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	$=$	$ax_7 \hat{\mathbf{x}} + \frac{1}{2}c \hat{\mathbf{z}}$	(4h) Ba I
\mathbf{B}_{13}	$=$	$-x_7 \mathbf{a}_1 - x_7 \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	$=$	$-ax_7 \hat{\mathbf{x}} + \frac{1}{2}c \hat{\mathbf{z}}$	(4h) Ba I
\mathbf{B}_{14}	$=$	$x_8 \mathbf{a}_1 + x_8 \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	$=$	$ax_8 \hat{\mathbf{x}} + \frac{1}{2}c \hat{\mathbf{z}}$	(4h) O IV
\mathbf{B}_{15}	$=$	$-x_8 \mathbf{a}_1 - x_8 \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	$=$	$-ax_8 \hat{\mathbf{x}} + \frac{1}{2}c \hat{\mathbf{z}}$	(4h) O IV

References

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