

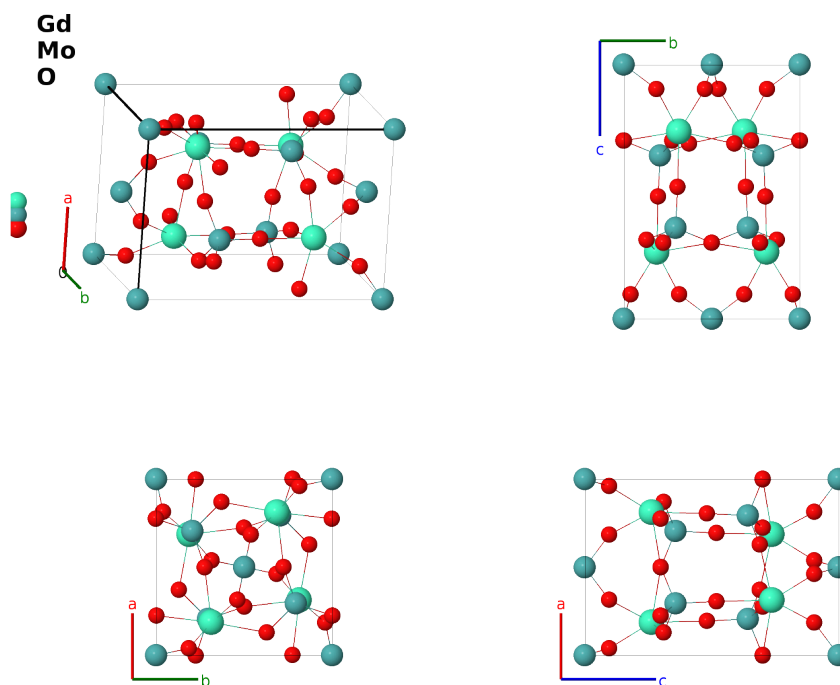
β -Gd₂(MoO₄)₃ Structure: A2B3C12_tP34_113_e_ae_2e2f-001

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<https://aflow.org/prototype-encyclopedia/53TN>

https://aflow.org/prototype-encyclopedia/A2B3C12_tP34_113_e_ae_2e2f-001



Prototype	Gd ₂ Mo ₃ O ₁₂
AFLOW prototype label	A2B3C12_tP34_113_e_ae_2e2f-001
ICSD	2708
CCDC	1592520
Pearson symbol	tP34
Space group number	113
Space group symbol	$P\bar{4}2_1m$
AFLOW prototype command	<pre>aflow --proto=A2B3C12_tP34_113_e_ae_2e2f-001 --params=a, c/a, x₂, z₂, x₃, z₃, x₄, z₄, x₅, z₅, x₆, y₆, z₆, x₇, y₇, z₇</pre>

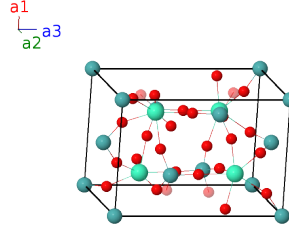
Other compounds with this structure

Dy₂(MoO₄)₃, Eu₂(MoO₄)₃, Gd₂(MoO₄)₃, Nd₂(MoO₄)₃, Pr₂(MoO₄)₃, Sm₂(MoO₄)₃, Tb₂(MoO₄)₃

