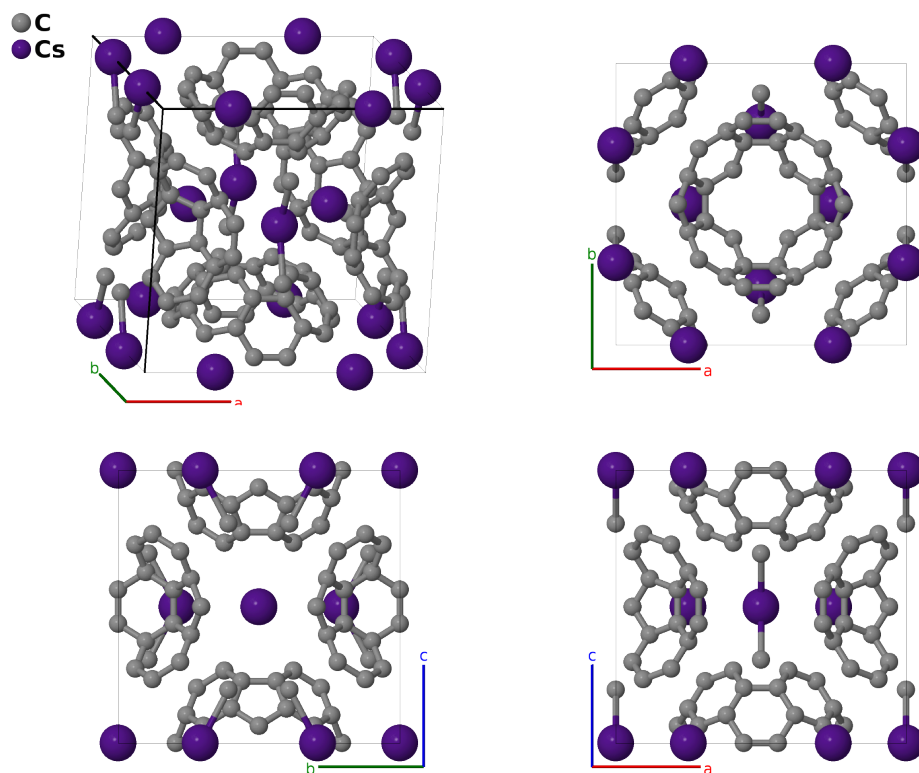


Orthorhombic Fullerene (Cs_3C_{60}) Structure: A15B_oI128_71_lmn6o_eg-001

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<https://aflow.org/p/88NV>

https://aflow.org/p/A15B_oI128_71_lmn6o_eg-001

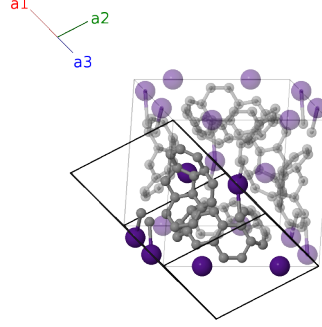


Prototype	C_{60}Cs_3
AFLOW prototype label	A15B_oI128_71_lmn6o_eg-001
ICSD	None
Pearson symbol	oI128
Space group number	71
Space group symbol	$Immm$
AFLOW prototype command	<pre>aflow --proto=A15B_oI128_71_lmn6o_eg-001 --params=a,b/a,c/a,x1,y2,y3,z3,x4,z4,x5,y5,x6,y6,z6,x7,y7,z7,x8,y8,z8,x9,y9, z9,x10,y10,z10,x11,y11,z11</pre>

- The Cesium (4e) and (4g) sites each have 75% occupancy.

