

Brownmillerite (Srebrodolskite) Brownmillerite ($\text{Ca}_2\text{Fe}_2\text{O}_5$) Structure:

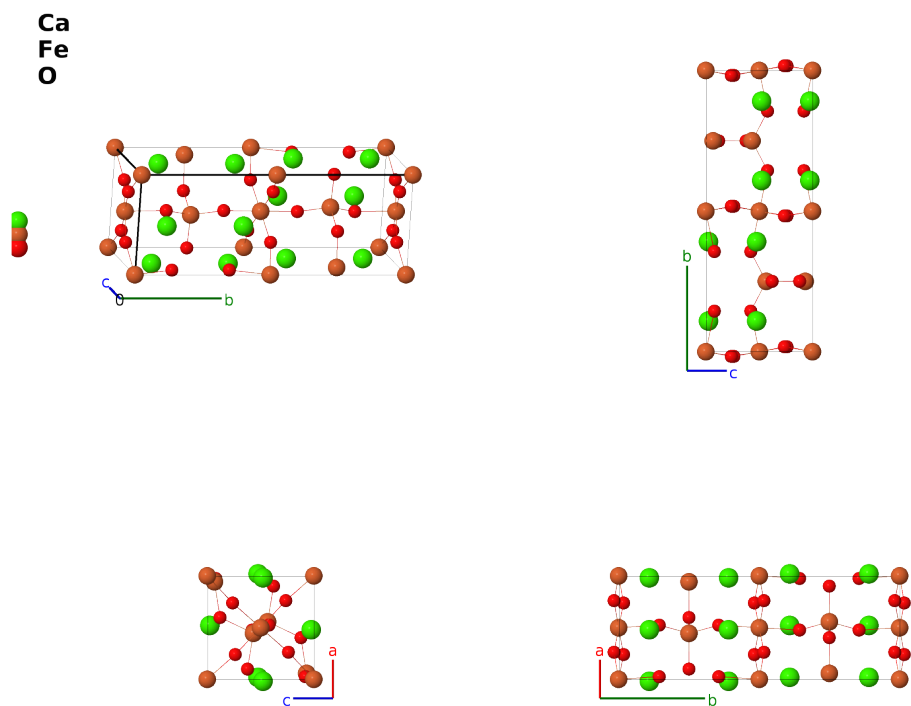
A2B2C5_oP36_62_d_ac_c2d-001

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<https://aflow.org/prototype-encyclopedia/6H47>

https://aflow.org/prototype-encyclopedia/A2B2C5_oP36_62_d_ac_c2d-001



Prototype	$\text{Ca}_2\text{Fe}_2\text{O}_5$
AFLOW prototype label	A2B2C5_oP36_62_d_ac_c2d-001
Mineral name	brownmillerite
ICSD	155632
CCDC	1672233
Pearson symbol	oP36
Space group number	62
Space group symbol	$Pnma$

AFLOW prototype command `aflow --proto=A2B2C5_oP36_62_d_ac_c2d-001`
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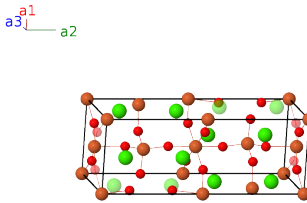
Other compounds with this structure

Ca₂Al₂O₅, Sr₂Co₂O₅, Sr₂Fe₂O₅

- Brownmillerite typically has the composition Fe_{2-x}Al_xO₅, but the pure compound, which the ICSD names Srebrodolskite, has been observed.
- Above 950K this structure transforms into a body-centered orthorhombic structure (Shaula, 2006). This transformation also occurs in the alloyed compounds when $x > 0.56$ (Redhammer, 2004).
- (Shaula, 2006) list the O3 Wyckoff position as (8d), but the coordinates are given for a (4c) site, which gives the proper stoichiometry.