- $\text{Gd}_2\text{Mo}_3\text{O}_{12}$ takes on several different forms with changing temperature (Yuan, 2001):
 - below 159°C it is in the orthorhombic ground state β' - $\text{Gd}_2(\text{MoO}_4)_3$ structure.
 - In the range 159 - 850°C it is in the monoclinic α - $\text{Gd}_2(\text{MoO}_4)_3$ structure.
 - Above 850°C it is in the tetragonal β - $\text{Gd}_2(\text{MoO}_4)_3$ structure. (Shown here)
- The ICSD entry for (Jeitschko, 1972) gives the structural information in the $\text{C}\bar{4}\text{m}2_1$ setting of space group #113 rather than the standard $\text{P}\bar{4}2_1\text{m}$ setting. This doubled unit cell is nearly cubic. If $\mathbf{a}_1$, $\mathbf{a}_2$, and $\mathbf{a}_3$ are the primitive vectors of $\text{P}\bar{4}2_1\text{m}$ cell, then the primitive vectors of the $\text{C}\bar{4}\text{m}2_1$ cell are:
 - $\mathbf{a}_1' = \mathbf{a}_1 - \mathbf{a}_2$
 - $\mathbf{a}_2' = \mathbf{a}_1 + \mathbf{a}_2$
 - $\mathbf{a}_3' = \mathbf{a}_3$
- The data was taken at 183°C . If the phase diagram from (Yaun, 2001) is correct, β - $\text{Gd}_2(\text{MoO}_4)_3$ is metastable at this temperature. (Jeitschko, 1972) only gives data for the β and β' phases.

Simple Tetragonal primitive vectors

$$\begin{aligned}\mathbf{a}_1 &= a \hat{\mathbf{x}} \\ \mathbf{a}_2 &= a \hat{\mathbf{y}} \\ \mathbf{a}_3 &= c \hat{\mathbf{z}}\end{aligned}$$



