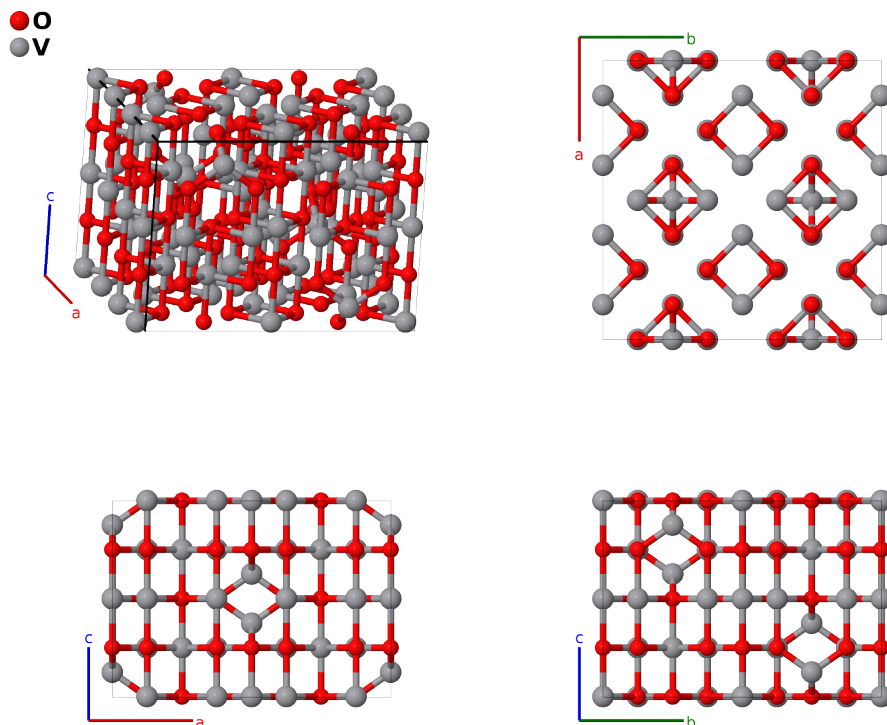


# V<sub>13</sub>O<sub>16</sub> Structure: A16B13\_tI116\_141\_2hi\_a2fh-001

Cite this page as: H. Eckert, S. Divilov, A. Zettel, M. J. Mehl, D. Hicks, and S. Curtarolo, *The AFLOW Library of Crystallographic Prototypes: Part 4*. In preparation.

<https://aflow.org/p/NCQA>

[https://aflow.org/p/A16B13\\_tI116\\_141\\_2hi\\_a2fh-001](https://aflow.org/p/A16B13_tI116_141_2hi_a2fh-001)



Prototype	O <sub>16</sub> V <sub>13</sub>
AFLOW prototype label	A16B13_tI116_141_2hi_a2fh-001
ICSD	77708
Pearson symbol	tI116
Space group number	141
Space group symbol	<i>I</i> 4 <sub>1</sub> / <i>amd</i>
AFLOW prototype command	<code>aflow --proto=A16B13_tI116_141_2hi_a2fh-001 --params=a, c/a, x<sub>2</sub>, x<sub>3</sub>, y<sub>4</sub>, z<sub>4</sub>, y<sub>5</sub>, z<sub>5</sub>, y<sub>6</sub>, z<sub>6</sub>, x<sub>7</sub>, y<sub>7</sub>, z<sub>7</sub></code>

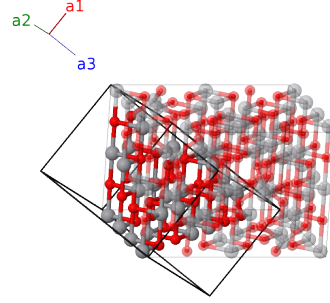
- There are several problems with this structure:
- It is not clear if (Andersson, 1970) put this in the first (4a site at the origin) or second (inversion site at the origin) setting of space group *I*4<sub>1</sub>/*amd* #141.
- Furthermore, they give values for x and z for the (16h) positions, even though the standard definition is (0 y z) in both settings.

- The ICSD entry assumes the first setting, and that the authors meant “y” rather than “x” for the first coordinate, but kept x as “x” for the other Wyckoff positions.
- We follow this convention, using AFLOW to convert that structure to the standard second setting. The result is shown here.
- However, (Andersson, 1970) call this structure a distorted rock salt (*B1*) structure with vacancies on the vanadium sites and interstitial vanadium atoms on the (4a) sites, and our structure look nothing like this.
- Furthermore, the (presumably relaxed) structure found on the Materials Project page (Jain, 2013) has the same symmetry and occupied Wyckoff positions, but is actually much different than this structure.
- We fill investigate this further. If updates are necessary we will revise this page.

