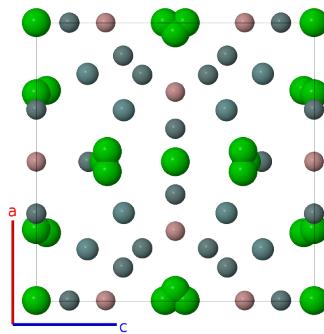
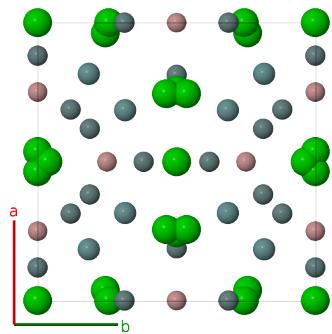
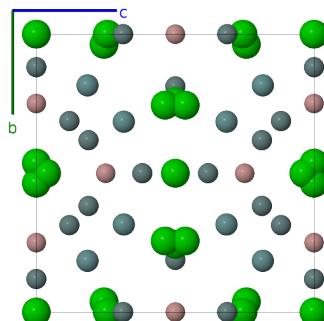
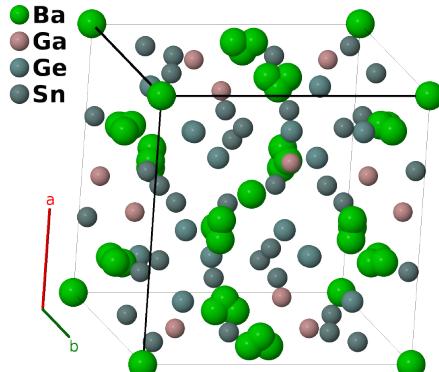