Basis vectors

	Lattice coordinates		Cartesian coordinates	Wyckoff position	Atom type
$\mathbf{B}_1$	$= 0$	$=$	0	(2a)	Mo I
$\mathbf{B}_2$	$= \frac{1}{2} \mathbf{a}_1 + \frac{1}{2} \mathbf{a}_2$	$=$	$\frac{1}{2} a \hat{\mathbf{x}} + \frac{1}{2} a \hat{\mathbf{y}}$	(2a)	Mo I
$\mathbf{B}_3$	$= x_2 \mathbf{a}_1 + (x_2 + \frac{1}{2}) \mathbf{a}_2 + z_2 \mathbf{a}_3$	$=$	$ax_2 \hat{\mathbf{x}} + a(x_2 + \frac{1}{2}) \hat{\mathbf{y}} + cz_2 \hat{\mathbf{z}}$	(4e)	Gd I
$\mathbf{B}_4$	$= -x_2 \mathbf{a}_1 - (x_2 - \frac{1}{2}) \mathbf{a}_2 + z_2 \mathbf{a}_3$	$=$	$-ax_2 \hat{\mathbf{x}} - a(x_2 - \frac{1}{2}) \hat{\mathbf{y}} + cz_2 \hat{\mathbf{z}}$	(4e)	Gd I
$\mathbf{B}_5$	$= (x_2 + \frac{1}{2}) \mathbf{a}_1 - x_2 \mathbf{a}_2 - z_2 \mathbf{a}_3$	$=$	$a(x_2 + \frac{1}{2}) \hat{\mathbf{x}} - ax_2 \hat{\mathbf{y}} - cz_2 \hat{\mathbf{z}}$	(4e)	Gd I
$\mathbf{B}_6$	$= -(x_2 - \frac{1}{2}) \mathbf{a}_1 + x_2 \mathbf{a}_2 - z_2 \mathbf{a}_3$	$=$	$-a(x_2 - \frac{1}{2}) \hat{\mathbf{x}} + ax_2 \hat{\mathbf{y}} - cz_2 \hat{\mathbf{z}}$	(4e)	Gd I
$\mathbf{B}_7$	$= x_3 \mathbf{a}_1 + (x_3 + \frac{1}{2}) \mathbf{a}_2 + z_3 \mathbf{a}_3$	$=$	$ax_3 \hat{\mathbf{x}} + a(x_3 + \frac{1}{2}) \hat{\mathbf{y}} + cz_3 \hat{\mathbf{z}}$	(4e)	Mo II
$\mathbf{B}_8$	$= -x_3 \mathbf{a}_1 - (x_3 - \frac{1}{2}) \mathbf{a}_2 + z_3 \mathbf{a}_3$	$=$	$-ax_3 \hat{\mathbf{x}} - a(x_3 - \frac{1}{2}) \hat{\mathbf{y}} + cz_3 \hat{\mathbf{z}}$	(4e)	Mo II
$\mathbf{B}_9$	$= (x_3 + \frac{1}{2}) \mathbf{a}_1 - x_3 \mathbf{a}_2 - z_3 \mathbf{a}_3$	$=$	$a(x_3 + \frac{1}{2}) \hat{\mathbf{x}} - ax_3 \hat{\mathbf{y}} - cz_3 \hat{\mathbf{z}}$	(4e)	Mo II
$\mathbf{B}_{10}$	$= -(x_3 - \frac{1}{2}) \mathbf{a}_1 + x_3 \mathbf{a}_2 - z_3 \mathbf{a}_3$	$=$	$-a(x_3 - \frac{1}{2}) \hat{\mathbf{x}} + ax_3 \hat{\mathbf{y}} - cz_3 \hat{\mathbf{z}}$	(4e)	Mo II
$\mathbf{B}_{11}$	$= x_4 \mathbf{a}_1 + (x_4 + \frac{1}{2}) \mathbf{a}_2 + z_4 \mathbf{a}_3$	$=$	$ax_4 \hat{\mathbf{x}} + a(x_4 + \frac{1}{2}) \hat{\mathbf{y}} + cz_4 \hat{\mathbf{z}}$	(4e)	O I
$\mathbf{B}_{12}$	$= -x_4 \mathbf{a}_1 - (x_4 - \frac{1}{2}) \mathbf{a}_2 + z_4 \mathbf{a}_3$	$=$	$-ax_4 \hat{\mathbf{x}} - a(x_4 - \frac{1}{2}) \hat{\mathbf{y}} + cz_4 \hat{\mathbf{z}}$	(4e)	O I
$\mathbf{B}_{13}$	$= (x_4 + \frac{1}{2}) \mathbf{a}_1 - x_4 \mathbf{a}_2 - z_4 \mathbf{a}_3$	$=$	$a(x_4 + \frac{1}{2}) \hat{\mathbf{x}} - ax_4 \hat{\mathbf{y}} - cz_4 \hat{\mathbf{z}}$	(4e)	O I
$\mathbf{B}_{14}$	$= -(x_4 - \frac{1}{2}) \mathbf{a}_1 + x_4 \mathbf{a}_2 - z_4 \mathbf{a}_3$	$=$	$-a(x_4 - \frac{1}{2}) \hat{\mathbf{x}} + ax_4 \hat{\mathbf{y}} - cz_4 \hat{\mathbf{z}}$	(4e)	O I
$\mathbf{B}_{15}$	$= x_5 \mathbf{a}_1 + (x_5 + \frac{1}{2}) \mathbf{a}_2 + z_5 \mathbf{a}_3$	$=$	$ax_5 \hat{\mathbf{x}} + a(x_5 + \frac{1}{2}) \hat{\mathbf{y}} + cz_5 \hat{\mathbf{z}}$	(4e)	O II
$\mathbf{B}_{16}$	$= -x_5 \mathbf{a}_1 - (x_5 - \frac{1}{2}) \mathbf{a}_2 + z_5 \mathbf{a}_3$	$=$	$-ax_5 \hat{\mathbf{x}} - a(x_5 - \frac{1}{2}) \hat{\mathbf{y}} + cz_5 \hat{\mathbf{z}}$	(4e)	O II