Body-centered Orthorhombic primitive vectors

$$\begin{aligned}\mathbf{a}_1 &= -\frac{1}{2}a \hat{\mathbf{x}} + \frac{1}{2}b \hat{\mathbf{y}} + \frac{1}{2}c \hat{\mathbf{z}} \\ \mathbf{a}_2 &= \frac{1}{2}a \hat{\mathbf{x}} - \frac{1}{2}b \hat{\mathbf{y}} + \frac{1}{2}c \hat{\mathbf{z}} \\ \mathbf{a}_3 &= \frac{1}{2}a \hat{\mathbf{x}} + \frac{1}{2}b \hat{\mathbf{y}} - \frac{1}{2}c \hat{\mathbf{z}}\end{aligned}$$



Basis vectors

	Lattice coordinates		Cartesian coordinates	Wyckoff position	Atom type
\mathbf{B}_1	$= x_1 \mathbf{a}_2 + x_1 \mathbf{a}_3$	$=$	$ax_1 \hat{\mathbf{x}}$	(4e)	Cs I
\mathbf{B}_2	$= -x_1 \mathbf{a}_2 - x_1 \mathbf{a}_3$	$=$	$-ax_1 \hat{\mathbf{x}}$	(4e)	Cs I
\mathbf{B}_3	$= y_2 \mathbf{a}_1 + y_2 \mathbf{a}_3$	$=$	$by_2 \hat{\mathbf{y}}$	(4g)	Cs II
\mathbf{B}_4	$= -y_2 \mathbf{a}_1 - y_2 \mathbf{a}_3$	$=$	$-by_2 \hat{\mathbf{y}}$	(4g)	Cs II
\mathbf{B}_5	$= (y_3 + z_3) \mathbf{a}_1 + z_3 \mathbf{a}_2 + y_3 \mathbf{a}_3$	$=$	$by_3 \hat{\mathbf{y}} + cz_3 \hat{\mathbf{z}}$	(8l)	C I
\mathbf{B}_6	$= -(y_3 - z_3) \mathbf{a}_1 + z_3 \mathbf{a}_2 - y_3 \mathbf{a}_3$	$=$	$-by_3 \hat{\mathbf{y}} + cz_3 \hat{\mathbf{z}}$	(8l)	C I
\mathbf{B}_7	$= (y_3 - z_3) \mathbf{a}_1 - z_3 \mathbf{a}_2 + y_3 \mathbf{a}_3$	$=$	$by_3 \hat{\mathbf{y}} - cz_3 \hat{\mathbf{z}}$	(8l)	C I
\mathbf{B}_8	$= -(y_3 + z_3) \mathbf{a}_1 - z_3 \mathbf{a}_2 - y_3 \mathbf{a}_3$	$=$	$-by_3 \hat{\mathbf{y}} - cz_3 \hat{\mathbf{z}}$	(8l)	C I
\mathbf{B}_9	$= z_4 \mathbf{a}_1 + (x_4 + z_4) \mathbf{a}_2 + x_4 \mathbf{a}_3$	$=$	$ax_4 \hat{\mathbf{x}} + cz_4 \hat{\mathbf{z}}$	(8m)	C II
\mathbf{B}_{10}	$= z_4 \mathbf{a}_1 - (x_4 - z_4) \mathbf{a}_2 - x_4 \mathbf{a}_3$	$=$	$-ax_4 \hat{\mathbf{x}} + cz_4 \hat{\mathbf{z}}$	(8m)	C II
\mathbf{B}_{11}	$= -z_4 \mathbf{a}_1 - (x_4 + z_4) \mathbf{a}_2 - x_4 \mathbf{a}_3$	$=$	$-ax_4 \hat{\mathbf{x}} - cz_4 \hat{\mathbf{z}}$	(8m)	C II
\mathbf{B}_{12}	$= -z_4 \mathbf{a}_1 + (x_4 - z_4) \mathbf{a}_2 + x_4 \mathbf{a}_3$	$=$	$ax_4 \hat{\mathbf{x}} - cz_4 \hat{\mathbf{z}}$	(8m)	C II
