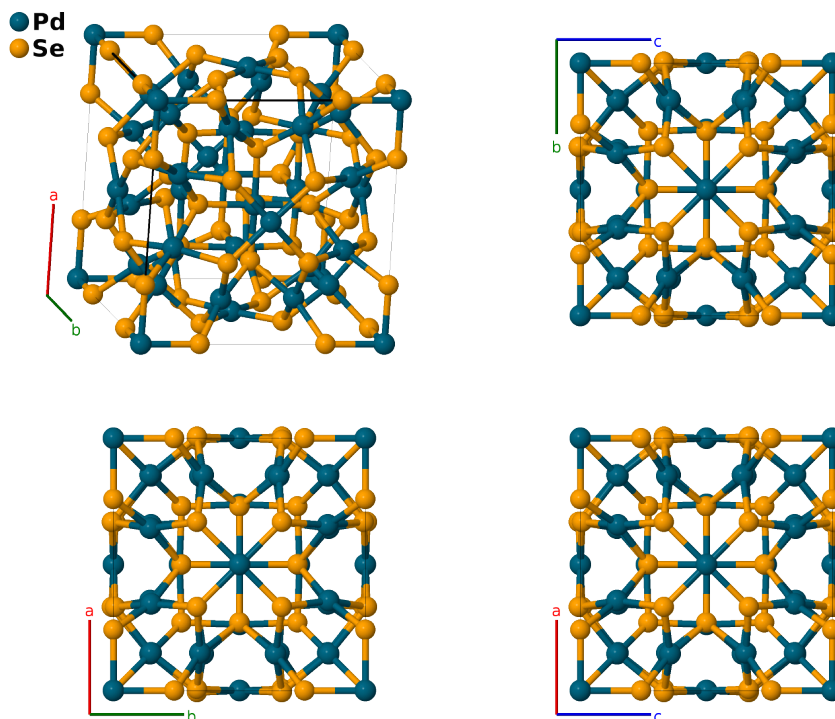


# Palladseite ( $\text{Pd}_{17}\text{Se}_{15}$ ) Structure: A17B15\_cP64\_215\_acg2i\_f2i-001

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<https://aflow.org/p/55EV>

[https://aflow.org/p/A17B15\\_cP64\\_215\\_acg2i\\_f2i-001](https://aflow.org/p/A17B15_cP64_215_acg2i_f2i-001)



Prototype	$\text{Pd}_{17}\text{Se}_{15}$
AFLOW prototype label	A17B15_cP64_215_acg2i_f2i-001
Mineral name	palladseite
ICSD	none
Pearson symbol	cP64
Space group number	215
Space group symbol	$P\bar{4}3m$
AFLOW prototype command	<code>aflow --proto=A17B15_cP64_215_acg2i_f2i-001 --params=a, x3, x4, x5, z5, x6, z6, x7, z7, x8, z8</code>

## Other compounds with this structure

$\text{Rh}_{17}\text{S}_{15}$

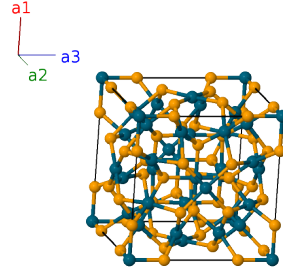
- (Geller, 1962) determined that  $\text{Pd}_{17}\text{Se}_{15}$  could be in space group  $Pm\bar{3}m$  #221,  $P\bar{4}3m$  #215 (this structure), or  $P432$  #207, and finds that  $Pm\bar{3}m$  gives the best fit to single-crystal X-ray diffraction pattern, even though the fit of the parameters for the all of the Wyckoff sites could not be converged. We therefore present all three structure possibilities.

- We shifted the coordinates of (Geller, 1962) to move the Pd-I atom from the center of the cubic cell, Wyckoff position (1b), to the origin, Wyckoff position (1a).