$$\begin{aligned}
\mathbf{B}_{17} &= \left(x_5 + \frac{1}{2}\right) \mathbf{a}_1 - x_5 \mathbf{a}_2 - z_5 \mathbf{a}_3 &= a \left(x_5 + \frac{1}{2}\right) \hat{\mathbf{x}} - ax_5 \hat{\mathbf{y}} - cz_5 \hat{\mathbf{z}} &(4e) & \text{O II} \\
\mathbf{B}_{18} &= -\left(x_5 - \frac{1}{2}\right) \mathbf{a}_1 + x_5 \mathbf{a}_2 - z_5 \mathbf{a}_3 &= -a \left(x_5 - \frac{1}{2}\right) \hat{\mathbf{x}} + ax_5 \hat{\mathbf{y}} - cz_5 \hat{\mathbf{z}} &(4e) & \text{O II} \\
\mathbf{B}_{19} &= x_6 \mathbf{a}_1 + y_6 \mathbf{a}_2 + z_6 \mathbf{a}_3 &= ax_6 \hat{\mathbf{x}} + ay_6 \hat{\mathbf{y}} + cz_6 \hat{\mathbf{z}} &(8f) & \text{O III} \\
\mathbf{B}_{20} &= -x_6 \mathbf{a}_1 - y_6 \mathbf{a}_2 + z_6 \mathbf{a}_3 &= -ax_6 \hat{\mathbf{x}} - ay_6 \hat{\mathbf{y}} + cz_6 \hat{\mathbf{z}} &(8f) & \text{O III} \\
\mathbf{B}_{21} &= y_6 \mathbf{a}_1 - x_6 \mathbf{a}_2 - z_6 \mathbf{a}_3 &= ay_6 \hat{\mathbf{x}} - ax_6 \hat{\mathbf{y}} - cz_6 \hat{\mathbf{z}} &(8f) & \text{O III} \\
\mathbf{B}_{22} &= -y_6 \mathbf{a}_1 + x_6 \mathbf{a}_2 - z_6 \mathbf{a}_3 &= -ay_6 \hat{\mathbf{x}} + ax_6 \hat{\mathbf{y}} - cz_6 \hat{\mathbf{z}} &(8f) & \text{O III} \\
\mathbf{B}_{23} &= -\left(x_6 - \frac{1}{2}\right) \mathbf{a}_1 + \left(y_6 + \frac{1}{2}\right) \mathbf{a}_2 - z_6 \mathbf{a}_3 &= -a \left(x_6 - \frac{1}{2}\right) \hat{\mathbf{x}} + a \left(y_6 + \frac{1}{2}\right) \hat{\mathbf{y}} - cz_6 \hat{\mathbf{z}} &(8f) & \text{O III} \\
\mathbf{B}_{24} &= \left(x_6 + \frac{1}{2}\right) \mathbf{a}_1 - \left(y_6 - \frac{1}{2}\right) \mathbf{a}_2 - z_6 \mathbf{a}_3 &= a \left(x_6 + \frac{1}{2}\right) \hat{\mathbf{x}} - a \left(y_6 - \frac{1}{2}\right) \hat{\mathbf{y}} - cz_6 \hat{\mathbf{z}} &(8f) & \text{O III} \\
\mathbf{B}_{25} &= -\left(y_6 - \frac{1}{2}\right) \mathbf{a}_1 - \left(x_6 - \frac{1}{2}\right) \mathbf{a}_2 + z_6 \mathbf{a}_3 &= -a \left(y_6 - \frac{1}{2}\right) \hat{\mathbf{x}} - a \left(x_6 - \frac{1}{2}\right) \hat{\mathbf{y}} + cz_6 \hat{\mathbf{z}} &(8f) & \text{O III} \\
\mathbf{B}_{26} &= \left(y_6 + \frac{1}{2}\right) \mathbf{a}_1 + \left(x_6 + \frac{1}{2}\right) \mathbf{a}_2 + z_6 \mathbf{a}_3 &= a \left(y_6 + \frac{1}{2}\right) \hat{\mathbf{x}} + a \left(x_6 + \frac{1}{2}\right) \hat{\mathbf{y}} + cz_6 \hat{\mathbf{z}} &(8f) & \text{O III} \\
\mathbf{B}_{27} &= x_7 \mathbf{a}_1 + y_7 \mathbf{a}_2 + z_7 \mathbf{a}_3 &= ax_7 \hat{\mathbf{x}} + ay_7 \hat{\mathbf{y}} + cz_7 \hat{\mathbf{z}} &(8f) & \text{O IV} \\