\mathbf{B}_{13}	$= y_5 \mathbf{a}_1 + x_5 \mathbf{a}_2 + (x_5 + y_5) \mathbf{a}_3$	$=$	$ax_5 \hat{\mathbf{x}} + by_5 \hat{\mathbf{y}}$	(8n)	C III
\mathbf{B}_{14}	$= -y_5 \mathbf{a}_1 - x_5 \mathbf{a}_2 - (x_5 + y_5) \mathbf{a}_3$	$=$	$-ax_5 \hat{\mathbf{x}} - by_5 \hat{\mathbf{y}}$	(8n)	C III
\mathbf{B}_{15}	$= y_5 \mathbf{a}_1 - x_5 \mathbf{a}_2 - (x_5 - y_5) \mathbf{a}_3$	$=$	$-ax_5 \hat{\mathbf{x}} + by_5 \hat{\mathbf{y}}$	(8n)	C III
\mathbf{B}_{16}	$= -y_5 \mathbf{a}_1 + x_5 \mathbf{a}_2 + (x_5 - y_5) \mathbf{a}_3$	$=$	$ax_5 \hat{\mathbf{x}} - by_5 \hat{\mathbf{y}}$	(8n)	C III
\mathbf{B}_{17}	$= (y_6 + z_6) \mathbf{a}_1 + (x_6 + z_6) \mathbf{a}_2 + (x_6 + y_6) \mathbf{a}_3$	$=$	$ax_6 \hat{\mathbf{x}} + by_6 \hat{\mathbf{y}} + cz_6 \hat{\mathbf{z}}$	(16o)	C IV
\mathbf{B}_{18}	$= -(y_6 - z_6) \mathbf{a}_1 - (x_6 - z_6) \mathbf{a}_2 - (x_6 + y_6) \mathbf{a}_3$	$=$	$-ax_6 \hat{\mathbf{x}} - by_6 \hat{\mathbf{y}} + cz_6 \hat{\mathbf{z}}$	(16o)	C IV
\mathbf{B}_{19}	$= (y_6 - z_6) \mathbf{a}_1 - (x_6 + z_6) \mathbf{a}_2 - (x_6 - y_6) \mathbf{a}_3$	$=$	$-ax_6 \hat{\mathbf{x}} + by_6 \hat{\mathbf{y}} - cz_6 \hat{\mathbf{z}}$	(16o)	C IV
\mathbf{B}_{20}	$= -(y_6 + z_6) \mathbf{a}_1 + (x_6 - z_6) \mathbf{a}_2 + (x_6 - y_6) \mathbf{a}_3$	$=$	$ax_6 \hat{\mathbf{x}} - by_6 \hat{\mathbf{y}} - cz_6 \hat{\mathbf{z}}$	(16o)	C IV
\mathbf{B}_{21}	$= -(y_6 + z_6) \mathbf{a}_1 - (x_6 + z_6) \mathbf{a}_2 - (x_6 + y_6) \mathbf{a}_3$	$=$	$-ax_6 \hat{\mathbf{x}} - by_6 \hat{\mathbf{y}} - cz_6 \hat{\mathbf{z}}$	(16o)	C IV
\mathbf{B}_{22}	$= (y_6 - z_6) \mathbf{a}_1 + (x_6 - z_6) \mathbf{a}_2 + (x_6 + y_6) \mathbf{a}_3$	$=$	$ax_6 \hat{\mathbf{x}} + by_6 \hat{\mathbf{y}} - cz_6 \hat{\mathbf{z}}$	(16o)	C IV
\mathbf{B}_{23}	$= -(y_6 - z_6) \mathbf{a}_1 + (x_6 + z_6) \mathbf{a}_2 + (x_6 - y_6) \mathbf{a}_3$	$=$	$ax_6 \hat{\mathbf{x}} - by_6 \hat{\mathbf{y}} + cz_6 \hat{\mathbf{z}}$	(16o)	C IV