Simple Orthorhombic primitive vectors

$$\begin{aligned} \mathbf{a}_1 &= a \hat{\mathbf{x}} \\ \mathbf{a}_2 &= b \hat{\mathbf{y}} \\ \mathbf{a}_3 &= c \hat{\mathbf{z}} \end{aligned}$$



Basis vectors

	Lattice coordinates		Cartesian coordinates	Wyckoff position	Atom type
$\mathbf{B}_1$	$=$	0	$=$	0	(4a) Fe I
$\mathbf{B}_2$	$=$	$\frac{1}{2} \mathbf{a}_1 + \frac{1}{2} \mathbf{a}_3$	$=$	$\frac{1}{2} a \hat{\mathbf{x}} + \frac{1}{2} c \hat{\mathbf{z}}$	(4a) Fe I
$\mathbf{B}_3$	$=$	$\frac{1}{2} \mathbf{a}_2$	$=$	$\frac{1}{2} b \hat{\mathbf{y}}$	(4a) Fe I
$\mathbf{B}_4$	$=$	$\frac{1}{2} \mathbf{a}_1 + \frac{1}{2} \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	$=$	$\frac{1}{2} a \hat{\mathbf{x}} + \frac{1}{2} b \hat{\mathbf{y}} + \frac{1}{2} c \hat{\mathbf{z}}$	(4a) Fe I
$\mathbf{B}_5$	$=$	$x_2 \mathbf{a}_1 + \frac{1}{4} \mathbf{a}_2 + z_2 \mathbf{a}_3$	$=$	$ax_2 \hat{\mathbf{x}} + \frac{1}{4} b \hat{\mathbf{y}} + cz_2 \hat{\mathbf{z}}$	(4c) Fe II
$\mathbf{B}_6$	$=$	$-(x_2 - \frac{1}{2}) \mathbf{a}_1 + \frac{3}{4} \mathbf{a}_2 + (z_2 + \frac{1}{2}) \mathbf{a}_3$	$=$	$-a(x_2 - \frac{1}{2}) \hat{\mathbf{x}} + \frac{3}{4} b \hat{\mathbf{y}} + c(z_2 + \frac{1}{2}) \hat{\mathbf{z}}$	(4c) Fe II
$\mathbf{B}_7$	$=$	$-x_2 \mathbf{a}_1 + \frac{3}{4} \mathbf{a}_2 - z_2 \mathbf{a}_3$	$=$	$-ax_2 \hat{\mathbf{x}} + \frac{3}{4} b \hat{\mathbf{y}} - cz_2 \hat{\mathbf{z}}$	(4c) Fe II
$\mathbf{B}_8$	$=$	$(x_2 + \frac{1}{2}) \mathbf{a}_1 + \frac{1}{4} \mathbf{a}_2 - (z_2 - \frac{1}{2}) \mathbf{a}_3$	$=$	$a(x_2 + \frac{1}{2}) \hat{\mathbf{x}} + \frac{1}{4} b \hat{\mathbf{y}} - c(z_2 - \frac{1}{2}) \hat{\mathbf{z}}$	(4c) Fe II
$\mathbf{B}_9$	$=$	$x_3 \mathbf{a}_1 + \frac{1}{4} \mathbf{a}_2 + z_3 \mathbf{a}_3$	$=$	$ax_3 \hat{\mathbf{x}} + \frac{1}{4} b \hat{\mathbf{y}} + cz_3 \hat{\mathbf{z}}$	(4c) O I
$\mathbf{B}_{10}$	$=$	$-(x_3 - \frac{1}{2}) \mathbf{a}_1 + \frac{3}{4} \mathbf{a}_2 + (z_3 + \frac{1}{2}) \mathbf{a}_3$	$=$	$-a(x_3 - \frac{1}{2}) \hat{\mathbf{x}} + \frac{3}{4} b \hat{\mathbf{y}} + c(z_3 + \frac{1}{2}) \hat{\mathbf{z}}$	(4c) O I
$\mathbf{B}_{11}$	$=$	$-x_3 \mathbf{a}_1 + \frac{3}{4} \mathbf{a}_2 - z_3 \mathbf{a}_3$	$=$	$-ax_3 \hat{\mathbf{x}} + \frac{3}{4} b \hat{\mathbf{y}} - cz_3 \hat{\mathbf{z}}$	(4c) O I
$\mathbf{B}_{12}$	$=$	$(x_3 + \frac{1}{2}) \mathbf{a}_1 + \frac{1}{4} \mathbf{a}_2 - (z_3 - \frac{1}{2}) \mathbf{a}_3$	$=$	$a(x_3 + \frac{1}{2}) \hat{\mathbf{x}} + \frac{1}{4} b \hat{\mathbf{y}} - c(z_3 - \frac{1}{2}) \hat{\mathbf{z}}$	(4c) O I
$\mathbf{B}_{13}$	$=$	$x_4 \mathbf{a}_1 + y_4 \mathbf{a}_2 + z_4 \mathbf{a}_3$	$=$	$ax_4 \hat{\mathbf{x}} + by_4 \hat{\mathbf{y}} + cz_4 \hat{\mathbf{z}}$	(8d) Ca I
$\mathbf{B}_{14}$	$=$	$-(x_4 - \frac{1}{2}) \mathbf{a}_1 - y_4 \mathbf{a}_2 + (z_4 + \frac{1}{2}) \mathbf{a}_3$	$=$	$-a(x_4 - \frac{1}{2}) \hat{\mathbf{x}} - by_4 \hat{\mathbf{y}} + c(z_4 + \frac{1}{2}) \hat{\mathbf{z}}$	(8d) Ca I
$\mathbf{B}_{15}$	$=$	$-x_4 \mathbf{a}_1 + (y_4 + \frac{1}{2}) \mathbf{a}_2 - z_4 \mathbf{a}_3$	$=$	$-ax_4 \hat{\mathbf{x}} + b(y_4 + \frac{1}{2}) \hat{\mathbf{y}} - cz_4 \hat{\mathbf{z}}$	(8d) Ca I