---

### Body-centered Tetragonal primitive vectors

$$\begin{aligned} \mathbf{a}_1 &= -\frac{1}{2}a \hat{\mathbf{x}} + \frac{1}{2}a \hat{\mathbf{y}} + \frac{1}{2}c \hat{\mathbf{z}} \\ \mathbf{a}_2 &= \frac{1}{2}a \hat{\mathbf{x}} - \frac{1}{2}a \hat{\mathbf{y}} + \frac{1}{2}c \hat{\mathbf{z}} \\ \mathbf{a}_3 &= \frac{1}{2}a \hat{\mathbf{x}} + \frac{1}{2}a \hat{\mathbf{y}} - \frac{1}{2}c \hat{\mathbf{z}} \end{aligned}$$




---

### Basis vectors

	Lattice coordinates		Cartesian coordinates	Wyckoff position	Atom type
$\mathbf{B}_1$	$= \frac{7}{8} \mathbf{a}_1 + \frac{1}{8} \mathbf{a}_2 + \frac{3}{4} \mathbf{a}_3$	$=$	$\frac{3}{4}a \hat{\mathbf{y}} + \frac{1}{8}c \hat{\mathbf{z}}$	(4a)	V I
$\mathbf{B}_2$	$= \frac{1}{8} \mathbf{a}_1 + \frac{7}{8} \mathbf{a}_2 + \frac{1}{4} \mathbf{a}_3$	$=$	$\frac{1}{2}a \hat{\mathbf{x}} - \frac{1}{4}a \hat{\mathbf{y}} + \frac{3}{8}c \hat{\mathbf{z}}$	(4a)	V I
$\mathbf{B}_3$	$= x_2 \mathbf{a}_2 + x_2 \mathbf{a}_3$	$=$	$ax_2 \hat{\mathbf{x}}$	(16f)	V II
$\mathbf{B}_4$	$= \frac{1}{2} \mathbf{a}_1 - x_2 \mathbf{a}_2 - (x_2 - \frac{1}{2}) \mathbf{a}_3$	$=$	$-ax_2 \hat{\mathbf{x}} + \frac{1}{2}a \hat{\mathbf{y}}$	(16f)	V II
$\mathbf{B}_5$	$= x_2 \mathbf{a}_1 + \frac{1}{2} \mathbf{a}_2 + x_2 \mathbf{a}_3$	$=$	$\frac{1}{4}a \hat{\mathbf{x}} + a(x_2 - \frac{1}{4}) \hat{\mathbf{y}} + \frac{1}{4}c \hat{\mathbf{z}}$	(16f)	V II
$\mathbf{B}_6$	$= -x_2 \mathbf{a}_1 - (x_2 - \frac{1}{2}) \mathbf{a}_3$	$=$	$\frac{1}{4}a \hat{\mathbf{x}} - a(x_2 - \frac{1}{4}) \hat{\mathbf{y}} - \frac{1}{4}c \hat{\mathbf{z}}$	(16f)	V II
$\mathbf{B}_7$	$= -x_2 \mathbf{a}_2 - x_2 \mathbf{a}_3$	$=$	$-ax_2 \hat{\mathbf{x}}$	(16f)	V II
$\mathbf{B}_8$	$= \frac{1}{2} \mathbf{a}_1 + x_2 \mathbf{a}_2 + (x_2 + \frac{1}{2}) \mathbf{a}_3$	$=$	$ax_2 \hat{\mathbf{x}} + \frac{1}{2}a \hat{\mathbf{y}}$	(16f)	V II
