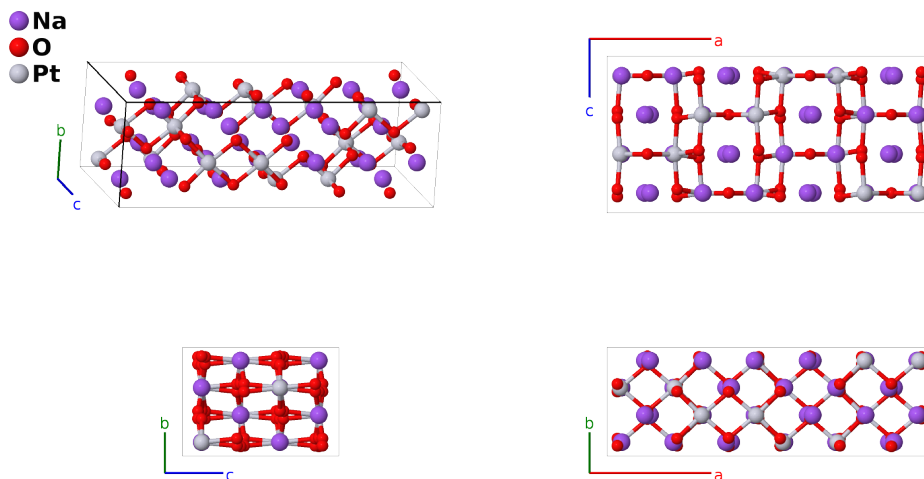


β -Na₂PtO₃ Structure: A2B3C_oF96_70_2e_fh_e-001

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<https://aflow.org/p/7WUP>

https://aflow.org/p/A2B3C_oF96_70_2e_fh_e-001



Prototype	Na ₂ O ₃ Pt
AFLOW prototype label	A2B3C_oF96_70_2e_fh_e-001
ICSD	25020
Pearson symbol	oF96
Space group number	70
Space group symbol	<i>Fddd</i>
AFLOW prototype command	aflow --proto=A2B3C_oF96_70_2e_fh_e-001 --params=a, b/a, c/a, x ₁ , x ₂ , x ₃ , y ₄ , x ₅ , y ₅ , z ₅

Other compounds with this structure

β -Li₂IrO₃

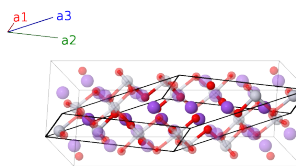
- Na₂PtO₃ can also be found in the α -Na₂PtO₃ phase, which has the Li₂SnO₃ structure.