$$\begin{aligned}
\mathbf{B}_{48} &= \begin{pmatrix} (y_9 + z_9) \mathbf{a}_1 - (x_9 - z_9) \mathbf{a}_2 - \\ (x_9 - y_9) \mathbf{a}_3 \end{pmatrix} = -ax_9 \hat{\mathbf{x}} + by_9 \hat{\mathbf{y}} + cz_9 \hat{\mathbf{z}} & (16o) & \text{C VII} \\
\mathbf{B}_{49} &= \begin{pmatrix} (y_{10} + z_{10}) \mathbf{a}_1 + (x_{10} + z_{10}) \mathbf{a}_2 + \\ (x_{10} + y_{10}) \mathbf{a}_3 \end{pmatrix} = ax_{10} \hat{\mathbf{x}} + by_{10} \hat{\mathbf{y}} + cz_{10} \hat{\mathbf{z}} & (16o) & \text{C VIII} \\
\mathbf{B}_{50} &= \begin{pmatrix} -(y_{10} - z_{10}) \mathbf{a}_1 - \\ (x_{10} - z_{10}) \mathbf{a}_2 - (x_{10} + y_{10}) \mathbf{a}_3 \end{pmatrix} = -ax_{10} \hat{\mathbf{x}} - by_{10} \hat{\mathbf{y}} + cz_{10} \hat{\mathbf{z}} & (16o) & \text{C VIII} \\
\mathbf{B}_{51} &= \begin{pmatrix} (y_{10} - z_{10}) \mathbf{a}_1 - (x_{10} + z_{10}) \mathbf{a}_2 - \\ (x_{10} - y_{10}) \mathbf{a}_3 \end{pmatrix} = -ax_{10} \hat{\mathbf{x}} + by_{10} \hat{\mathbf{y}} - cz_{10} \hat{\mathbf{z}} & (16o) & \text{C VIII} \\
\mathbf{B}_{52} &= \begin{pmatrix} -(y_{10} + z_{10}) \mathbf{a}_1 + \\ (x_{10} - z_{10}) \mathbf{a}_2 + (x_{10} - y_{10}) \mathbf{a}_3 \end{pmatrix} = ax_{10} \hat{\mathbf{x}} - by_{10} \hat{\mathbf{y}} - cz_{10} \hat{\mathbf{z}} & (16o) & \text{C VIII} \\
\mathbf{B}_{53} &= \begin{pmatrix} -(y_{10} + z_{10}) \mathbf{a}_1 - \\ (x_{10} + z_{10}) \mathbf{a}_2 - (x_{10} + y_{10}) \mathbf{a}_3 \end{pmatrix} = -ax_{10} \hat{\mathbf{x}} - by_{10} \hat{\mathbf{y}} - cz_{10} \hat{\mathbf{z}} & (16o) & \text{C VIII} \\
\mathbf{B}_{54} &= \begin{pmatrix} (y_{10} - z_{10}) \mathbf{a}_1 + (x_{10} - z_{10}) \mathbf{a}_2 + \\ (x_{10} + y_{10}) \mathbf{a}_3 \end{pmatrix} = ax_{10} \hat{\mathbf{x}} + by_{10} \hat{\mathbf{y}} - cz_{10} \hat{\mathbf{z}} & (16o) & \text{C VIII} \\
\mathbf{B}_{55} &= \begin{pmatrix} -(y_{10} - z_{10}) \mathbf{a}_1 + \\ (x_{10} + z_{10}) \mathbf{a}_2 + (x_{10} - y_{10}) \mathbf{a}_3 \end{pmatrix} = ax_{10} \hat{\mathbf{x}} - by_{10} \hat{\mathbf{y}} + cz_{10} \hat{\mathbf{z}} & (16o) & \text{C VIII} \\
\mathbf{B}_{56} &= \begin{pmatrix} (y_{10} + z_{10}) \mathbf{a}_1 - (x_{10} - z_{10}) \mathbf{a}_2 - \\ (x_{10} - y_{10}) \mathbf{a}_3 \end{pmatrix} = -ax_{10} \hat{\mathbf{x}} + by_{10} \hat{\mathbf{y}} + cz_{10} \hat{\mathbf{z}} & (16o) & \text{C VIII} \\