$$\begin{aligned}
\mathbf{B}_{16} &= \begin{pmatrix} x_4 + \frac{1}{2} \\ z_4 - \frac{1}{2} \end{pmatrix} \mathbf{a}_1 - \begin{pmatrix} y_4 - \frac{1}{2} \\ z_4 - \frac{1}{2} \end{pmatrix} \mathbf{a}_2 - \mathbf{a}_3 &= a \begin{pmatrix} x_4 + \frac{1}{2} \\ z_4 - \frac{1}{2} \end{pmatrix} \hat{\mathbf{x}} - b \begin{pmatrix} y_4 - \frac{1}{2} \\ z_4 - \frac{1}{2} \end{pmatrix} \hat{\mathbf{y}} - c \begin{pmatrix} z_4 - \frac{1}{2} \\ z_4 - \frac{1}{2} \end{pmatrix} \hat{\mathbf{z}} &(8d) & \text{Ca I} \\
\mathbf{B}_{17} &= -x_4 \mathbf{a}_1 - y_4 \mathbf{a}_2 - z_4 \mathbf{a}_3 &= -ax_4 \hat{\mathbf{x}} - by_4 \hat{\mathbf{y}} - cz_4 \hat{\mathbf{z}} &(8d) & \text{Ca I} \\
\mathbf{B}_{18} &= \begin{pmatrix} x_4 + \frac{1}{2} \\ z_4 - \frac{1}{2} \end{pmatrix} \mathbf{a}_1 + y_4 \mathbf{a}_2 - \begin{pmatrix} z_4 - \frac{1}{2} \\ z_4 - \frac{1}{2} \end{pmatrix} \mathbf{a}_3 &= a \begin{pmatrix} x_4 + \frac{1}{2} \\ z_4 - \frac{1}{2} \end{pmatrix} \hat{\mathbf{x}} + by_4 \hat{\mathbf{y}} - c \begin{pmatrix} z_4 - \frac{1}{2} \\ z_4 - \frac{1}{2} \end{pmatrix} \hat{\mathbf{z}} &(8d) & \text{Ca I} \\
\mathbf{B}_{19} &= x_4 \mathbf{a}_1 - \begin{pmatrix} y_4 - \frac{1}{2} \\ z_4 - \frac{1}{2} \end{pmatrix} \mathbf{a}_2 + z_4 \mathbf{a}_3 &= ax_4 \hat{\mathbf{x}} - b \begin{pmatrix} y_4 - \frac{1}{2} \\ z_4 - \frac{1}{2} \end{pmatrix} \hat{\mathbf{y}} + cz_4 \hat{\mathbf{z}} &(8d) & \text{Ca I} \\
\mathbf{B}_{20} &= -\begin{pmatrix} x_4 - \frac{1}{2} \\ z_4 + \frac{1}{2} \end{pmatrix} \mathbf{a}_1 + \begin{pmatrix} y_4 + \frac{1}{2} \\ z_4 + \frac{1}{2} \end{pmatrix} \mathbf{a}_2 + \mathbf{a}_3 &= -a \begin{pmatrix} x_4 - \frac{1}{2} \\ z_4 + \frac{1}{2} \end{pmatrix} \hat{\mathbf{x}} + b \begin{pmatrix} y_4 + \frac{1}{2} \\ z_4 + \frac{1}{2} \end{pmatrix} \hat{\mathbf{y}} + c \begin{pmatrix} z_4 + \frac{1}{2} \\ z_4 + \frac{1}{2} \end{pmatrix} \hat{\mathbf{z}} &(8d) & \text{Ca I} \\
\mathbf{B}_{21} &= x_5 \mathbf{a}_1 + y_5 \mathbf{a}_2 + z_5 \mathbf{a}_3 &= ax_5 \hat{\mathbf{x}} + by_5 \hat{\mathbf{y}} + cz_5 \hat{\mathbf{z}} &(8d) & \text{O II} \\