β -Ba₈Ga₁₆Sn₃₀ Clathrate Structure: A13B3C8D12_cP72_223_ak_c_i_k-001

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<https://aflow.org/p/KF6U>

https://aflow.org/p/A13B3C8D12_cP72_223_ak_c_i_k-001



Prototype Ba₄Ga₈Sn₁₅

AFLOW prototype label A13B3C8D12_cP72_223_ak_c_i_k-001

ICSD none

Pearson symbol cP72

Space group number 223

Space group symbol $Pm\bar{3}n$

AFLOW prototype command

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aflow --proto=A13B3C8D12_cP72_223_ak_c_i_k-001  
--params=a,x3,y4,z4,y5,z5
```

Other compounds with this structure

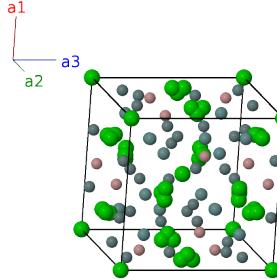
Ba₈Ga₁₆Ge₃₀

- There is a considerable amount of disorder in this system:
 - The (2a) site is pure barium and labeled Ba.

- The (6c) site is pure gallium and labeled Ga.
 - The (16i) site is 64.4% tin and 35.6% gallium. We label this as germanium, Ge, as that is another possible component of this compound and to avoid confusion with the other gallium and tin sites.
 - The first (24k) site is 25% barium, with the remainder of the sites vacant. This can be seen as four-lobed atom clusters in the figure, when it is expanded beyond one unit cell. We label this site as barium, Ba.
 - The final (24k) site is 74.8% tin and 25.2% gallium. We label this as tin, Sn.
- (Aliva, 2006) found another clathrate structure with this stoichiometry, $\alpha\text{-Ba}_8\text{Ga}_{16}\text{Sn}_{30}$.

Simple Cubic primitive vectors

$$\begin{aligned}\mathbf{a}_1 &= a \hat{\mathbf{x}} \\ \mathbf{a}_2 &= a \hat{\mathbf{y}} \\ \mathbf{a}_3 &= a \hat{\mathbf{z}}\end{aligned}$$



Basis vectors

	Lattice coordinates	=	Cartesian coordinates	Wyckoff position	Atom type
\mathbf{B}_1	0	=	0	(2a)	Ba I
\mathbf{B}_2	$\frac{1}{2} \mathbf{a}_1 + \frac{1}{2} \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	=	$\frac{1}{2}a \hat{\mathbf{x}} + \frac{1}{2}a \hat{\mathbf{y}} + \frac{1}{2}a \hat{\mathbf{z}}$	(2a)	Ba I
\mathbf{B}_3	$\frac{1}{4} \mathbf{a}_1 + \frac{1}{2} \mathbf{a}_3$	=	$\frac{1}{4}a \hat{\mathbf{x}} + \frac{1}{2}a \hat{\mathbf{z}}$	(6c)	Ga I
\mathbf{B}_4	$\frac{3}{4} \mathbf{a}_1 + \frac{1}{2} \mathbf{a}_3$	=	$\frac{3}{4}a \hat{\mathbf{x}} + \frac{1}{2}a \hat{\mathbf{z}}$	(6c)	Ga I
\mathbf{B}_5	$\frac{1}{2} \mathbf{a}_1 + \frac{1}{4} \mathbf{a}_2$	=	$\frac{1}{2}a \hat{\mathbf{x}} + \frac{1}{4}a \hat{\mathbf{y}}$	(6c)	Ga I
\mathbf{B}_6	$\frac{1}{2} \mathbf{a}_1 + \frac{3}{4} \mathbf{a}_2$	=	$\frac{1}{2}a \hat{\mathbf{x}} + \frac{3}{4}a \hat{\mathbf{y}}$	(6c)	Ga I
\mathbf{B}_7	$\frac{1}{2} \mathbf{a}_2 + \frac{1}{4} \mathbf{a}_3$	=	$\frac{1}{2}a \hat{\mathbf{y}} + \frac{1}{4}a \hat{\mathbf{z}}$	(6c)	Ga I
\mathbf{B}_8	$\frac{1}{2} \mathbf{a}_2 + \frac{3}{4} \mathbf{a}_3$	=	$\frac{1}{2}a \hat{\mathbf{y}} + \frac{3}{4}a \hat{\mathbf{z}}$	(6c)	Ga I
\mathbf{B}_9	$x_3 \mathbf{a}_1 + x_3 \mathbf{a}_2 + x_3 \mathbf{a}_3$	=	$ax_3 \hat{\mathbf{x}} + ax_3 \hat{\mathbf{y}} + ax_3 \hat{\mathbf{z}}$	(16i)	Ge I
\mathbf{B}_{10}	$-x_3 \mathbf{a}_1 - x_3 \mathbf{a}_2 + x_3 \mathbf{a}_3$	=	$-ax_3 \hat{\mathbf{x}} - ax_3 \hat{\mathbf{y}} + ax_3 \hat{\mathbf{z}}$	(16i)	Ge I
