

NiBi Structure:

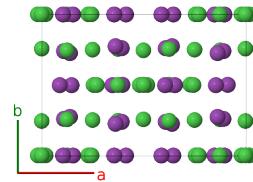
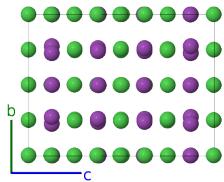
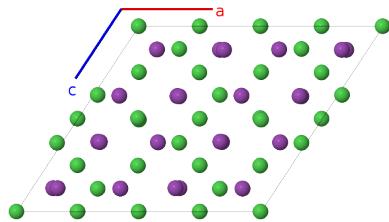
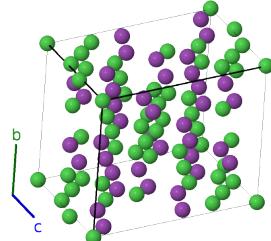
A16B17_mC66_12_4i2j_aeh4ij-001

Cite this page as: H. Eckert, S. Divilov, A. Zettel, M. J. Mehl, D. Hicks, and S. Curtarolo, *The AFLOW Library of Crystallographic Prototypes: Part 4*. In preparation.

<https://aflow.org/p/V4P2>

https://aflow.org/p/A16B17_mC66_12_4i2j_aeh4ij-001

● Bi
● Ni



Prototype BiNi

AFLOW prototype label A16B17_mC66_12_4i2j_aeh4ij-001

ICSD 410878

Pearson symbol mC66

Space group number 12

Space group symbol $C2/m$

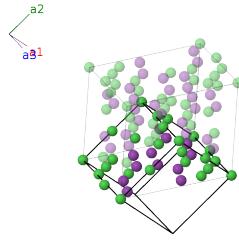
AFLOW prototype command

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x_12,y_12,z_12,x_13,y_13,z_13,x_14,y_14,z_14
```

- In the ideal stoichiometry half of the Ni-VII sites are occupied. Similar structures have compositions $\text{Ni}_x\text{Bi}_{1-x}$ with $x > 1/2$, so it is likely the some of the excess nickel atoms sit on this site.
- (Ruck, 1999) and the ICSD entry put this structure in the $F2/m$ setting of space-group #12, where we can see that it is pseudo-orthorhombic. We used FINDSYM to place this in the standard $C2/m$ setting.

Base-centered Monoclinic primitive vectors

$$\begin{aligned}
\mathbf{a}_1 &= \frac{1}{2}a\hat{\mathbf{x}} - \frac{1}{2}b\hat{\mathbf{y}} \\
\mathbf{a}_2 &= \frac{1}{2}a\hat{\mathbf{x}} + \frac{1}{2}b\hat{\mathbf{y}} \\
\mathbf{a}_3 &= c \cos \beta \hat{\mathbf{x}} + c \sin \beta \hat{\mathbf{z}}
\end{aligned}$$



Basis vectors

	Lattice coordinates	=	Cartesian coordinates	Wyckoff position	Atom type
\mathbf{B}_1	0	=	0	(2a)	Ni I
\mathbf{B}_2	$\frac{1}{2}\mathbf{a}_2$	=	$\frac{1}{4}a\hat{\mathbf{x}} + \frac{1}{4}b\hat{\mathbf{y}}$	(4e)	Ni II
\mathbf{B}_3	$\frac{1}{2}\mathbf{a}_1$	=	$\frac{1}{4}a\hat{\mathbf{x}} - \frac{1}{4}b\hat{\mathbf{y}}$	(4e)	Ni II
\mathbf{B}_4	$-y_3 \mathbf{a}_1 + y_3 \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	=	$\frac{1}{2}c \cos \beta \hat{\mathbf{x}} + b y_3 \hat{\mathbf{y}} + \frac{1}{2}c \sin \beta \hat{\mathbf{z}}$	(4h)	Ni III
