

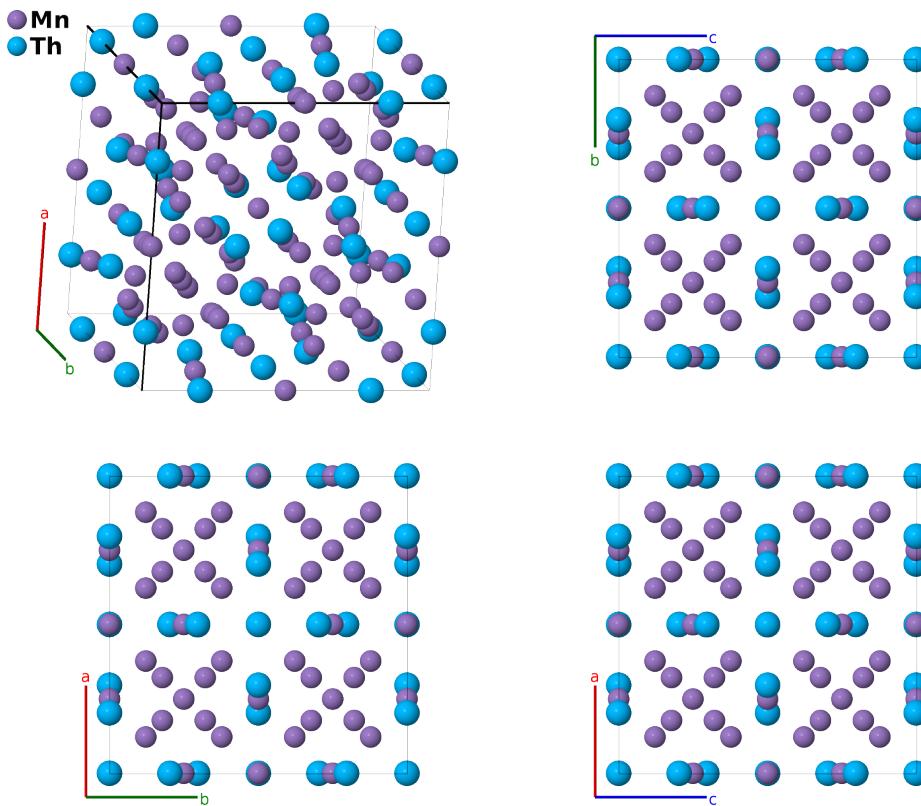
Th₆Mn₂₃ ($D8_a$) Structure: A23B6_cF116_225_ad2f_e-001

This structure originally had the label A23B6_cF116_225_bd2f_e. Calls to that address will be redirected here.

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<https://aflow.org/p/W8MF>

https://aflow.org/p/A23B6_cF116_225_ad2f_e-001



Prototype	Mn ₂₃ Th ₆
AFLOW prototype label	A23B6_cF116_225_ad2f_e-001
Strukturbericht designation	$D8_a$
ICSD	104987
Pearson symbol	cF116
Space group number	225
Space group symbol	$Fm\bar{3}m$
AFLOW prototype command	<code>aflow --proto=A23B6_cF116_225_ad2f_e-001 --params=a,x₃,x₄,x₅</code>

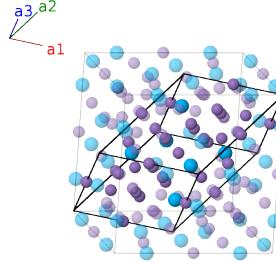
Other compounds with this structure

Co₂₃Zr₆, Fe₂₃Er₆, Fe₂₃Ho₆, Fe₂₃Sm₆, Fe₂₃Tb₆, Li₂₃Sr₆, Mg₂₃Ba₆, Mg₂₃Dy₆, Mg₂₃Er₆, Mg₂₃Gd₆, Mg₂₃Ho₆, Mg₂₃Lu₆, Mg₂₃Nd₆, Mg₂₃Sr₆, Mg₂₃Tb₆, Mg₂₃Th₆, Mg₂₃Tm₆, Mg₂₃Y₆, Mn₂₃Th_{6-x}Y_x, Mn₂₃Th₆, Mn₂₃Y₆, Fe₃Zn, Ge₁₃Fe₁₀Ti₆

- We have moved the ternary compounds with this structure to the Mg₆Si₇Cu₁₆ page.