Face-centered Orthorhombic primitive vectors

$$\mathbf{a}_1 = \frac{1}{2}b\hat{\mathbf{y}} + \frac{1}{2}c\hat{\mathbf{z}}$$

$$\mathbf{a}_2 = \frac{1}{2}a\hat{\mathbf{x}} + \frac{1}{2}c\hat{\mathbf{z}}$$

$$\mathbf{a}_3 = \frac{1}{2}a\hat{\mathbf{x}} + \frac{1}{2}b\hat{\mathbf{y}}$$



Basis vectors

	Lattice coordinates		Cartesian coordinates	Wyckoff position	Atom type
\mathbf{B}_1	$= -\left(x_1 - \frac{1}{4}\right) \mathbf{a}_1 + x_1 \mathbf{a}_2 + x_1 \mathbf{a}_3$	$=$	$ax_1 \hat{\mathbf{x}} + \frac{1}{8}b \hat{\mathbf{y}} + \frac{1}{8}c \hat{\mathbf{z}}$	(16e)	Na I
\mathbf{B}_2	$= x_1 \mathbf{a}_1 - \left(x_1 - \frac{1}{4}\right) \mathbf{a}_2 - \left(x_1 - \frac{1}{4}\right) \mathbf{a}_3$	$=$	$-a \left(x_1 - \frac{1}{4}\right) \hat{\mathbf{x}} + \frac{1}{8}b \hat{\mathbf{y}} + \frac{1}{8}c \hat{\mathbf{z}}$	(16e)	Na I
\mathbf{B}_3	$= \left(x_1 + \frac{3}{4}\right) \mathbf{a}_1 - x_1 \mathbf{a}_2 - x_1 \mathbf{a}_3$	$=$	$-ax_1 \hat{\mathbf{x}} + \frac{3}{8}b \hat{\mathbf{y}} + \frac{3}{8}c \hat{\mathbf{z}}$	(16e)	Na I
\mathbf{B}_4	$= -x_1 \mathbf{a}_1 + \left(x_1 + \frac{3}{4}\right) \mathbf{a}_2 +$ $\left(x_1 + \frac{3}{4}\right) \mathbf{a}_3$	$=$	$a \left(x_1 + \frac{3}{4}\right) \hat{\mathbf{x}} + \frac{3}{8}b \hat{\mathbf{y}} + \frac{3}{8}c \hat{\mathbf{z}}$	(16e)	Na I
\mathbf{B}_5	$= -\left(x_2 - \frac{1}{4}\right) \mathbf{a}_1 + x_2 \mathbf{a}_2 + x_2 \mathbf{a}_3$	$=$	$ax_2 \hat{\mathbf{x}} + \frac{1}{8}b \hat{\mathbf{y}} + \frac{1}{8}c \hat{\mathbf{z}}$	(16e)	Na II
\mathbf{B}_6	$= x_2 \mathbf{a}_1 - \left(x_2 - \frac{1}{4}\right) \mathbf{a}_2 - \left(x_2 - \frac{1}{4}\right) \mathbf{a}_3$	$=$	$-a \left(x_2 - \frac{1}{4}\right) \hat{\mathbf{x}} + \frac{1}{8}b \hat{\mathbf{y}} + \frac{1}{8}c \hat{\mathbf{z}}$	(16e)	Na II
\mathbf{B}_7	$= \left(x_2 + \frac{3}{4}\right) \mathbf{a}_1 - x_2 \mathbf{a}_2 - x_2 \mathbf{a}_3$	$=$	$-ax_2 \hat{\mathbf{x}} + \frac{3}{8}b \hat{\mathbf{y}} + \frac{3}{8}c \hat{\mathbf{z}}$	(16e)	Na II
\mathbf{B}_8	$= -x_2 \mathbf{a}_1 + \left(x_2 + \frac{3}{4}\right) \mathbf{a}_2 +$ $\left(x_2 + \frac{3}{4}\right) \mathbf{a}_3$	$=$	$a \left(x_2 + \frac{3}{4}\right) \hat{\mathbf{x}} + \frac{3}{8}b \hat{\mathbf{y}} + \frac{3}{8}c \hat{\mathbf{z}}$	(16e)	Na II
\mathbf{B}_9	$= -\left(x_3 - \frac{1}{4}\right) \mathbf{a}_1 + x_3 \mathbf{a}_2 + x_3 \mathbf{a}_3$	$=$	$ax_3 \hat{\mathbf{x}} + \frac{1}{8}b \hat{\mathbf{y}} + \frac{1}{8}c \hat{\mathbf{z}}$	(16e)	Pt I
\mathbf{B}_{10}	$= x_3 \mathbf{a}_1 - \left(x_3 - \frac{1}{4}\right) \mathbf{a}_2 - \left(x_3 - \frac{1}{4}\right) \mathbf{a}_3$	$=$	$-a \left(x_3 - \frac{1}{4}\right) \hat{\mathbf{x}} + \frac{1}{8}b \hat{\mathbf{y}} + \frac{1}{8}c \hat{\mathbf{z}}$	(16e)	Pt I
\mathbf{B}_{11}	$= \left(x_3 + \frac{3}{4}\right) \mathbf{a}_1 - x_3 \mathbf{a}_2 - x_3 \mathbf{a}_3$	$=$	$-ax_3 \hat{\mathbf{x}} + \frac{3}{8}b \hat{\mathbf{y}} + \frac{3}{8}c \hat{\mathbf{z}}$	(16e)	Pt I
\mathbf{B}_{12}	$= -x_3 \mathbf{a}_1 + \left(x_3 + \frac{3}{4}\right) \mathbf{a}_2 +$ $\left(x_3 + \frac{3}{4}\right) \mathbf{a}_3$	$=$	$a \left(x_3 + \frac{3}{4}\right) \hat{\mathbf{x}} + \frac{3}{8}b \hat{\mathbf{y}} + \frac{3}{8}c \hat{\mathbf{z}}$	(16e)	Pt I
\mathbf{B}_{13}	$= y_4 \mathbf{a}_1 - \left(y_4 - \frac{1}{4}\right) \mathbf{a}_2 + y_4 \mathbf{a}_3$	$=$	$\frac{1}{8}a \hat{\mathbf{x}} + by_4 \hat{\mathbf{y}} + \frac{1}{8}c \hat{\mathbf{z}}$	(16f)	O I