\mathbf{B}_{57} &= \begin{pmatrix} (y_{11} + z_{11}) \mathbf{a}_1 + (x_{11} + z_{11}) \mathbf{a}_2 + \\ (x_{11} + y_{11}) \mathbf{a}_3 \end{pmatrix} = ax_{11} \hat{\mathbf{x}} + by_{11} \hat{\mathbf{y}} + cz_{11} \hat{\mathbf{z}} & (16o) & \text{C IX} \\
\mathbf{B}_{58} &= \begin{pmatrix} -(y_{11} - z_{11}) \mathbf{a}_1 - \\ (x_{11} - z_{11}) \mathbf{a}_2 - (x_{11} + y_{11}) \mathbf{a}_3 \end{pmatrix} = -ax_{11} \hat{\mathbf{x}} - by_{11} \hat{\mathbf{y}} + cz_{11} \hat{\mathbf{z}} & (16o) & \text{C IX} \\
\mathbf{B}_{59} &= \begin{pmatrix} (y_{11} - z_{11}) \mathbf{a}_1 - (x_{11} + z_{11}) \mathbf{a}_2 - \\ (x_{11} - y_{11}) \mathbf{a}_3 \end{pmatrix} = -ax_{11} \hat{\mathbf{x}} + by_{11} \hat{\mathbf{y}} - cz_{11} \hat{\mathbf{z}} & (16o) & \text{C IX} \\
\mathbf{B}_{60} &= \begin{pmatrix} -(y_{11} + z_{11}) \mathbf{a}_1 + \\ (x_{11} - z_{11}) \mathbf{a}_2 + (x_{11} - y_{11}) \mathbf{a}_3 \end{pmatrix} = ax_{11} \hat{\mathbf{x}} - by_{11} \hat{\mathbf{y}} - cz_{11} \hat{\mathbf{z}} & (16o) & \text{C IX} \\
\mathbf{B}_{61} &= \begin{pmatrix} -(y_{11} + z_{11}) \mathbf{a}_1 - \\ (x_{11} + z_{11}) \mathbf{a}_2 - (x_{11} + y_{11}) \mathbf{a}_3 \end{pmatrix} = -ax_{11} \hat{\mathbf{x}} - by_{11} \hat{\mathbf{y}} - cz_{11} \hat{\mathbf{z}} & (16o) & \text{C IX} \\
\mathbf{B}_{62} &= \begin{pmatrix} (y_{11} - z_{11}) \mathbf{a}_1 + (x_{11} - z_{11}) \mathbf{a}_2 + \\ (x_{11} + y_{11}) \mathbf{a}_3 \end{pmatrix} = ax_{11} \hat{\mathbf{x}} + by_{11} \hat{\mathbf{y}} - cz_{11} \hat{\mathbf{z}} & (16o) & \text{C IX} \\
\mathbf{B}_{63} &= \begin{pmatrix} -(y_{11} - z_{11}) \mathbf{a}_1 + \\ (x_{11} + z_{11}) \mathbf{a}_2 + (x_{11} - y_{11}) \mathbf{a}_3 \end{pmatrix} = ax_{11} \hat{\mathbf{x}} - by_{11} \hat{\mathbf{y}} + cz_{11} \hat{\mathbf{z}} & (16o) & \text{C IX} \\
\mathbf{B}_{64} &= \begin{pmatrix} (y_{11} + z_{11}) \mathbf{a}_1 - (x_{11} - z_{11}) \mathbf{a}_2 - \\ (x_{11} - y_{11}) \mathbf{a}_3 \end{pmatrix} = -ax_{11} \hat{\mathbf{x}} + by_{11} \hat{\mathbf{y}} + cz_{11} \hat{\mathbf{z}} & (16o) & \text{C IX}
\end{aligned}$$

References

- [1] Y. Yoshida, Y. Kubozono, S. Kashino, and Y. Murakami, *Structure and electronic properties of Cs₃C₆₀ under ambient pressure revealed by X-ray diffraction and ESR*, Chem. Phys. Lett. **291**, 31–36 (1998), doi:10.1016/S0009-2614(98)00598-3.