\mathbf{B}_{11}	$-x_3 \mathbf{a}_1 + x_3 \mathbf{a}_2 - x_3 \mathbf{a}_3$	=	$-ax_3 \hat{\mathbf{x}} + ax_3 \hat{\mathbf{y}} - ax_3 \hat{\mathbf{z}}$	(16i)	Ge I
\mathbf{B}_{12}	$x_3 \mathbf{a}_1 - x_3 \mathbf{a}_2 - x_3 \mathbf{a}_3$	=	$ax_3 \hat{\mathbf{x}} - ax_3 \hat{\mathbf{y}} - ax_3 \hat{\mathbf{z}}$	(16i)	Ge I
\mathbf{B}_{13}	$(x_3 + \frac{1}{2}) \mathbf{a}_1 + (x_3 + \frac{1}{2}) \mathbf{a}_2 - (x_3 - \frac{1}{2}) \mathbf{a}_3$	=	$a(x_3 + \frac{1}{2}) \hat{\mathbf{x}} + a(x_3 + \frac{1}{2}) \hat{\mathbf{y}} - a(x_3 - \frac{1}{2}) \hat{\mathbf{z}}$	(16i)	Ge I
\mathbf{B}_{14}	$-(x_3 - \frac{1}{2}) \mathbf{a}_1 - (x_3 - \frac{1}{2}) \mathbf{a}_2 - (x_3 - \frac{1}{2}) \mathbf{a}_3$	=	$-a(x_3 - \frac{1}{2}) \hat{\mathbf{x}} - a(x_3 - \frac{1}{2}) \hat{\mathbf{y}} - a(x_3 - \frac{1}{2}) \hat{\mathbf{z}}$	(16i)	Ge I
\mathbf{B}_{15}	$(x_3 + \frac{1}{2}) \mathbf{a}_1 - (x_3 - \frac{1}{2}) \mathbf{a}_2 + (x_3 + \frac{1}{2}) \mathbf{a}_3$	=	$a(x_3 + \frac{1}{2}) \hat{\mathbf{x}} - a(x_3 - \frac{1}{2}) \hat{\mathbf{y}} + a(x_3 + \frac{1}{2}) \hat{\mathbf{z}}$	(16i)	Ge I
\mathbf{B}_{16}	$-(x_3 - \frac{1}{2}) \mathbf{a}_1 + (x_3 + \frac{1}{2}) \mathbf{a}_2 + (x_3 + \frac{1}{2}) \mathbf{a}_3$	=	$-a(x_3 - \frac{1}{2}) \hat{\mathbf{x}} + a(x_3 + \frac{1}{2}) \hat{\mathbf{y}} + a(x_3 + \frac{1}{2}) \hat{\mathbf{z}}$	(16i)	Ge I
\mathbf{B}_{17}	$-x_3 \mathbf{a}_1 - x_3 \mathbf{a}_2 - x_3 \mathbf{a}_3$	=	$-ax_3 \hat{\mathbf{x}} - ax_3 \hat{\mathbf{y}} - ax_3 \hat{\mathbf{z}}$	(16i)	Ge I
\mathbf{B}_{18}	$x_3 \mathbf{a}_1 + x_3 \mathbf{a}_2 - x_3 \mathbf{a}_3$	=	$ax_3 \hat{\mathbf{x}} + ax_3 \hat{\mathbf{y}} - ax_3 \hat{\mathbf{z}}$	(16i)	Ge I
\mathbf{B}_{19}	$x_3 \mathbf{a}_1 - x_3 \mathbf{a}_2 + x_3 \mathbf{a}_3$	=	$ax_3 \hat{\mathbf{x}} - ax_3 \hat{\mathbf{y}} + ax_3 \hat{\mathbf{z}}$	(16i)	Ge I

$\mathbf{B}_{55} =$	$-z_5 \mathbf{a}_1 + y_5 \mathbf{a}_3$	=	$-az_5 \hat{\mathbf{x}} + ay_5 \hat{\mathbf{z}}$	(24k)	Sn I
$\mathbf{B}_{56} =$	$-z_5 \mathbf{a}_1 - y_5 \mathbf{a}_3$	=	$-az_5 \hat{\mathbf{x}} - ay_5 \hat{\mathbf{z}}$	(24k)	Sn I
$\mathbf{B}_{57} =$	$y_5 \mathbf{a}_1 + z_5 \mathbf{a}_2$	=	$ay_5 \hat{\mathbf{x}} + az_5 \hat{\mathbf{y}}$	(24k)	Sn I
$\mathbf{B}_{58} =$	$-y_5 \mathbf{a}_1 + z_5 \mathbf{a}_2$	=	$-ay_5 \hat{\mathbf{x}} + az_5 \hat{\mathbf{y}}$	(24k)	Sn I
$\mathbf{B}_{59} =$	$y_5 \mathbf{a}_1 - z_5 \mathbf{a}_2$	=	$ay_5 \hat{\mathbf{x}} - az_5 \hat{\mathbf{y}}$	(24k)	Sn I
$\mathbf{B}_{60} =$	$-y_5 \mathbf{a}_1 - z_5 \mathbf{a}_2$	=	$-ay_5 \hat{\mathbf{x}} - az_5 \hat{\mathbf{y}}$	(24k)	Sn I
$\mathbf{B}_{61} =$	$(y_5 + \frac{1}{2}) \mathbf{a}_1 + \frac{1}{2} \mathbf{a}_2 - (z_5 - \frac{1}{2}) \mathbf{a}_3$	=	$a(y_5 + \frac{1}{2}) \hat{\mathbf{x}} + \frac{1}{2}a \hat{\mathbf{y}} - a(z_5 - \frac{1}{2}) \hat{\mathbf{z}}$	(24k)	Sn I
$\mathbf{B}_{62} =$	$-(y_5 - \frac{1}{2}) \mathbf{a}_1 + \frac{1}{2} \mathbf{a}_2 - (z_5 - \frac{1}{2}) \mathbf{a}_3$	=	$-a(y_5 - \frac{1}{2}) \hat{\mathbf{x}} + \frac{1}{2}a \hat{\mathbf{y}} - a(z_5 - \frac{1}{2}) \hat{\mathbf{z}}$	(24k)	Sn I