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### Simple Cubic primitive vectors

$$\begin{aligned}\mathbf{a}_1 &= a \hat{\mathbf{x}} \\ \mathbf{a}_2 &= a \hat{\mathbf{y}} \\ \mathbf{a}_3 &= a \hat{\mathbf{z}}\end{aligned}$$




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### Basis vectors

	Lattice coordinates		Cartesian coordinates	Wyckoff position	Atom type
$\mathbf{B}_1 =$	$0$	$=$	$0$	(1a)	Pd I
$\mathbf{B}_2 =$	$\frac{1}{2} \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	$=$	$\frac{1}{2} a \hat{\mathbf{y}} + \frac{1}{2} a \hat{\mathbf{z}}$	(3c)	Pd II
$\mathbf{B}_3 =$	$\frac{1}{2} \mathbf{a}_1 + \frac{1}{2} \mathbf{a}_3$	$=$	$\frac{1}{2} a \hat{\mathbf{x}} + \frac{1}{2} a \hat{\mathbf{z}}$	(3c)	Pd II
$\mathbf{B}_4 =$	$\frac{1}{2} \mathbf{a}_1 + \frac{1}{2} \mathbf{a}_2$	$=$	$\frac{1}{2} a \hat{\mathbf{x}} + \frac{1}{2} a \hat{\mathbf{y}}$	(3c)	Pd II
$\mathbf{B}_5 =$	$x_3 \mathbf{a}_1$	$=$	$ax_3 \hat{\mathbf{x}}$	(6f)	Se I
$\mathbf{B}_6 =$	$-x_3 \mathbf{a}_1$	$=$	$-ax_3 \hat{\mathbf{x}}$	(6f)	Se I
$\mathbf{B}_7 =$	$x_3 \mathbf{a}_2$	$=$	$ax_3 \hat{\mathbf{y}}$	(6f)	Se I
$\mathbf{B}_8 =$	$-x_3 \mathbf{a}_2$	$=$	$-ax_3 \hat{\mathbf{y}}$	(6f)	Se I
$\mathbf{B}_9 =$	$x_3 \mathbf{a}_3$	$=$	$ax_3 \hat{\mathbf{z}}$	(6f)	Se I
$\mathbf{B}_{10} =$	$-x_3 \mathbf{a}_3$	$=$	$-ax_3 \hat{\mathbf{z}}$	(6f)	Se I
$\mathbf{B}_{11} =$	$x_4 \mathbf{a}_1 + \frac{1}{2} \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	$=$	$ax_4 \hat{\mathbf{x}} + \frac{1}{2} a \hat{\mathbf{y}} + \frac{1}{2} a \hat{\mathbf{z}}$	(6g)	Pd III
$\mathbf{B}_{12} =$	$-x_4 \mathbf{a}_1 + \frac{1}{2} \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	$=$	$-ax_4 \hat{\mathbf{x}} + \frac{1}{2} a \hat{\mathbf{y}} + \frac{1}{2} a \hat{\mathbf{z}}$	(6g)	Pd III
$\mathbf{B}_{13} =$	$\frac{1}{2} \mathbf{a}_1 + x_4 \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	$=$	$\frac{1}{2} a \hat{\mathbf{x}} + ax_4 \hat{\mathbf{y}} + \frac{1}{2} a \hat{\mathbf{z}}$	(6g)	Pd III
$\mathbf{B}_{14} =$	$\frac{1}{2} \mathbf{a}_1 - x_4 \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	$=$	$\frac{1}{2} a \hat{\mathbf{x}} - ax_4 \hat{\mathbf{y}} + \frac{1}{2} a \hat{\mathbf{z}}$	(6g)	Pd III