\mathbf{B}_{28} &= -x_7 \mathbf{a}_1 - y_7 \mathbf{a}_2 + z_7 \mathbf{a}_3 &= -ax_7 \hat{\mathbf{x}} - ay_7 \hat{\mathbf{y}} + cz_7 \hat{\mathbf{z}} &(8f) & \text{O IV} \\
\mathbf{B}_{29} &= y_7 \mathbf{a}_1 - x_7 \mathbf{a}_2 - z_7 \mathbf{a}_3 &= ay_7 \hat{\mathbf{x}} - ax_7 \hat{\mathbf{y}} - cz_7 \hat{\mathbf{z}} &(8f) & \text{O IV} \\
\mathbf{B}_{30} &= -y_7 \mathbf{a}_1 + x_7 \mathbf{a}_2 - z_7 \mathbf{a}_3 &= -ay_7 \hat{\mathbf{x}} + ax_7 \hat{\mathbf{y}} - cz_7 \hat{\mathbf{z}} &(8f) & \text{O IV} \\
\mathbf{B}_{31} &= -\left(x_7 - \frac{1}{2}\right) \mathbf{a}_1 + \left(y_7 + \frac{1}{2}\right) \mathbf{a}_2 - z_7 \mathbf{a}_3 &= -a \left(x_7 - \frac{1}{2}\right) \hat{\mathbf{x}} + a \left(y_7 + \frac{1}{2}\right) \hat{\mathbf{y}} - cz_7 \hat{\mathbf{z}} &(8f) & \text{O IV} \\
\mathbf{B}_{32} &= \left(x_7 + \frac{1}{2}\right) \mathbf{a}_1 - \left(y_7 - \frac{1}{2}\right) \mathbf{a}_2 - z_7 \mathbf{a}_3 &= a \left(x_7 + \frac{1}{2}\right) \hat{\mathbf{x}} - a \left(y_7 - \frac{1}{2}\right) \hat{\mathbf{y}} - cz_7 \hat{\mathbf{z}} &(8f) & \text{O IV} \\
\mathbf{B}_{33} &= -\left(y_7 - \frac{1}{2}\right) \mathbf{a}_1 - \left(x_7 - \frac{1}{2}\right) \mathbf{a}_2 + z_7 \mathbf{a}_3 &= -a \left(y_7 - \frac{1}{2}\right) \hat{\mathbf{x}} - a \left(x_7 - \frac{1}{2}\right) \hat{\mathbf{y}} + cz_7 \hat{\mathbf{z}} &(8f) & \text{O IV} \\
\mathbf{B}_{34} &= \left(y_7 + \frac{1}{2}\right) \mathbf{a}_1 + \left(x_7 + \frac{1}{2}\right) \mathbf{a}_2 + z_7 \mathbf{a}_3 &= a \left(y_7 + \frac{1}{2}\right) \hat{\mathbf{x}} + a \left(x_7 + \frac{1}{2}\right) \hat{\mathbf{y}} + cz_7 \hat{\mathbf{z}} &(8f) & \text{O IV}
\end{aligned}$$

References

- [1] W. Jeitschko, *A comprehensive X-ray study of the ferroelectric-ferroelastic and paraelectric-paraelastic phases of $\text{Gd}_2(\text{MoO}_4)_3$* , Acta Crystallogr. Sect. B **28**, 60–76 (1972), doi:10.1107/S0567740872001876.
- [2] Q. Yuan, C. Zhao, W. Luo, X. Yin, J. Xu, and S. Pan, *Crystal growth of β' - $\text{Gd}_2(\text{MoO}_4)_3$ and in situ observation of its domain structure by the microscope and the synchrotron X-ray topography*, J. Cryst. Growth **233**, 717–722 (2001), doi:10.1016/S0022-0248(01)01594-9.

Found in

- [1] *Inorganic Crystal Structure Database*. Entry 2708 ($\text{Gd}_2(\text{MoO}_4)_3$).

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