\mathbf{B}_5	$y_3 \mathbf{a}_1 - y_3 \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	=	$\frac{1}{2}c \cos \beta \hat{\mathbf{x}} - b y_3 \hat{\mathbf{y}} + \frac{1}{2}c \sin \beta \hat{\mathbf{z}}$	(4h)	Ni III
\mathbf{B}_6	$x_4 \mathbf{a}_1 + x_4 \mathbf{a}_2 + z_4 \mathbf{a}_3$	=	$(ax_4 + cz_4 \cos \beta) \hat{\mathbf{x}} + cz_4 \sin \beta \hat{\mathbf{z}}$	(4i)	Bi I
\mathbf{B}_7	$-x_4 \mathbf{a}_1 - x_4 \mathbf{a}_2 - z_4 \mathbf{a}_3$	=	$-(ax_4 + cz_4 \cos \beta) \hat{\mathbf{x}} - cz_4 \sin \beta \hat{\mathbf{z}}$	(4i)	Bi I
\mathbf{B}_8	$x_5 \mathbf{a}_1 + x_5 \mathbf{a}_2 + z_5 \mathbf{a}_3$	=	$(ax_5 + cz_5 \cos \beta) \hat{\mathbf{x}} + cz_5 \sin \beta \hat{\mathbf{z}}$	(4i)	Bi II
\mathbf{B}_9	$-x_5 \mathbf{a}_1 - x_5 \mathbf{a}_2 - z_5 \mathbf{a}_3$	=	$-(ax_5 + cz_5 \cos \beta) \hat{\mathbf{x}} - cz_5 \sin \beta \hat{\mathbf{z}}$	(4i)	Bi II
\mathbf{B}_{10}	$x_6 \mathbf{a}_1 + x_6 \mathbf{a}_2 + z_6 \mathbf{a}_3$	=	$(ax_6 + cz_6 \cos \beta) \hat{\mathbf{x}} + cz_6 \sin \beta \hat{\mathbf{z}}$	(4i)	Bi III
\mathbf{B}_{11}	$-x_6 \mathbf{a}_1 - x_6 \mathbf{a}_2 - z_6 \mathbf{a}_3$	=	$-(ax_6 + cz_6 \cos \beta) \hat{\mathbf{x}} - cz_6 \sin \beta \hat{\mathbf{z}}$	(4i)	Bi III
\mathbf{B}_{12}	$x_7 \mathbf{a}_1 + x_7 \mathbf{a}_2 + z_7 \mathbf{a}_3$	=	$(ax_7 + cz_7 \cos \beta) \hat{\mathbf{x}} + cz_7 \sin \beta \hat{\mathbf{z}}$	(4i)	Bi IV
\mathbf{B}_{13}	$-x_7 \mathbf{a}_1 - x_7 \mathbf{a}_2 - z_7 \mathbf{a}_3$	=	$-(ax_7 + cz_7 \cos \beta) \hat{\mathbf{x}} - cz_7 \sin \beta \hat{\mathbf{z}}$	(4i)	Bi IV
\mathbf{B}_{14}	$x_8 \mathbf{a}_1 + x_8 \mathbf{a}_2 + z_8 \mathbf{a}_3$	=	$(ax_8 + cz_8 \cos \beta) \hat{\mathbf{x}} + cz_8 \sin \beta \hat{\mathbf{z}}$	(4i)	Ni IV
\mathbf{B}_{15}	$-x_8 \mathbf{a}_1 - x_8 \mathbf{a}_2 - z_8 \mathbf{a}_3$	=	$-(ax_8 + cz_8 \cos \beta) \hat{\mathbf{x}} - cz_8 \sin \beta \hat{\mathbf{z}}$	(4i)	Ni IV
\mathbf{B}_{16}	$x_9 \mathbf{a}_1 + x_9 \mathbf{a}_2 + z_9 \mathbf{a}_3$	=	$(ax_9 + cz_9 \cos \beta) \hat{\mathbf{x}} + cz_9 \sin \beta \hat{\mathbf{z}}$	(4i)	Ni V
\mathbf{B}_{17}	$-x_9 \mathbf{a}_1 - x_9 \mathbf{a}_2 - z_9 \mathbf{a}_3$	=	$-(ax_9 + cz_9 \cos \beta) \hat{\mathbf{x}} - cz_9 \sin \beta \hat{\mathbf{z}}$	(4i)	Ni V