$\mathbf{B}_{15} =$	$\frac{1}{2} \mathbf{a}_1 + \frac{1}{2} \mathbf{a}_2 + x_4 \mathbf{a}_3$	$=$	$\frac{1}{2} a \hat{\mathbf{x}} + \frac{1}{2} a \hat{\mathbf{y}} + ax_4 \hat{\mathbf{z}}$	(6g)	Pd III
$\mathbf{B}_{16} =$	$\frac{1}{2} \mathbf{a}_1 + \frac{1}{2} \mathbf{a}_2 - x_4 \mathbf{a}_3$	$=$	$\frac{1}{2} a \hat{\mathbf{x}} + \frac{1}{2} a \hat{\mathbf{y}} - ax_4 \hat{\mathbf{z}}$	(6g)	Pd III
$\mathbf{B}_{17} =$	$x_5 \mathbf{a}_1 + x_5 \mathbf{a}_2 + z_5 \mathbf{a}_3$	$=$	$ax_5 \hat{\mathbf{x}} + ax_5 \hat{\mathbf{y}} + az_5 \hat{\mathbf{z}}$	(12i)	Pd IV
$\mathbf{B}_{18} =$	$-x_5 \mathbf{a}_1 - x_5 \mathbf{a}_2 + z_5 \mathbf{a}_3$	$=$	$-ax_5 \hat{\mathbf{x}} - ax_5 \hat{\mathbf{y}} + az_5 \hat{\mathbf{z}}$	(12i)	Pd IV
$\mathbf{B}_{19} =$	$-x_5 \mathbf{a}_1 + x_5 \mathbf{a}_2 - z_5 \mathbf{a}_3$	$=$	$-ax_5 \hat{\mathbf{x}} + ax_5 \hat{\mathbf{y}} - az_5 \hat{\mathbf{z}}$	(12i)	Pd IV
$\mathbf{B}_{20} =$	$x_5 \mathbf{a}_1 - x_5 \mathbf{a}_2 - z_5 \mathbf{a}_3$	$=$	$ax_5 \hat{\mathbf{x}} - ax_5 \hat{\mathbf{y}} - az_5 \hat{\mathbf{z}}$	(12i)	Pd IV
$\mathbf{B}_{21} =$	$z_5 \mathbf{a}_1 + x_5 \mathbf{a}_2 + x_5 \mathbf{a}_3$	$=$	$az_5 \hat{\mathbf{x}} + ax_5 \hat{\mathbf{y}} + ax_5 \hat{\mathbf{z}}$	(12i)	Pd IV
$\mathbf{B}_{22} =$	$z_5 \mathbf{a}_1 - x_5 \mathbf{a}_2 - x_5 \mathbf{a}_3$	$=$	$az_5 \hat{\mathbf{x}} - ax_5 \hat{\mathbf{y}} - ax_5 \hat{\mathbf{z}}$	(12i)	Pd IV
$\mathbf{B}_{23} =$	$-z_5 \mathbf{a}_1 - x_5 \mathbf{a}_2 + x_5 \mathbf{a}_3$	$=$	$-az_5 \hat{\mathbf{x}} - ax_5 \hat{\mathbf{y}} + ax_5 \hat{\mathbf{z}}$	(12i)	Pd IV
$\mathbf{B}_{24} =$	$-z_5 \mathbf{a}_1 + x_5 \mathbf{a}_2 - x_5 \mathbf{a}_3$	$=$	$-az_5 \hat{\mathbf{x}} + ax_5 \hat{\mathbf{y}} - ax_5 \hat{\mathbf{z}}$	(12i)	Pd IV
$\mathbf{B}_{25} =$	$x_5 \mathbf{a}_1 + z_5 \mathbf{a}_2 + x_5 \mathbf{a}_3$	$=$	$ax_5 \hat{\mathbf{x}} + az_5 \hat{\mathbf{y}} + ax_5 \hat{\mathbf{z}}$	(12i)	Pd IV
$\mathbf{B}_{26} =$	$-x_5 \mathbf{a}_1 + z_5 \mathbf{a}_2 - x_5 \mathbf{a}_3$	$=$	$-ax_5 \hat{\mathbf{x}} + az_5 \hat{\mathbf{y}} - ax_5 \hat{\mathbf{z}}$	(12i)	Pd IV
$\mathbf{B}_{27} =$	$x_5 \mathbf{a}_1 - z_5 \mathbf{a}_2 - x_5 \mathbf{a}_3$	$=$	$ax_5 \hat{\mathbf{x}} - az_5 \hat{\mathbf{y}} - ax_5 \hat{\mathbf{z}}$	(12i)	Pd IV