\mathbf{B}_{22} &= -\begin{pmatrix} x_5 - \frac{1}{2} \\ z_5 + \frac{1}{2} \end{pmatrix} \mathbf{a}_1 - y_5 \mathbf{a}_2 + \mathbf{a}_3 &= -a \begin{pmatrix} x_5 - \frac{1}{2} \\ z_5 + \frac{1}{2} \end{pmatrix} \hat{\mathbf{x}} - by_5 \hat{\mathbf{y}} + c \begin{pmatrix} z_5 + \frac{1}{2} \\ z_5 + \frac{1}{2} \end{pmatrix} \hat{\mathbf{z}} &(8d) & \text{O II} \\
\mathbf{B}_{23} &= -x_5 \mathbf{a}_1 + \begin{pmatrix} y_5 + \frac{1}{2} \\ z_5 - \frac{1}{2} \end{pmatrix} \mathbf{a}_2 - z_5 \mathbf{a}_3 &= -ax_5 \hat{\mathbf{x}} + b \begin{pmatrix} y_5 + \frac{1}{2} \\ z_5 - \frac{1}{2} \end{pmatrix} \hat{\mathbf{y}} - cz_5 \hat{\mathbf{z}} &(8d) & \text{O II} \\
\mathbf{B}_{24} &= \begin{pmatrix} x_5 + \frac{1}{2} \\ z_5 - \frac{1}{2} \end{pmatrix} \mathbf{a}_1 - \begin{pmatrix} y_5 - \frac{1}{2} \\ z_5 - \frac{1}{2} \end{pmatrix} \mathbf{a}_2 - \mathbf{a}_3 &= a \begin{pmatrix} x_5 + \frac{1}{2} \\ z_5 - \frac{1}{2} \end{pmatrix} \hat{\mathbf{x}} - b \begin{pmatrix} y_5 - \frac{1}{2} \\ z_5 - \frac{1}{2} \end{pmatrix} \hat{\mathbf{y}} - c \begin{pmatrix} z_5 - \frac{1}{2} \\ z_5 - \frac{1}{2} \end{pmatrix} \hat{\mathbf{z}} &(8d) & \text{O II} \\
\mathbf{B}_{25} &= -x_5 \mathbf{a}_1 - y_5 \mathbf{a}_2 - z_5 \mathbf{a}_3 &= -ax_5 \hat{\mathbf{x}} - by_5 \hat{\mathbf{y}} - cz_5 \hat{\mathbf{z}} &(8d) & \text{O II} \\
\mathbf{B}_{26} &= \begin{pmatrix} x_5 + \frac{1}{2} \\ z_5 - \frac{1}{2} \end{pmatrix} \mathbf{a}_1 + y_5 \mathbf{a}_2 - \begin{pmatrix} z_5 - \frac{1}{2} \\ z_5 - \frac{1}{2} \end{pmatrix} \mathbf{a}_3 &= a \begin{pmatrix} x_5 + \frac{1}{2} \\ z_5 - \frac{1}{2} \end{pmatrix} \hat{\mathbf{x}} + by_5 \hat{\mathbf{y}} - c \begin{pmatrix} z_5 - \frac{1}{2} \\ z_5 - \frac{1}{2} \end{pmatrix} \hat{\mathbf{z}} &(8d) & \text{O II} \\
\mathbf{B}_{27} &= x_5 \mathbf{a}_1 - \begin{pmatrix} y_5 - \frac{1}{2} \\ z_5 - \frac{1}{2} \end{pmatrix} \mathbf{a}_2 + z_5 \mathbf{a}_3 &= ax_5 \hat{\mathbf{x}} - b \begin{pmatrix} y_5 - \frac{1}{2} \\ z_5 - \frac{1}{2} \end{pmatrix} \hat{\mathbf{y}} + cz_5 \hat{\mathbf{z}} &(8d) & \text{O II} \\