\mathbf{B}_{18}	$x_{10} \mathbf{a}_1 + x_{10} \mathbf{a}_2 + z_{10} \mathbf{a}_3$	=	$(ax_{10} + cz_{10} \cos \beta) \hat{\mathbf{x}} + cz_{10} \sin \beta \hat{\mathbf{z}}$	(4i)	Ni VI
\mathbf{B}_{19}	$-x_{10} \mathbf{a}_1 - x_{10} \mathbf{a}_2 - z_{10} \mathbf{a}_3$	=	$-(ax_{10} + cz_{10} \cos \beta) \hat{\mathbf{x}} - cz_{10} \sin \beta \hat{\mathbf{z}}$	(4i)	Ni VI
\mathbf{B}_{20}	$x_{11} \mathbf{a}_1 + x_{11} \mathbf{a}_2 + z_{11} \mathbf{a}_3$	=	$(ax_{11} + cz_{11} \cos \beta) \hat{\mathbf{x}} + cz_{11} \sin \beta \hat{\mathbf{z}}$	(4i)	Ni VII
\mathbf{B}_{21}	$-x_{11} \mathbf{a}_1 - x_{11} \mathbf{a}_2 - z_{11} \mathbf{a}_3$	=	$-(ax_{11} + cz_{11} \cos \beta) \hat{\mathbf{x}} - cz_{11} \sin \beta \hat{\mathbf{z}}$	(4i)	Ni VII
\mathbf{B}_{22}	$(x_{12} - y_{12}) \mathbf{a}_1 + (x_{12} + y_{12}) \mathbf{a}_2 + z_{12} \mathbf{a}_3$	=	$(ax_{12} + cz_{12} \cos \beta) \hat{\mathbf{x}} + by_{12} \hat{\mathbf{y}} + cz_{12} \sin \beta \hat{\mathbf{z}}$	(8j)	Bi V
\mathbf{B}_{23}	$-(x_{12} + y_{12}) \mathbf{a}_1 - (x_{12} - y_{12}) \mathbf{a}_2 - z_{12} \mathbf{a}_3$	=	$-(ax_{12} + cz_{12} \cos \beta) \hat{\mathbf{x}} + by_{12} \hat{\mathbf{y}} - cz_{12} \sin \beta \hat{\mathbf{z}}$	(8j)	Bi V
\mathbf{B}_{24}	$-(x_{12} - y_{12}) \mathbf{a}_1 - (x_{12} + y_{12}) \mathbf{a}_2 - z_{12} \mathbf{a}_3$	=	$-(ax_{12} + cz_{12} \cos \beta) \hat{\mathbf{x}} - by_{12} \hat{\mathbf{y}} - cz_{12} \sin \beta \hat{\mathbf{z}}$	(8j)	Bi V
\mathbf{B}_{25}	$(x_{12} + y_{12}) \mathbf{a}_1 + (x_{12} - y_{12}) \mathbf{a}_2 + z_{12} \mathbf{a}_3$	=	$(ax_{12} + cz_{12} \cos \beta) \hat{\mathbf{x}} - by_{12} \hat{\mathbf{y}} + cz_{12} \sin \beta \hat{\mathbf{z}}$	(8j)	Bi V
\mathbf{B}_{26}	$(x_{13} - y_{13}) \mathbf{a}_1 + (x_{13} + y_{13}) \mathbf{a}_2 + z_{13} \mathbf{a}_3$	=	$(ax_{13} + cz_{13} \cos \beta) \hat{\mathbf{x}} + by_{13} \hat{\mathbf{y}} + cz_{13} \sin \beta \hat{\mathbf{z}}$	(8j)	Bi VI
\mathbf{B}_{27}	$-(x_{13} + y_{13}) \mathbf{a}_1 - (x_{13} - y_{13}) \mathbf{a}_2 - z_{13} \mathbf{a}_3$	=	$-(ax_{13} + cz_{13} \cos \beta) \hat{\mathbf{x}} + by_{13} \hat{\mathbf{y}} - cz_{13} \sin \beta \hat{\mathbf{z}}$	(8j)	Bi VI