$\mathbf{B}_{28} =$	$-x_5 \mathbf{a}_1 - z_5 \mathbf{a}_2 + x_5 \mathbf{a}_3$	$=$	$-ax_5 \hat{\mathbf{x}} - az_5 \hat{\mathbf{y}} + ax_5 \hat{\mathbf{z}}$	(12i)	Pd IV
$\mathbf{B}_{29} =$	$x_6 \mathbf{a}_1 + x_6 \mathbf{a}_2 + z_6 \mathbf{a}_3$	$=$	$ax_6 \hat{\mathbf{x}} + ax_6 \hat{\mathbf{y}} + az_6 \hat{\mathbf{z}}$	(12i)	Pd V
$\mathbf{B}_{30} =$	$-x_6 \mathbf{a}_1 - x_6 \mathbf{a}_2 + z_6 \mathbf{a}_3$	$=$	$-ax_6 \hat{\mathbf{x}} - ax_6 \hat{\mathbf{y}} + az_6 \hat{\mathbf{z}}$	(12i)	Pd V
$\mathbf{B}_{31} =$	$-x_6 \mathbf{a}_1 + x_6 \mathbf{a}_2 - z_6 \mathbf{a}_3$	$=$	$-ax_6 \hat{\mathbf{x}} + ax_6 \hat{\mathbf{y}} - az_6 \hat{\mathbf{z}}$	(12i)	Pd V
$\mathbf{B}_{32} =$	$x_6 \mathbf{a}_1 - x_6 \mathbf{a}_2 - z_6 \mathbf{a}_3$	$=$	$ax_6 \hat{\mathbf{x}} - ax_6 \hat{\mathbf{y}} - az_6 \hat{\mathbf{z}}$	(12i)	Pd V
$\mathbf{B}_{33} =$	$z_6 \mathbf{a}_1 + x_6 \mathbf{a}_2 + x_6 \mathbf{a}_3$	$=$	$az_6 \hat{\mathbf{x}} + ax_6 \hat{\mathbf{y}} + ax_6 \hat{\mathbf{z}}$	(12i)	Pd V
$\mathbf{B}_{34} =$	$z_6 \mathbf{a}_1 - x_6 \mathbf{a}_2 - x_6 \mathbf{a}_3$	$=$	$az_6 \hat{\mathbf{x}} - ax_6 \hat{\mathbf{y}} - ax_6 \hat{\mathbf{z}}$	(12i)	Pd V
$\mathbf{B}_{35} =$	$-z_6 \mathbf{a}_1 - x_6 \mathbf{a}_2 + x_6 \mathbf{a}_3$	$=$	$-az_6 \hat{\mathbf{x}} - ax_6 \hat{\mathbf{y}} + ax_6 \hat{\mathbf{z}}$	(12i)	Pd V
$\mathbf{B}_{36} =$	$-z_6 \mathbf{a}_1 + x_6 \mathbf{a}_2 - x_6 \mathbf{a}_3$	$=$	$-az_6 \hat{\mathbf{x}} + ax_6 \hat{\mathbf{y}} - ax_6 \hat{\mathbf{z}}$	(12i)	Pd V
$\mathbf{B}_{37} =$	$x_6 \mathbf{a}_1 + z_6 \mathbf{a}_2 + x_6 \mathbf{a}_3$	$=$	$ax_6 \hat{\mathbf{x}} + az_6 \hat{\mathbf{y}} + ax_6 \hat{\mathbf{z}}$	(12i)	Pd V
$\mathbf{B}_{38} =$	$-x_6 \mathbf{a}_1 + z_6 \mathbf{a}_2 - x_6 \mathbf{a}_3$	$=$	$-ax_6 \hat{\mathbf{x}} + az_6 \hat{\mathbf{y}} - ax_6 \hat{\mathbf{z}}$	(12i)	Pd V
$\mathbf{B}_{39} =$	$x_6 \mathbf{a}_1 - z_6 \mathbf{a}_2 - x_6 \mathbf{a}_3$	$=$	$ax_6 \hat{\mathbf{x}} - az_6 \hat{\mathbf{y}} - ax_6 \hat{\mathbf{z}}$	(12i)	Pd V
$\mathbf{B}_{40} =$	$-x_6 \mathbf{a}_1 - z_6 \mathbf{a}_2 + x_6 \mathbf{a}_3$	$=$	$-ax_6 \hat{\mathbf{x}} - az_6 \hat{\mathbf{y}} + ax_6 \hat{\mathbf{z}}$	(12i)	Pd V