$\mathbf{B}_{63} =$	$(y_5 + \frac{1}{2}) \mathbf{a}_1 + \frac{1}{2} \mathbf{a}_2 + (z_5 + \frac{1}{2}) \mathbf{a}_3$	=	$a(y_5 + \frac{1}{2}) \hat{\mathbf{x}} + \frac{1}{2}a \hat{\mathbf{y}} + a(z_5 + \frac{1}{2}) \hat{\mathbf{z}}$	(24k)	Sn I
$\mathbf{B}_{64} =$	$-(y_5 - \frac{1}{2}) \mathbf{a}_1 + \frac{1}{2} \mathbf{a}_2 + (z_5 + \frac{1}{2}) \mathbf{a}_3$	=	$-a(y_5 - \frac{1}{2}) \hat{\mathbf{x}} + \frac{1}{2}a \hat{\mathbf{y}} + a(z_5 + \frac{1}{2}) \hat{\mathbf{z}}$	(24k)	Sn I
$\mathbf{B}_{65} =$	$\frac{1}{2} \mathbf{a}_1 + (z_5 + \frac{1}{2}) \mathbf{a}_2 - (y_5 - \frac{1}{2}) \mathbf{a}_3$	=	$\frac{1}{2}a \hat{\mathbf{x}} + a(z_5 + \frac{1}{2}) \hat{\mathbf{y}} - a(y_5 - \frac{1}{2}) \hat{\mathbf{z}}$	(24k)	Sn I
$\mathbf{B}_{66} =$	$\frac{1}{2} \mathbf{a}_1 + (z_5 + \frac{1}{2}) \mathbf{a}_2 + (y_5 + \frac{1}{2}) \mathbf{a}_3$	=	$\frac{1}{2}a \hat{\mathbf{x}} + a(z_5 + \frac{1}{2}) \hat{\mathbf{y}} + a(y_5 + \frac{1}{2}) \hat{\mathbf{z}}$	(24k)	Sn I
$\mathbf{B}_{67} =$	$\frac{1}{2} \mathbf{a}_1 - (z_5 - \frac{1}{2}) \mathbf{a}_2 - (y_5 - \frac{1}{2}) \mathbf{a}_3$	=	$\frac{1}{2}a \hat{\mathbf{x}} - a(z_5 - \frac{1}{2}) \hat{\mathbf{y}} - a(y_5 - \frac{1}{2}) \hat{\mathbf{z}}$	(24k)	Sn I
$\mathbf{B}_{68} =$	$\frac{1}{2} \mathbf{a}_1 - (z_5 - \frac{1}{2}) \mathbf{a}_2 + (y_5 + \frac{1}{2}) \mathbf{a}_3$	=	$\frac{1}{2}a \hat{\mathbf{x}} - a(z_5 - \frac{1}{2}) \hat{\mathbf{y}} + a(y_5 + \frac{1}{2}) \hat{\mathbf{z}}$	(24k)	Sn I
$\mathbf{B}_{69} =$	$(z_5 + \frac{1}{2}) \mathbf{a}_1 + (y_5 + \frac{1}{2}) \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	=	$a(z_5 + \frac{1}{2}) \hat{\mathbf{x}} + a(y_5 + \frac{1}{2}) \hat{\mathbf{y}} + \frac{1}{2}a \hat{\mathbf{z}}$	(24k)	Sn I
$\mathbf{B}_{70} =$	$(z_5 + \frac{1}{2}) \mathbf{a}_1 - (y_5 - \frac{1}{2}) \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	=	$a(z_5 + \frac{1}{2}) \hat{\mathbf{x}} - a(y_5 - \frac{1}{2}) \hat{\mathbf{y}} + \frac{1}{2}a \hat{\mathbf{z}}$	(24k)	Sn I
$\mathbf{B}_{71} =$	$-(z_5 - \frac{1}{2}) \mathbf{a}_1 + (y_5 + \frac{1}{2}) \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	=	$-a(z_5 - \frac{1}{2}) \hat{\mathbf{x}} + a(y_5 + \frac{1}{2}) \hat{\mathbf{y}} + \frac{1}{2}a \hat{\mathbf{z}}$	(24k)	Sn I
$\mathbf{B}_{72} =$	$-(z_5 - \frac{1}{2}) \mathbf{a}_1 - (y_5 - \frac{1}{2}) \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	=	$-a(z_5 - \frac{1}{2}) \hat{\mathbf{x}} - a(y_5 - \frac{1}{2}) \hat{\mathbf{y}} + \frac{1}{2}a \hat{\mathbf{z}}$	(24k)	Sn I

References

- [1] M. A. Avila, K. Suekuni, K. Umeo, H. Fukuoka, S. Yamanaka, and T. Takabatake, *Ba₈Ga₁₆Sn₃₀ with type-I clathrate structure: Drastic suppression of heat conduction*, Appl. Phys. Lett. **92**, 041901 (2007), doi:10.1063/1.2831926.
- [2] M. A. Avila, K. Suekuni, K. Umeo, H. Fukuoka, S. Yamanaka, and T. Takabatake, *Glasslike versus crystalline thermal conductivity in carrier-tuned Ba₈Ga₁₆X₃₀ clathrates (X=Ge,Sn)*, Phys. Rev. B **74**, 125109 (2006), doi:10.1103/PhysRevB.74.125109.