$$\begin{aligned}
\mathbf{B}_{28} &= -(x_{13} - y_{13}) \mathbf{a}_1 - (x_{13} + y_{13}) \mathbf{a}_2 - z_{13} \mathbf{a}_3 & = & - (ax_{13} + cz_{13} \cos \beta) \hat{\mathbf{x}} - by_{13} \hat{\mathbf{y}} - cz_{13} \sin \beta \hat{\mathbf{z}} & (8j) & \text{Bi VI} \\
\mathbf{B}_{29} &= (x_{13} + y_{13}) \mathbf{a}_1 + (x_{13} - y_{13}) \mathbf{a}_2 + z_{13} \mathbf{a}_3 & = & (ax_{13} + cz_{13} \cos \beta) \hat{\mathbf{x}} - by_{13} \hat{\mathbf{y}} + cz_{13} \sin \beta \hat{\mathbf{z}} & (8j) & \text{Bi VI} \\
\mathbf{B}_{30} &= (x_{14} - y_{14}) \mathbf{a}_1 + (x_{14} + y_{14}) \mathbf{a}_2 + z_{14} \mathbf{a}_3 & = & (ax_{14} + cz_{14} \cos \beta) \hat{\mathbf{x}} + by_{14} \hat{\mathbf{y}} + cz_{14} \sin \beta \hat{\mathbf{z}} & (8j) & \text{Ni VIII} \\
\mathbf{B}_{31} &= -(x_{14} + y_{14}) \mathbf{a}_1 - (x_{14} - y_{14}) \mathbf{a}_2 - z_{14} \mathbf{a}_3 & = & - (ax_{14} + cz_{14} \cos \beta) \hat{\mathbf{x}} + by_{14} \hat{\mathbf{y}} - cz_{14} \sin \beta \hat{\mathbf{z}} & (8j) & \text{Ni VIII} \\
\mathbf{B}_{32} &= -(x_{14} - y_{14}) \mathbf{a}_1 - (x_{14} + y_{14}) \mathbf{a}_2 - z_{14} \mathbf{a}_3 & = & - (ax_{14} + cz_{14} \cos \beta) \hat{\mathbf{x}} - by_{14} \hat{\mathbf{y}} - cz_{14} \sin \beta \hat{\mathbf{z}} & (8j) & \text{Ni VIII} \\
\mathbf{B}_{33} &= (x_{14} + y_{14}) \mathbf{a}_1 + (x_{14} - y_{14}) \mathbf{a}_2 + z_{14} \mathbf{a}_3 & = & (ax_{14} + cz_{14} \cos \beta) \hat{\mathbf{x}} - by_{14} \hat{\mathbf{y}} + cz_{14} \sin \beta \hat{\mathbf{z}} & (8j) & \text{Ni VIII}
\end{aligned}$$

References

[1] M. Ruck, *Die Kristallstruktur von BiNi: eine komplexe Ausdünnungsvariante des InNi₂-Typs*, Z. Anorganische und Allgemeine Chemie **625**, 2050–2054 (1999), doi:10.1002/(SICI)1521-3749(199912)625:12<2050::AID-ZAAC2050>3.0.CO;2-R.

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[1] G. P. Vassilev and K. I. Lillova, *Notes on some supposed transitions of the phase NiBi*, Crys. Res. Technol. **42**, 237–240 (2007), doi:10.1002/crat.200610806.