$\mathbf{B}_{41} =$	$x_7 \mathbf{a}_1 + x_7 \mathbf{a}_2 + z_7 \mathbf{a}_3$	$=$	$ax_7 \hat{\mathbf{x}} + ax_7 \hat{\mathbf{y}} + az_7 \hat{\mathbf{z}}$	(12i)	Se II
$\mathbf{B}_{42} =$	$-x_7 \mathbf{a}_1 - x_7 \mathbf{a}_2 + z_7 \mathbf{a}_3$	$=$	$-ax_7 \hat{\mathbf{x}} - ax_7 \hat{\mathbf{y}} + az_7 \hat{\mathbf{z}}$	(12i)	Se II
$\mathbf{B}_{43} =$	$-x_7 \mathbf{a}_1 + x_7 \mathbf{a}_2 - z_7 \mathbf{a}_3$	$=$	$-ax_7 \hat{\mathbf{x}} + ax_7 \hat{\mathbf{y}} - az_7 \hat{\mathbf{z}}$	(12i)	Se II
$\mathbf{B}_{44} =$	$x_7 \mathbf{a}_1 - x_7 \mathbf{a}_2 - z_7 \mathbf{a}_3$	$=$	$ax_7 \hat{\mathbf{x}} - ax_7 \hat{\mathbf{y}} - az_7 \hat{\mathbf{z}}$	(12i)	Se II
$\mathbf{B}_{45} =$	$z_7 \mathbf{a}_1 + x_7 \mathbf{a}_2 + x_7 \mathbf{a}_3$	$=$	$az_7 \hat{\mathbf{x}} + ax_7 \hat{\mathbf{y}} + ax_7 \hat{\mathbf{z}}$	(12i)	Se II
$\mathbf{B}_{46} =$	$z_7 \mathbf{a}_1 - x_7 \mathbf{a}_2 - x_7 \mathbf{a}_3$	$=$	$az_7 \hat{\mathbf{x}} - ax_7 \hat{\mathbf{y}} - ax_7 \hat{\mathbf{z}}$	(12i)	Se II
$\mathbf{B}_{47} =$	$-z_7 \mathbf{a}_1 - x_7 \mathbf{a}_2 + x_7 \mathbf{a}_3$	$=$	$-az_7 \hat{\mathbf{x}} - ax_7 \hat{\mathbf{y}} + ax_7 \hat{\mathbf{z}}$	(12i)	Se II
$\mathbf{B}_{48} =$	$-z_7 \mathbf{a}_1 + x_7 \mathbf{a}_2 - x_7 \mathbf{a}_3$	$=$	$-az_7 \hat{\mathbf{x}} + ax_7 \hat{\mathbf{y}} - ax_7 \hat{\mathbf{z}}$	(12i)	Se II
$\mathbf{B}_{49} =$	$x_7 \mathbf{a}_1 + z_7 \mathbf{a}_2 + x_7 \mathbf{a}_3$	$=$	$ax_7 \hat{\mathbf{x}} + az_7 \hat{\mathbf{y}} + ax_7 \hat{\mathbf{z}}$	(12i)	Se II
$\mathbf{B}_{50} =$	$-x_7 \mathbf{a}_1 + z_7 \mathbf{a}_2 - x_7 \mathbf{a}_3$	$=$	$-ax_7 \hat{\mathbf{x}} + az_7 \hat{\mathbf{y}} - ax_7 \hat{\mathbf{z}}$	(12i)	Se II
$\mathbf{B}_{51} =$	$x_7 \mathbf{a}_1 - z_7 \mathbf{a}_2 - x_7 \mathbf{a}_3$	$=$	$ax_7 \hat{\mathbf{x}} - az_7 \hat{\mathbf{y}} - ax_7 \hat{\mathbf{z}}$	(12i)	Se II
$\mathbf{B}_{52} =$	$-x_7 \mathbf{a}_1 - z_7 \mathbf{a}_2 + x_7 \mathbf{a}_3$	$=$	$-ax_7 \hat{\mathbf{x}} - az_7 \hat{\mathbf{y}} + ax_7 \hat{\mathbf{z}}$	(12i)	Se II