$\mathbf{B}_9$	$= -x_2 \mathbf{a}_1 + \frac{1}{2} \mathbf{a}_2 - x_2 \mathbf{a}_3$	$=$	$\frac{1}{4}a \hat{\mathbf{x}} - a(x_2 + \frac{1}{4}) \hat{\mathbf{y}} + \frac{1}{4}c \hat{\mathbf{z}}$	(16f)	V II
$\mathbf{B}_{10}$	$= x_2 \mathbf{a}_1 + (x_2 + \frac{1}{2}) \mathbf{a}_3$	$=$	$\frac{1}{4}a \hat{\mathbf{x}} + a(x_2 + \frac{1}{4}) \hat{\mathbf{y}} - \frac{1}{4}c \hat{\mathbf{z}}$	(16f)	V II
$\mathbf{B}_{11}$	$= x_3 \mathbf{a}_2 + x_3 \mathbf{a}_3$	$=$	$ax_3 \hat{\mathbf{x}}$	(16f)	V III
$\mathbf{B}_{12}$	$= \frac{1}{2} \mathbf{a}_1 - x_3 \mathbf{a}_2 - (x_3 - \frac{1}{2}) \mathbf{a}_3$	$=$	$-ax_3 \hat{\mathbf{x}} + \frac{1}{2}a \hat{\mathbf{y}}$	(16f)	V III
$\mathbf{B}_{13}$	$= x_3 \mathbf{a}_1 + \frac{1}{2} \mathbf{a}_2 + x_3 \mathbf{a}_3$	$=$	$\frac{1}{4}a \hat{\mathbf{x}} + a(x_3 - \frac{1}{4}) \hat{\mathbf{y}} + \frac{1}{4}c \hat{\mathbf{z}}$	(16f)	V III
$\mathbf{B}_{14}$	$= -x_3 \mathbf{a}_1 - (x_3 - \frac{1}{2}) \mathbf{a}_3$	$=$	$\frac{1}{4}a \hat{\mathbf{x}} - a(x_3 - \frac{1}{4}) \hat{\mathbf{y}} - \frac{1}{4}c \hat{\mathbf{z}}$	(16f)	V III
$\mathbf{B}_{15}$	$= -x_3 \mathbf{a}_2 - x_3 \mathbf{a}_3$	$=$	$-ax_3 \hat{\mathbf{x}}$	(16f)	V III
$\mathbf{B}_{16}$	$= \frac{1}{2} \mathbf{a}_1 + x_3 \mathbf{a}_2 + (x_3 + \frac{1}{2}) \mathbf{a}_3$	$=$	$ax_3 \hat{\mathbf{x}} + \frac{1}{2}a \hat{\mathbf{y}}$	(16f)	V III
$\mathbf{B}_{17}$	$= -x_3 \mathbf{a}_1 + \frac{1}{2} \mathbf{a}_2 - x_3 \mathbf{a}_3$	$=$	$\frac{1}{4}a \hat{\mathbf{x}} - a(x_3 + \frac{1}{4}) \hat{\mathbf{y}} + \frac{1}{4}c \hat{\mathbf{z}}$	(16f)	V III
$\mathbf{B}_{18}$	$= x_3 \mathbf{a}_1 + (x_3 + \frac{1}{2}) \mathbf{a}_3$	$=$	$\frac{1}{4}a \hat{\mathbf{x}} + a(x_3 + \frac{1}{4}) \hat{\mathbf{y}} - \frac{1}{4}c \hat{\mathbf{z}}$	(16f)	V III
$\mathbf{B}_{19}$	$= (y_4 + z_4) \mathbf{a}_1 + z_4 \mathbf{a}_2 + y_4 \mathbf{a}_3$	$=$	$ay_4 \hat{\mathbf{y}} + cz_4 \hat{\mathbf{z}}$	(16h)	O I



