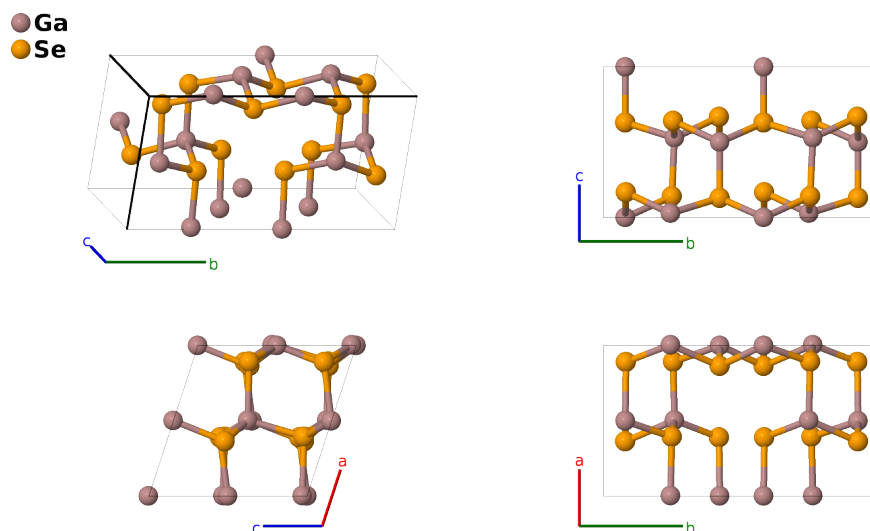


# Room Temperature Ga<sub>2</sub>Se<sub>3</sub> Structure: A2B3\_mC20\_9\_2a\_3a-001

Cite this page as: H. Eckert, S. Divilov, A. Zettel, M. J. Mehl, D. Hicks, and S. Curtarolo, *The AFLOW Library of Crystallographic Prototypes: Part 4*. In preparation.

<https://aflow.org/p/4F67>

[https://aflow.org/p/A2B3\\_mC20\\_9\\_2a\\_3a-001](https://aflow.org/p/A2B3_mC20_9_2a_3a-001)



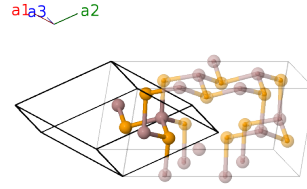
<b>Prototype</b>	Ga <sub>2</sub> Se <sub>3</sub>
<b>AFLOW prototype label</b>	A2B3_mC20_9_2a_3a-001
<b>ICSD</b>	635356
<b>Pearson symbol</b>	mC20
<b>Space group number</b>	9
<b>Space group symbol</b>	<i>Cc</i>
<b>AFLOW prototype command</b>	<code>aflow --proto=A2B3_mC20_9_2a_3a-001 --params=a, b/a, c/a, <math>\beta</math>, <math>x_1, y_1, z_1, x_2, y_2, z_2, x_3, y_3, z_3, x_4, y_4, z_4, x_5, y_5, z_5</math></code>

## Other compounds with this structure

Ga<sub>2</sub>S<sub>3</sub>

- Above 645-694K (Villars, 2018) this structure transforms to the cubic zincblende (*B3*) phase, with vacancies on the gallium sites to adjust the symmetry (Lübbbers, 1982).
- (Ghémard, 1983) give this structure in the “unique axis-*c*” setting of space group #9. We used FINDSYM to transform this to the standard “unique axis-*b*” setting.

## Base-centered Monoclinic primitive vectors



$$\begin{aligned}\mathbf{a}_1 &= \frac{1}{2}a\hat{\mathbf{x}} - \frac{1}{2}b\hat{\mathbf{y}} \\ \mathbf{a}_2 &= \frac{1}{2}a\hat{\mathbf{x}} + \frac{1}{2}b\hat{\mathbf{y}} \\ \mathbf{a}_3 &= c\cos\beta\hat{\mathbf{x}} + c\sin\beta\hat{\mathbf{z}}\end{aligned}$$

