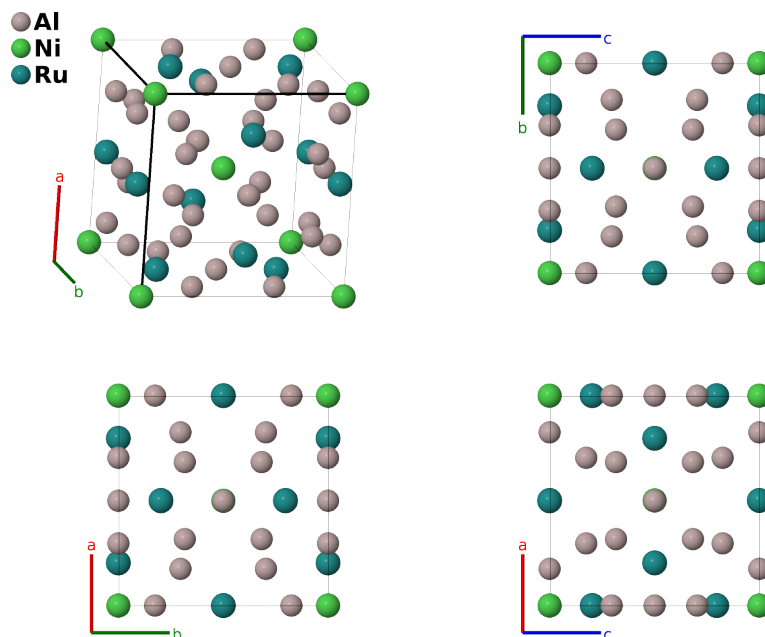


C-AlRuNi ($\text{Al}_{20}\text{Ni}_3\text{Ru}_5$) Structure: A23B2C6_cP31_200_cij_ab_f-001

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<https://afLOW.org/p/L1EN>

https://afLOW.org/p/A23B2C6_cP31_200_cij_ab_f-001



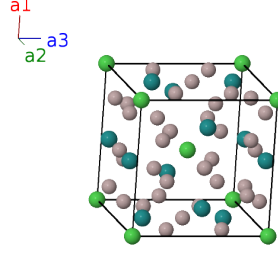
Prototype	$\text{Al}_{20}\text{Ni}_3\text{Ru}_5$
AFLOW prototype label	A23B2C6_cP31_200_cij_ab_f-001
ICSD	230569
Pearson symbol	cP31
Space group number	200
Space group symbol	$Pm\bar{3}$
AFLOW prototype command	<code>afLOW --proto=A23B2C6_cP31_200_cij_ab_f-001 --params=a, x4, x5, y6, z6</code>

- Most of these sites are partially or contained a mixture of species. We label them by the majority species:
 - Ni-I (1a) is 79% nickel and 21% ruthenium,
 - Ni-II (1b) is 100% nickel,
 - Al-I (3c) is 77% aluminum and 23% vacancies,
 - Ru-I (6g) is 81.4% ruthenium and 18.6% nickel,
 - Al-II (8i) is 74% aluminum and 26% vacancies, and
 - Al-III (12k) is 100% aluminum.

- This gives an actual composition of $\text{Al}_{20.23}\text{Ni}_{2.906}\text{Ru}_{5.094}$, which we simplify to $\text{Al}_{20}\text{Ni}_3\text{Ru}_5$.

Simple Cubic primitive vectors

$$\begin{aligned}\mathbf{a}_1 &= a \hat{\mathbf{x}} \\ \mathbf{a}_2 &= a \hat{\mathbf{y}} \\ \mathbf{a}_3 &= a \hat{\mathbf{z}}\end{aligned}$$