\mathbf{B}_{28} &= -\begin{pmatrix} x_5 - \frac{1}{2} \\ z_5 + \frac{1}{2} \end{pmatrix} \mathbf{a}_1 + \begin{pmatrix} y_5 + \frac{1}{2} \\ z_5 + \frac{1}{2} \end{pmatrix} \mathbf{a}_2 + \mathbf{a}_3 &= -a \begin{pmatrix} x_5 - \frac{1}{2} \\ z_5 + \frac{1}{2} \end{pmatrix} \hat{\mathbf{x}} + b \begin{pmatrix} y_5 + \frac{1}{2} \\ z_5 + \frac{1}{2} \end{pmatrix} \hat{\mathbf{y}} + c \begin{pmatrix} z_5 + \frac{1}{2} \\ z_5 + \frac{1}{2} \end{pmatrix} \hat{\mathbf{z}} &(8d) & \text{O II} \\
\mathbf{B}_{29} &= x_6 \mathbf{a}_1 + y_6 \mathbf{a}_2 + z_6 \mathbf{a}_3 &= ax_6 \hat{\mathbf{x}} + by_6 \hat{\mathbf{y}} + cz_6 \hat{\mathbf{z}} &(8d) & \text{O III} \\
\mathbf{B}_{30} &= -\begin{pmatrix} x_6 - \frac{1}{2} \\ z_6 + \frac{1}{2} \end{pmatrix} \mathbf{a}_1 - y_6 \mathbf{a}_2 + \mathbf{a}_3 &= -a \begin{pmatrix} x_6 - \frac{1}{2} \\ z_6 + \frac{1}{2} \end{pmatrix} \hat{\mathbf{x}} - by_6 \hat{\mathbf{y}} + c \begin{pmatrix} z_6 + \frac{1}{2} \\ z_6 + \frac{1}{2} \end{pmatrix} \hat{\mathbf{z}} &(8d) & \text{O III} \\
\mathbf{B}_{31} &= -x_6 \mathbf{a}_1 + \begin{pmatrix} y_6 + \frac{1}{2} \\ z_6 - \frac{1}{2} \end{pmatrix} \mathbf{a}_2 - z_6 \mathbf{a}_3 &= -ax_6 \hat{\mathbf{x}} + b \begin{pmatrix} y_6 + \frac{1}{2} \\ z_6 - \frac{1}{2} \end{pmatrix} \hat{\mathbf{y}} - cz_6 \hat{\mathbf{z}} &(8d) & \text{O III} \\
\mathbf{B}_{32} &= \begin{pmatrix} x_6 + \frac{1}{2} \\ z_6 - \frac{1}{2} \end{pmatrix} \mathbf{a}_1 - \begin{pmatrix} y_6 - \frac{1}{2} \\ z_6 - \frac{1}{2} \end{pmatrix} \mathbf{a}_2 - \mathbf{a}_3 &= a \begin{pmatrix} x_6 + \frac{1}{2} \\ z_6 - \frac{1}{2} \end{pmatrix} \hat{\mathbf{x}} - b \begin{pmatrix} y_6 - \frac{1}{2} \\ z_6 - \frac{1}{2} \end{pmatrix} \hat{\mathbf{y}} - c \begin{pmatrix} z_6 - \frac{1}{2} \\ z_6 - \frac{1}{2} \end{pmatrix} \hat{\mathbf{z}} &(8d) & \text{O III} \\