Face-centered Cubic primitive vectors

$$\begin{aligned}\mathbf{a}_1 &= \frac{1}{2}a\hat{\mathbf{y}} + \frac{1}{2}a\hat{\mathbf{z}} \\ \mathbf{a}_2 &= \frac{1}{2}a\hat{\mathbf{x}} + \frac{1}{2}a\hat{\mathbf{z}} \\ \mathbf{a}_3 &= \frac{1}{2}a\hat{\mathbf{x}} + \frac{1}{2}a\hat{\mathbf{y}}\end{aligned}$$



Basis vectors

	Lattice coordinates	Cartesian coordinates	Wyckoff position	Atom type
\mathbf{B}_1	= 0	= 0	(4a)	Mn I
\mathbf{B}_2	= $\frac{1}{2}\mathbf{a}_1$	= $\frac{1}{4}a\hat{\mathbf{y}} + \frac{1}{4}a\hat{\mathbf{z}}$	(24d)	Mn II
\mathbf{B}_3	= $\frac{1}{2}\mathbf{a}_2 + \frac{1}{2}\mathbf{a}_3$	= $\frac{1}{2}a\hat{\mathbf{x}} + \frac{1}{4}a\hat{\mathbf{y}} + \frac{1}{4}a\hat{\mathbf{z}}$	(24d)	Mn II
\mathbf{B}_4	= $\frac{1}{2}\mathbf{a}_2$	= $\frac{1}{4}a\hat{\mathbf{x}} + \frac{1}{4}a\hat{\mathbf{z}}$	(24d)	Mn II
\mathbf{B}_5	= $\frac{1}{2}\mathbf{a}_1 + \frac{1}{2}\mathbf{a}_3$	= $\frac{1}{4}a\hat{\mathbf{x}} + \frac{1}{2}a\hat{\mathbf{y}} + \frac{1}{4}a\hat{\mathbf{z}}$	(24d)	Mn II
\mathbf{B}_6	= $\frac{1}{2}\mathbf{a}_3$	= $\frac{1}{4}a\hat{\mathbf{x}} + \frac{1}{4}a\hat{\mathbf{y}}$	(24d)	Mn II
\mathbf{B}_7	= $\frac{1}{2}\mathbf{a}_1 + \frac{1}{2}\mathbf{a}_2$	= $\frac{1}{4}a\hat{\mathbf{x}} + \frac{1}{4}a\hat{\mathbf{y}} + \frac{1}{2}a\hat{\mathbf{z}}$	(24d)	Mn II
\mathbf{B}_8	= $-x_3\mathbf{a}_1 + x_3\mathbf{a}_2 + x_3\mathbf{a}_3$	= $ax_3\hat{\mathbf{x}}$	(24e)	Th I
\mathbf{B}_9	= $x_3\mathbf{a}_1 - x_3\mathbf{a}_2 - x_3\mathbf{a}_3$	= $-ax_3\hat{\mathbf{x}}$	(24e)	Th I
\mathbf{B}_{10}	= $x_3\mathbf{a}_1 - x_3\mathbf{a}_2 + x_3\mathbf{a}_3$	= $ax_3\hat{\mathbf{y}}$	(24e)	Th I
\mathbf{B}_{11}	= $-x_3\mathbf{a}_1 + x_3\mathbf{a}_2 - x_3\mathbf{a}_3$	= $-ax_3\hat{\mathbf{y}}$	(24e)	Th I
\mathbf{B}_{12}	= $x_3\mathbf{a}_1 + x_3\mathbf{a}_2 - x_3\mathbf{a}_3$	= $ax_3\hat{\mathbf{z}}$	(24e)	Th I
\mathbf{B}_{13}	= $-x_3\mathbf{a}_1 - x_3\mathbf{a}_2 + x_3\mathbf{a}_3$	= $-ax_3\hat{\mathbf{z}}$	(24e)	Th I
\mathbf{B}_{14}	= $x_4\mathbf{a}_1 + x_4\mathbf{a}_2 + x_4\mathbf{a}_3$	= $ax_4\hat{\mathbf{x}} + ax_4\hat{\mathbf{y}} + ax_4\hat{\mathbf{z}}$	(32f)	Mn III
\mathbf{B}_{15}	= $x_4\mathbf{a}_1 + x_4\mathbf{a}_2 - 3x_4\mathbf{a}_3$	= $-ax_4\hat{\mathbf{x}} - ax_4\hat{\mathbf{y}} + ax_4\hat{\mathbf{z}}$	(32f)	Mn III
\mathbf{B}_{16}	= $x_4\mathbf{a}_1 - 3x_4\mathbf{a}_2 + x_4\mathbf{a}_3$	= $-ax_4\hat{\mathbf{x}} + ax_4\hat{\mathbf{y}} - ax_4\hat{\mathbf{z}}$	(32f)	Mn III
\mathbf{B}_{17}	= $-3x_4\mathbf{a}_1 + x_4\mathbf{a}_2 + x_4\mathbf{a}_3$	= $ax_4\hat{\mathbf{x}} - ax_4\hat{\mathbf{y}} - ax_4\hat{\mathbf{z}}$	(32f)	Mn III
\mathbf{B}_{18}	= $-x_4\mathbf{a}_1 - x_4\mathbf{a}_2 + 3x_4\mathbf{a}_3$	= $ax_4\hat{\mathbf{x}} + ax_4\hat{\mathbf{y}} - ax_4\hat{\mathbf{z}}$	(32f)	Mn III
\mathbf{B}_{19}	= $-x_4\mathbf{a}_1 - x_4\mathbf{a}_2 - x_4\mathbf{a}_3$	= $-ax_4\hat{\mathbf{x}} - ax_4\hat{\mathbf{y}} - ax_4\hat{\mathbf{z}}$	(32f)	Mn III
\mathbf{B}_{20}	= $-x_4\mathbf{a}_1 + 3x_4\mathbf{a}_2 - x_4\mathbf{a}_3$	= $ax_4\hat{\mathbf{x}} - ax_4\hat{\mathbf{y}} + ax_4\hat{\mathbf{z}}$	(32f)	Mn III
\mathbf{B}_{21}	= $3x_4\mathbf{a}_1 - x_4\mathbf{a}_2 - x_4\mathbf{a}_3$	= $-ax_4\hat{\mathbf{x}} + ax_4\hat{\mathbf{y}} + ax_4\hat{\mathbf{z}}$	(32f)	Mn III
\mathbf{B}_{22}	= $x_5\mathbf{a}_1 + x_5\mathbf{a}_2 + x_5\mathbf{a}_3$	= $ax_5\hat{\mathbf{x}} + ax_5\hat{\mathbf{y}} + ax_5\hat{\mathbf{z}}$	(32f)	Mn IV
\mathbf{B}_{23}	= $x_5\mathbf{a}_1 + x_5\mathbf{a}_2 - 3x_5\mathbf{a}_3$	= $-ax_5\hat{\mathbf{x}} - ax_5\hat{\mathbf{y}} + ax_5\hat{\mathbf{z}}$	(32f)	Mn IV