## Basis vectors

	Lattice coordinates		Cartesian coordinates	Wyckoff position	Atom type
$\mathbf{B}_1$	$(x_1 - y_1)\mathbf{a}_1 + (x_1 + y_1)\mathbf{a}_2 + z_1\mathbf{a}_3$	=	$(ax_1 + cz_1\cos\beta)\hat{\mathbf{x}} + by_1\hat{\mathbf{y}} + cz_1\sin\beta\hat{\mathbf{z}}$	(4a)	Ga I
$\mathbf{B}_2$	$(x_1 + y_1)\mathbf{a}_1 + (x_1 - y_1)\mathbf{a}_2 + (z_1 + \frac{1}{2})\mathbf{a}_3$	=	$(ax_1 + c(z_1 + \frac{1}{2})\cos\beta)\hat{\mathbf{x}} - by_1\hat{\mathbf{y}} + c(z_1 + \frac{1}{2})\sin\beta\hat{\mathbf{z}}$	(4a)	Ga I
$\mathbf{B}_3$	$(x_2 - y_2)\mathbf{a}_1 + (x_2 + y_2)\mathbf{a}_2 + z_2\mathbf{a}_3$	=	$(ax_2 + cz_2\cos\beta)\hat{\mathbf{x}} + by_2\hat{\mathbf{y}} + cz_2\sin\beta\hat{\mathbf{z}}$	(4a)	Ga II
$\mathbf{B}_4$	$(x_2 + y_2)\mathbf{a}_1 + (x_2 - y_2)\mathbf{a}_2 + (z_2 + \frac{1}{2})\mathbf{a}_3$	=	$(ax_2 + c(z_2 + \frac{1}{2})\cos\beta)\hat{\mathbf{x}} - by_2\hat{\mathbf{y}} + c(z_2 + \frac{1}{2})\sin\beta\hat{\mathbf{z}}$	(4a)	Ga II
$\mathbf{B}_5$	$(x_3 - y_3)\mathbf{a}_1 + (x_3 + y_3)\mathbf{a}_2 + z_3\mathbf{a}_3$	=	$(ax_3 + cz_3\cos\beta)\hat{\mathbf{x}} + by_3\hat{\mathbf{y}} + cz_3\sin\beta\hat{\mathbf{z}}$	(4a)	Se I
$\mathbf{B}_6$	$(x_3 + y_3)\mathbf{a}_1 + (x_3 - y_3)\mathbf{a}_2 + (z_3 + \frac{1}{2})\mathbf{a}_3$	=	$(ax_3 + c(z_3 + \frac{1}{2})\cos\beta)\hat{\mathbf{x}} - by_3\hat{\mathbf{y}} + c(z_3 + \frac{1}{2})\sin\beta\hat{\mathbf{z}}$	(4a)	Se I
$\mathbf{B}_7$	$(x_4 - y_4)\mathbf{a}_1 + (x_4 + y_4)\mathbf{a}_2 + z_4\mathbf{a}_3$	=	$(ax_4 + cz_4\cos\beta)\hat{\mathbf{x}} + by_4\hat{\mathbf{y}} + cz_4\sin\beta\hat{\mathbf{z}}$	(4a)	Se II
$\mathbf{B}_8$	$(x_4 + y_4)\mathbf{a}_1 + (x_4 - y_4)\mathbf{a}_2 + (z_4 + \frac{1}{2})\mathbf{a}_3$	=	$(ax_4 + c(z_4 + \frac{1}{2})\cos\beta)\hat{\mathbf{x}} - by_4\hat{\mathbf{y}} + c(z_4 + \frac{1}{2})\sin\beta\hat{\mathbf{z}}$	(4a)	Se II
$\mathbf{B}_9$	$(x_5 - y_5)\mathbf{a}_1 + (x_5 + y_5)\mathbf{a}_2 + z_5\mathbf{a}_3$	=	$(ax_5 + cz_5\cos\beta)\hat{\mathbf{x}} + by_5\hat{\mathbf{y}} + cz_5\sin\beta\hat{\mathbf{z}}$	(4a)	Se III
$\mathbf{B}_{10}$	$(x_5 + y_5)\mathbf{a}_1 + (x_5 - y_5)\mathbf{a}_2 + (z_5 + \frac{1}{2})\mathbf{a}_3$	=	$(ax_5 + c(z_5 + \frac{1}{2})\cos\beta)\hat{\mathbf{x}} - by_5\hat{\mathbf{y}} + c(z_5 + \frac{1}{2})\sin\beta\hat{\mathbf{z}}$	(4a)	Se III

## References

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