$$\begin{aligned}
\mathbf{B}_{49} &= \begin{pmatrix} (x_7 - z_7) \mathbf{a}_1 + \\ (y_7 - z_7 + \frac{1}{2}) \mathbf{a}_2 + (x_7 + y_7) \mathbf{a}_3 \end{pmatrix} = a \left( y_7 + \frac{1}{4} \right) \hat{\mathbf{x}} + a \left( x_7 - \frac{1}{4} \right) \hat{\mathbf{y}} - c \left( z_7 - \frac{1}{4} \right) \hat{\mathbf{z}} & (32i) & \text{O III} \\
\mathbf{B}_{50} &= \begin{pmatrix} -(x_7 + z_7) \mathbf{a}_1 - (y_7 + z_7) \mathbf{a}_2 - \\ (x_7 + y_7 - \frac{1}{2}) \mathbf{a}_3 \end{pmatrix} = -a \left( y_7 - \frac{1}{4} \right) \hat{\mathbf{x}} - a \left( x_7 - \frac{1}{4} \right) \hat{\mathbf{y}} - c \left( z_7 + \frac{1}{4} \right) \hat{\mathbf{z}} & (32i) & \text{O III} \\
\mathbf{B}_{51} &= \begin{pmatrix} -(y_7 + z_7) \mathbf{a}_1 - (x_7 + z_7) \mathbf{a}_2 - \\ (x_7 + y_7) \mathbf{a}_3 \end{pmatrix} = -ax_7 \hat{\mathbf{x}} - ay_7 \hat{\mathbf{y}} - cz_7 \hat{\mathbf{z}} & (32i) & \text{O III} \\
\mathbf{B}_{52} &= \begin{pmatrix} (y_7 - z_7 + \frac{1}{2}) \mathbf{a}_1 + \\ (x_7 - z_7) \mathbf{a}_2 + (x_7 + y_7 + \frac{1}{2}) \mathbf{a}_3 \end{pmatrix} = ax_7 \hat{\mathbf{x}} + a \left( y_7 + \frac{1}{2} \right) \hat{\mathbf{y}} - cz_7 \hat{\mathbf{z}} & (32i) & \text{O III} \\
\mathbf{B}_{53} &= \begin{pmatrix} -(x_7 + z_7) \mathbf{a}_1 + \\ (y_7 - z_7 + \frac{1}{2}) \mathbf{a}_2 - (x_7 - y_7) \mathbf{a}_3 \end{pmatrix} = a \left( y_7 + \frac{1}{4} \right) \hat{\mathbf{x}} - a \left( x_7 + \frac{1}{4} \right) \hat{\mathbf{y}} - c \left( z_7 - \frac{1}{4} \right) \hat{\mathbf{z}} & (32i) & \text{O III} \\
\mathbf{B}_{54} &= \begin{pmatrix} (x_7 - z_7) \mathbf{a}_1 - (y_7 + z_7) \mathbf{a}_2 + \\ (x_7 - y_7 + \frac{1}{2}) \mathbf{a}_3 \end{pmatrix} = -a \left( y_7 - \frac{1}{4} \right) \hat{\mathbf{x}} + a \left( x_7 + \frac{1}{4} \right) \hat{\mathbf{y}} - c \left( z_7 + \frac{1}{4} \right) \hat{\mathbf{z}} & (32i) & \text{O III} \\
\mathbf{B}_{55} &= \begin{pmatrix} (-y_7 + z_7 + \frac{1}{2}) \mathbf{a}_1 + \\ (x_7 + z_7) \mathbf{a}_2 + (x_7 - y_7 + \frac{1}{2}) \mathbf{a}_3 \end{pmatrix} = ax_7 \hat{\mathbf{x}} - a \left( y_7 - \frac{1}{2} \right) \hat{\mathbf{y}} + cz_7 \hat{\mathbf{z}} & (32i) & \text{O III} \\
\mathbf{B}_{56} &= \begin{pmatrix} (y_7 + z_7) \mathbf{a}_1 - (x_7 - z_7) \mathbf{a}_2 - \\ (x_7 - y_7) \mathbf{a}_3 \end{pmatrix} = -ax_7 \hat{\mathbf{x}} + ay_7 \hat{\mathbf{y}} + cz_7 \hat{\mathbf{z}} & (32i) & \text{O III} \\
\mathbf{B}_{57} &= \begin{pmatrix} -(x_7 - z_7) \mathbf{a}_1 + \\ (-y_7 + z_7 + \frac{1}{2}) \mathbf{a}_2 - (x_7 + y_7) \mathbf{a}_3 \end{pmatrix} = -a \left( y_7 - \frac{1}{4} \right) \hat{\mathbf{x}} - a \left( x_7 + \frac{1}{4} \right) \hat{\mathbf{y}} + c \left( z_7 + \frac{1}{4} \right) \hat{\mathbf{z}} & (32i) & \text{O III} \\
\mathbf{B}_{58} &= \begin{pmatrix} (x_7 + z_7) \mathbf{a}_1 + (y_7 + z_7) \mathbf{a}_2 + \\ (x_7 + y_7 + \frac{1}{2}) \mathbf{a}_3 \end{pmatrix} = a \left( y_7 + \frac{1}{4} \right) \hat{\mathbf{x}} + a \left( x_7 + \frac{1}{4} \right) \hat{\mathbf{y}} + c \left( z_7 - \frac{1}{4} \right) \hat{\mathbf{z}} & (32i) & \text{O III}
\end{aligned}$$

## References

- [1] B. Andersson and J. Gj, *Ordered Phases in the Monoxide Region of the Vanadium-Oxygen System*, Acta Chem. Scand. **24**, 2250–2252 (1970), doi:10.3891/acta.chem.scand.24-2250.

## Found in

- [1] A. Jain, S. Ping, G. Hautier, W. Chen, W. D. Richards, S. Dacek, S. Cholia, D. Gunter, D. Skinner, G. Ceder, and K. A. Persson, *Commentary: The Materials Project: A materials genome approach to accelerating materials innovation*, APL Materials **1**, 011002 (2013), doi:10.1063/1.4812323. V<sub>13</sub>O<sub>16</sub>, mp-30065.