\mathbf{B}_{33} &= -x_6 \mathbf{a}_1 - y_6 \mathbf{a}_2 - z_6 \mathbf{a}_3 &= -ax_6 \hat{\mathbf{x}} - by_6 \hat{\mathbf{y}} - cz_6 \hat{\mathbf{z}} &(8d) & \text{O III} \\
\mathbf{B}_{34} &= \begin{pmatrix} x_6 + \frac{1}{2} \\ z_6 - \frac{1}{2} \end{pmatrix} \mathbf{a}_1 + y_6 \mathbf{a}_2 - \begin{pmatrix} z_6 - \frac{1}{2} \\ z_6 - \frac{1}{2} \end{pmatrix} \mathbf{a}_3 &= a \begin{pmatrix} x_6 + \frac{1}{2} \\ z_6 - \frac{1}{2} \end{pmatrix} \hat{\mathbf{x}} + by_6 \hat{\mathbf{y}} - c \begin{pmatrix} z_6 - \frac{1}{2} \\ z_6 - \frac{1}{2} \end{pmatrix} \hat{\mathbf{z}} &(8d) & \text{O III} \\
\mathbf{B}_{35} &= x_6 \mathbf{a}_1 - \begin{pmatrix} y_6 - \frac{1}{2} \\ z_6 - \frac{1}{2} \end{pmatrix} \mathbf{a}_2 + z_6 \mathbf{a}_3 &= ax_6 \hat{\mathbf{x}} - b \begin{pmatrix} y_6 - \frac{1}{2} \\ z_6 - \frac{1}{2} \end{pmatrix} \hat{\mathbf{y}} + cz_6 \hat{\mathbf{z}} &(8d) & \text{O III} \\
\mathbf{B}_{36} &= -\begin{pmatrix} x_6 - \frac{1}{2} \\ z_6 + \frac{1}{2} \end{pmatrix} \mathbf{a}_1 + \begin{pmatrix} y_6 + \frac{1}{2} \\ z_6 + \frac{1}{2} \end{pmatrix} \mathbf{a}_2 + \mathbf{a}_3 &= -a \begin{pmatrix} x_6 - \frac{1}{2} \\ z_6 + \frac{1}{2} \end{pmatrix} \hat{\mathbf{x}} + b \begin{pmatrix} y_6 + \frac{1}{2} \\ z_6 + \frac{1}{2} \end{pmatrix} \hat{\mathbf{y}} + c \begin{pmatrix} z_6 + \frac{1}{2} \\ z_6 + \frac{1}{2} \end{pmatrix} \hat{\mathbf{z}} &(8d) & \text{O III}
\end{aligned}$$

References

- [1] A. L. Shaula, Y. V. Pivak, J. C. Waerenborgh, P. G. nski, A. A. Yaremchenko, and V. V. Kharton, *Ionic conductivity of brownmillerite-type calcium ferrite under oxidizing conditions*, Solid State Ion. **177**, 2923–2930 (2006), doi:10.1016/j.ssi.2006.08.030.
- [2] G. J. Redhammer, G. Tippelt, G. Roth, and G. Amthauer, *Structural variations in the brownmillerite series $\text{Ca}_2(\text{Fe}_{2-x}\text{Al}_x)\text{O}_5$: Single-crystal X-ray diffraction at 25 °C and high-temperature X-ray powder diffraction (25 °C T 1000 °C)*, Am. Mineral. **89**, 405–420 (2004).

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