\mathbf{B}_{14}	$= -\left(y_4 - \frac{1}{4}\right) \mathbf{a}_1 + y_4 \mathbf{a}_2 -$ $\left(y_4 - \frac{1}{4}\right) \mathbf{a}_3$	$=$	$\frac{1}{8}a \hat{\mathbf{x}} - b \left(y_4 - \frac{1}{4}\right) \hat{\mathbf{y}} + \frac{1}{8}c \hat{\mathbf{z}}$	(16f)	O I
\mathbf{B}_{15}	$= -y_4 \mathbf{a}_1 + \left(y_4 + \frac{3}{4}\right) \mathbf{a}_2 - y_4 \mathbf{a}_3$	$=$	$\frac{3}{8}a \hat{\mathbf{x}} - by_4 \hat{\mathbf{y}} + \frac{3}{8}c \hat{\mathbf{z}}$	(16f)	O I
\mathbf{B}_{16}	$= \left(y_4 + \frac{3}{4}\right) \mathbf{a}_1 - y_4 \mathbf{a}_2 + \left(y_4 + \frac{3}{4}\right) \mathbf{a}_3$	$=$	$\frac{3}{8}a \hat{\mathbf{x}} + b \left(y_4 + \frac{3}{4}\right) \hat{\mathbf{y}} + \frac{3}{8}c \hat{\mathbf{z}}$	(16f)	O I
\mathbf{B}_{17}	$= \left(-x_5 + y_5 + z_5\right) \mathbf{a}_1 +$ $\left(x_5 - y_5 + z_5\right) \mathbf{a}_2 +$ $\left(x_5 + y_5 - z_5\right) \mathbf{a}_3$	$=$	$ax_5 \hat{\mathbf{x}} + by_5 \hat{\mathbf{y}} + cz_5 \hat{\mathbf{z}}$	(32h)	O II
\mathbf{B}_{18}	$= \left(x_5 - y_5 + z_5\right) \mathbf{a}_1 +$ $\left(-x_5 + y_5 + z_5\right) \mathbf{a}_2 -$ $\left(x_5 + y_5 + z_5 - \frac{1}{2}\right) \mathbf{a}_3$	$=$	$-a \left(x_5 - \frac{1}{4}\right) \hat{\mathbf{x}} - b \left(y_5 - \frac{1}{4}\right) \hat{\mathbf{y}} + cz_5 \hat{\mathbf{z}}$	(32h)	O II
\mathbf{B}_{19}	$= \left(x_5 + y_5 - z_5\right) \mathbf{a}_1 -$ $\left(x_5 + y_5 + z_5 - \frac{1}{2}\right) \mathbf{a}_2 +$ $\left(-x_5 + y_5 + z_5\right) \mathbf{a}_3$	$=$	$-a \left(x_5 - \frac{1}{4}\right) \hat{\mathbf{x}} + by_5 \hat{\mathbf{y}} - c \left(z_5 - \frac{1}{4}\right) \hat{\mathbf{z}}$	(32h)	O II
\mathbf{B}_{20}	$= -\left(x_5 + y_5 + z_5 - \frac{1}{2}\right) \mathbf{a}_1 +$ $\left(x_5 + y_5 - z_5\right) \mathbf{a}_2 +$ $\left(x_5 - y_5 + z_5\right) \mathbf{a}_3$	$=$	$ax_5 \hat{\mathbf{x}} - b \left(y_5 - \frac{1}{4}\right) \hat{\mathbf{y}} - c \left(z_5 - \frac{1}{4}\right) \hat{\mathbf{z}}$	(32h)	O II
\mathbf{B}_{21}	$= \left(x_5 - y_5 - z_5\right) \mathbf{a}_1 -$ $\left(x_5 - y_5 + z_5\right) \mathbf{a}_2 -$ $\left(x_5 + y_5 - z_5\right) \mathbf{a}_3$	$=$	$-ax_5 \hat{\mathbf{x}} - by_5 \hat{\mathbf{y}} - cz_5 \hat{\mathbf{z}}$	(32h)	O II
\mathbf{B}_{22}	$= -\left(x_5 - y_5 + z_5\right) \mathbf{a}_1 +$ $\left(x_5 - y_5 - z_5\right) \mathbf{a}_2 +$ $\left(x_5 + y_5 + z_5 + \frac{1}{2}\right) \mathbf{a}_3$	$=$	$a \left(x_5 + \frac{1}{4}\right) \hat{\mathbf{x}} + b \left(y_5 + \frac{1}{4}\right) \hat{\mathbf{y}} - cz_5 \hat{\mathbf{z}}$	(32h)	O II
\mathbf{B}_{23}	$= -\left(x_5 + y_5 - z_5\right) \mathbf{a}_1 +$ $\left(x_5 + y_5 + z_5 + \frac{1}{2}\right) \mathbf{a}_2 +$ $\left(x_5 - y_5 - z_5\right) \mathbf{a}_3$	$=$	$a \left(x_5 + \frac{1}{4}\right) \hat{\mathbf{x}} - by_5 \hat{\mathbf{y}} + c \left(z_5 + \frac{1}{4}\right) \hat{\mathbf{z}}$	(32h)	O II

$$\mathbf{B}_{24} = \begin{pmatrix} (x_5 + y_5 + z_5 + \frac{1}{2}) \mathbf{a}_1 - \\ (x_5 + y_5 - z_5) \mathbf{a}_2 - \\ (x_5 - y_5 + z_5) \mathbf{a}_3 \end{pmatrix} = -ax_5 \hat{\mathbf{x}} + b(y_5 + \frac{1}{4}) \hat{\mathbf{y}} + c(z_5 + \frac{1}{4}) \hat{\mathbf{z}} \quad (32h) \quad \text{O II}$$

References

- [1] W. Umland and R. Hoppe, *Zur Kenntnis der Oxoplatinate Na_2PtO_2 , Na_2PtO_3 , " K_2PtO_3 " und " Rb_2PtO_3 "*, *Z. Anorganische und Allgemeine Chemie* **392**, 23–36 (1972), doi:10.1002/zaac.19723920104.