$\mathbf{B}_{53} =$	$x_8 \mathbf{a}_1 + x_8 \mathbf{a}_2 + z_8 \mathbf{a}_3$	$=$	$ax_8 \hat{\mathbf{x}} + ax_8 \hat{\mathbf{y}} + az_8 \hat{\mathbf{z}}$	(12i)	Se III
$\mathbf{B}_{54} =$	$-x_8 \mathbf{a}_1 - x_8 \mathbf{a}_2 + z_8 \mathbf{a}_3$	$=$	$-ax_8 \hat{\mathbf{x}} - ax_8 \hat{\mathbf{y}} + az_8 \hat{\mathbf{z}}$	(12i)	Se III
$\mathbf{B}_{55} =$	$-x_8 \mathbf{a}_1 + x_8 \mathbf{a}_2 - z_8 \mathbf{a}_3$	$=$	$-ax_8 \hat{\mathbf{x}} + ax_8 \hat{\mathbf{y}} - az_8 \hat{\mathbf{z}}$	(12i)	Se III
$\mathbf{B}_{56} =$	$x_8 \mathbf{a}_1 - x_8 \mathbf{a}_2 - z_8 \mathbf{a}_3$	$=$	$ax_8 \hat{\mathbf{x}} - ax_8 \hat{\mathbf{y}} - az_8 \hat{\mathbf{z}}$	(12i)	Se III
$\mathbf{B}_{57} =$	$z_8 \mathbf{a}_1 + x_8 \mathbf{a}_2 + x_8 \mathbf{a}_3$	$=$	$az_8 \hat{\mathbf{x}} + ax_8 \hat{\mathbf{y}} + ax_8 \hat{\mathbf{z}}$	(12i)	Se III
$\mathbf{B}_{58} =$	$z_8 \mathbf{a}_1 - x_8 \mathbf{a}_2 - x_8 \mathbf{a}_3$	$=$	$az_8 \hat{\mathbf{x}} - ax_8 \hat{\mathbf{y}} - ax_8 \hat{\mathbf{z}}$	(12i)	Se III
$\mathbf{B}_{59} =$	$-z_8 \mathbf{a}_1 - x_8 \mathbf{a}_2 + x_8 \mathbf{a}_3$	$=$	$-az_8 \hat{\mathbf{x}} - ax_8 \hat{\mathbf{y}} + ax_8 \hat{\mathbf{z}}$	(12i)	Se III
$\mathbf{B}_{60} =$	$-z_8 \mathbf{a}_1 + x_8 \mathbf{a}_2 - x_8 \mathbf{a}_3$	$=$	$-az_8 \hat{\mathbf{x}} + ax_8 \hat{\mathbf{y}} - ax_8 \hat{\mathbf{z}}$	(12i)	Se III
$\mathbf{B}_{61} =$	$x_8 \mathbf{a}_1 + z_8 \mathbf{a}_2 + x_8 \mathbf{a}_3$	$=$	$ax_8 \hat{\mathbf{x}} + az_8 \hat{\mathbf{y}} + ax_8 \hat{\mathbf{z}}$	(12i)	Se III
$\mathbf{B}_{62} =$	$-x_8 \mathbf{a}_1 + z_8 \mathbf{a}_2 - x_8 \mathbf{a}_3$	$=$	$-ax_8 \hat{\mathbf{x}} + az_8 \hat{\mathbf{y}} - ax_8 \hat{\mathbf{z}}$	(12i)	Se III
$\mathbf{B}_{63} =$	$x_8 \mathbf{a}_1 - z_8 \mathbf{a}_2 - x_8 \mathbf{a}_3$	$=$	$ax_8 \hat{\mathbf{x}} - az_8 \hat{\mathbf{y}} - ax_8 \hat{\mathbf{z}}$	(12i)	Se III
$\mathbf{B}_{64} =$	$-x_8 \mathbf{a}_1 - z_8 \mathbf{a}_2 + x_8 \mathbf{a}_3$	$=$	$-ax_8 \hat{\mathbf{x}} - az_8 \hat{\mathbf{y}} + ax_8 \hat{\mathbf{z}}$	(12i)	Se III

## References

- [1] S. Geller, *The Crystal Structure of Pd<sub>17</sub>Se<sub>15</sub>*, Acta Cryst. **15**, 713–721 (1962), doi:10.1107/S0365110X62001929.