\mathbf{B}_{24}	$x_5 \mathbf{a}_1 - 3x_5 \mathbf{a}_2 + x_5 \mathbf{a}_3$	=	$-ax_5 \hat{\mathbf{x}} + ax_5 \hat{\mathbf{y}} - ax_5 \hat{\mathbf{z}}$	(32f)	Mn IV
\mathbf{B}_{25}	$-3x_5 \mathbf{a}_1 + x_5 \mathbf{a}_2 + x_5 \mathbf{a}_3$	=	$ax_5 \hat{\mathbf{x}} - ax_5 \hat{\mathbf{y}} - ax_5 \hat{\mathbf{z}}$	(32f)	Mn IV
\mathbf{B}_{26}	$-x_5 \mathbf{a}_1 - x_5 \mathbf{a}_2 + 3x_5 \mathbf{a}_3$	=	$ax_5 \hat{\mathbf{x}} + ax_5 \hat{\mathbf{y}} - ax_5 \hat{\mathbf{z}}$	(32f)	Mn IV
\mathbf{B}_{27}	$-x_5 \mathbf{a}_1 - x_5 \mathbf{a}_2 - x_5 \mathbf{a}_3$	=	$-ax_5 \hat{\mathbf{x}} - ax_5 \hat{\mathbf{y}} - ax_5 \hat{\mathbf{z}}$	(32f)	Mn IV
\mathbf{B}_{28}	$-x_5 \mathbf{a}_1 + 3x_5 \mathbf{a}_2 - x_5 \mathbf{a}_3$	=	$ax_5 \hat{\mathbf{x}} - ax_5 \hat{\mathbf{y}} + ax_5 \hat{\mathbf{z}}$	(32f)	Mn IV
\mathbf{B}_{29}	$3x_5 \mathbf{a}_1 - x_5 \mathbf{a}_2 - x_5 \mathbf{a}_3$	=	$-ax_5 \hat{\mathbf{x}} + ax_5 \hat{\mathbf{y}} + ax_5 \hat{\mathbf{z}}$	(32f)	Mn IV

References

- [1] J. V. Florio, R. E. Rundle, and A. I. Snow, *Compounds of thorium with transition metals. I. The thorium-manganese system* 5, 445–457 (1952), doi:10.1107/S0365110X52001337.

Found in

- [1] W. B. Pearson, *A Handbook of Lattice Spacings and Structures of Metals and Alloys, International Series of Monographs on Metal Physics and Physical Metallurgy*, vol. 4 (Pergamon Press, Oxford, London, Edinburgh, New York, Paris, Frankfort, 1958), 1964 reprint with corrections edn.