Basis vectors

	Lattice coordinates		Cartesian coordinates	Wyckoff position	Atom type
\mathbf{B}_1	$= 0$	$=$	0	(1a)	Ni I
\mathbf{B}_2	$= \frac{1}{2} \mathbf{a}_1 + \frac{1}{2} \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	$=$	$\frac{1}{2} a \hat{\mathbf{x}} + \frac{1}{2} a \hat{\mathbf{y}} + \frac{1}{2} a \hat{\mathbf{z}}$	(1b)	Ni II
\mathbf{B}_3	$= \frac{1}{2} \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	$=$	$\frac{1}{2} a \hat{\mathbf{y}} + \frac{1}{2} a \hat{\mathbf{z}}$	(3c)	Al I
\mathbf{B}_4	$= \frac{1}{2} \mathbf{a}_1 + \frac{1}{2} \mathbf{a}_3$	$=$	$\frac{1}{2} a \hat{\mathbf{x}} + \frac{1}{2} a \hat{\mathbf{z}}$	(3c)	Al I
\mathbf{B}_5	$= \frac{1}{2} \mathbf{a}_1 + \frac{1}{2} \mathbf{a}_2$	$=$	$\frac{1}{2} a \hat{\mathbf{x}} + \frac{1}{2} a \hat{\mathbf{y}}$	(3c)	Al I
\mathbf{B}_6	$= x_4 \mathbf{a}_1 + \frac{1}{2} \mathbf{a}_3$	$=$	$ax_4 \hat{\mathbf{x}} + \frac{1}{2} a \hat{\mathbf{z}}$	(6f)	Ru I
\mathbf{B}_7	$= -x_4 \mathbf{a}_1 + \frac{1}{2} \mathbf{a}_3$	$=$	$-ax_4 \hat{\mathbf{x}} + \frac{1}{2} a \hat{\mathbf{z}}$	(6f)	Ru I
\mathbf{B}_8	$= \frac{1}{2} \mathbf{a}_1 + x_4 \mathbf{a}_2$	$=$	$\frac{1}{2} a \hat{\mathbf{x}} + ax_4 \hat{\mathbf{y}}$	(6f)	Ru I
\mathbf{B}_9	$= \frac{1}{2} \mathbf{a}_1 - x_4 \mathbf{a}_2$	$=$	$\frac{1}{2} a \hat{\mathbf{x}} - ax_4 \hat{\mathbf{y}}$	(6f)	Ru I
\mathbf{B}_{10}	$= \frac{1}{2} \mathbf{a}_2 + x_4 \mathbf{a}_3$	$=$	$\frac{1}{2} a \hat{\mathbf{y}} + ax_4 \hat{\mathbf{z}}$	(6f)	Ru I
\mathbf{B}_{11}	$= \frac{1}{2} \mathbf{a}_2 - x_4 \mathbf{a}_3$	$=$	$\frac{1}{2} a \hat{\mathbf{y}} - ax_4 \hat{\mathbf{z}}$	(6f)	Ru I
\mathbf{B}_{12}	$= x_5 \mathbf{a}_1 + x_5 \mathbf{a}_2 + x_5 \mathbf{a}_3$	$=$	$ax_5 \hat{\mathbf{x}} + ax_5 \hat{\mathbf{y}} + ax_5 \hat{\mathbf{z}}$	(8i)	Al II
\mathbf{B}_{13}	$= -x_5 \mathbf{a}_1 - x_5 \mathbf{a}_2 + x_5 \mathbf{a}_3$	$=$	$-ax_5 \hat{\mathbf{x}} - ax_5 \hat{\mathbf{y}} + ax_5 \hat{\mathbf{z}}$	(8i)	Al II
\mathbf{B}_{14}	$= -x_5 \mathbf{a}_1 + x_5 \mathbf{a}_2 - x_5 \mathbf{a}_3$	$=$	$-ax_5 \hat{\mathbf{x}} + ax_5 \hat{\mathbf{y}} - ax_5 \hat{\mathbf{z}}$	(8i)	Al II
\mathbf{B}_{15}	$= x_5 \mathbf{a}_1 - x_5 \mathbf{a}_2 - x_5 \mathbf{a}_3$	$=$	$ax_5 \hat{\mathbf{x}} - ax_5 \hat{\mathbf{y}} - ax_5 \hat{\mathbf{z}}$	(8i)	Al II
\mathbf{B}_{16}	$= -x_5 \mathbf{a}_1 - x_5 \mathbf{a}_2 - x_5 \mathbf{a}_3$	$=$	$-ax_5 \hat{\mathbf{x}} - ax_5 \hat{\mathbf{y}} - ax_5 \hat{\mathbf{z}}$	(8i)	Al II
\mathbf{B}_{17}	$= x_5 \mathbf{a}_1 + x_5 \mathbf{a}_2 - x_5 \mathbf{a}_3$	$=$	$ax_5 \hat{\mathbf{x}} + ax_5 \hat{\mathbf{y}} - ax_5 \hat{\mathbf{z}}$	(8i)	Al II
\mathbf{B}_{18}	$= x_5 \mathbf{a}_1 - x_5 \mathbf{a}_2 + x_5 \mathbf{a}_3$	$=$	$ax_5 \hat{\mathbf{x}} - ax_5 \hat{\mathbf{y}} + ax_5 \hat{\mathbf{z}}$	(8i)	Al II
\mathbf{B}_{19}	$= -x_5 \mathbf{a}_1 + x_5 \mathbf{a}_2 + x_5 \mathbf{a}_3$	$=$	$-ax_5 \hat{\mathbf{x}} + ax_5 \hat{\mathbf{y}} + ax_5 \hat{\mathbf{z}}$	(8i)	Al II
\mathbf{B}_{20}	$= y_6 \mathbf{a}_2 + z_6 \mathbf{a}_3$	$=$	$ay_6 \hat{\mathbf{y}} + az_6 \hat{\mathbf{z}}$	(12j)	Al III
\mathbf{B}_{21}	$= -y_6 \mathbf{a}_2 + z_6 \mathbf{a}_3$	$=$	$-ay_6 \hat{\mathbf{y}} + az_6 \hat{\mathbf{z}}$	(12j)	Al III
\mathbf{B}_{22}	$= y_6 \mathbf{a}_2 - z_6 \mathbf{a}_3$	$=$	$ay_6 \hat{\mathbf{y}} - az_6 \hat{\mathbf{z}}$	(12j)	Al III
\mathbf{B}_{23}	$= -y_6 \mathbf{a}_2 - z_6 \mathbf{a}_3$	$=$	$-ay_6 \hat{\mathbf{y}} - az_6 \hat{\mathbf{z}}$	(12j)	Al III
\mathbf{B}_{24}	$= z_6 \mathbf{a}_1 + y_6 \mathbf{a}_3$	$=$	$az_6 \hat{\mathbf{x}} + ay_6 \hat{\mathbf{z}}$	(12j)	Al III
\mathbf{B}_{25}	$= z_6 \mathbf{a}_1 - y_6 \mathbf{a}_3$	$=$	$az_6 \hat{\mathbf{x}} - ay_6 \hat{\mathbf{z}}$	(12j)	Al III
\mathbf{B}_{26}	$= -z_6 \mathbf{a}_1 + y_6 \mathbf{a}_3$	$=$	$-az_6 \hat{\mathbf{x}} + ay_6 \hat{\mathbf{z}}$	(12j)	Al III
\mathbf{B}_{27}	$= -z_6 \mathbf{a}_1 - y_6 \mathbf{a}_3$	$=$	$-az_6 \hat{\mathbf{x}} - ay_6 \hat{\mathbf{z}}$	(12j)	Al III
\mathbf{B}_{28}	$= y_6 \mathbf{a}_1 + z_6 \mathbf{a}_2$	$=$	$ay_6 \hat{\mathbf{x}} + az_6 \hat{\mathbf{y}}$	(12j)	Al III

$$\mathbf{B}_{29} = -y_6 \mathbf{a}_1 + z_6 \mathbf{a}_2 = -ay_6 \hat{\mathbf{x}} + az_6 \hat{\mathbf{y}} \quad (12j) \quad \text{Al III}$$

$$\mathbf{B}_{30} = y_6 \mathbf{a}_1 - z_6 \mathbf{a}_2 = ay_6 \hat{\mathbf{x}} - az_6 \hat{\mathbf{y}} \quad (12j) \quad \text{Al III}$$

$$\mathbf{B}_{31} = -y_6 \mathbf{a}_1 - z_6 \mathbf{a}_2 = -ay_6 \hat{\mathbf{x}} - az_6 \hat{\mathbf{y}} \quad (12j) \quad \text{Al III}$$

References

- [1] R. Simura, K. Sugiyama, S. Suzuki, and T. Kawamata, *Crystal Structure of the C-AlRuNi Phase*, Mater. Trans. **58**, 1101–1105 (2017), doi:10.2320/matertrans.M2017106.