

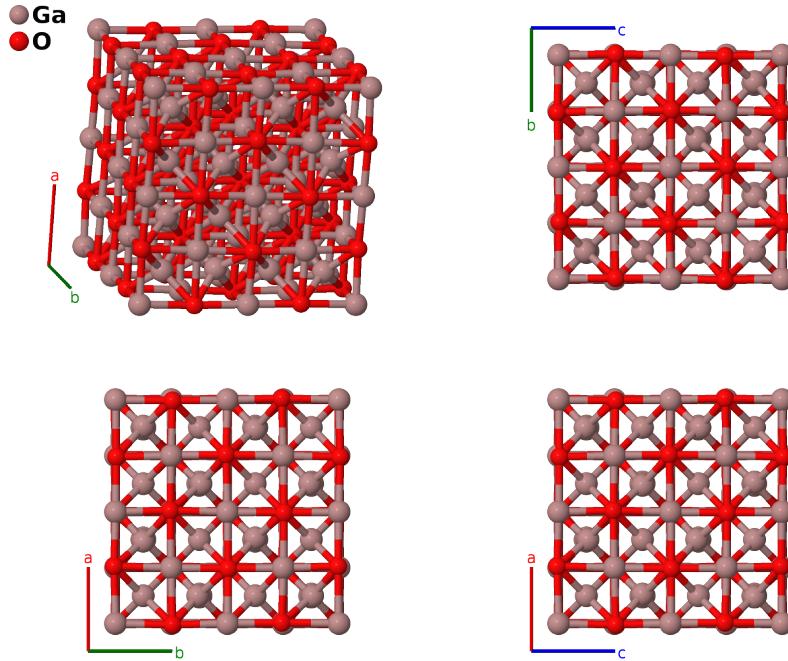
# $\gamma$ -Ga<sub>2</sub>O<sub>3</sub> Structure: A11B4\_cF120\_227\_acdf\_e-001

This structure originally had the label A11B4\_cF120\_227\_acdf\_e. Calls to that address will be redirected here.

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<https://aflow.org/p/VTDR>

[https://aflow.org/p/A11B4\\_cF120\\_227\\_acdf\\_e-001](https://aflow.org/p/A11B4_cF120_227_acdf_e-001)



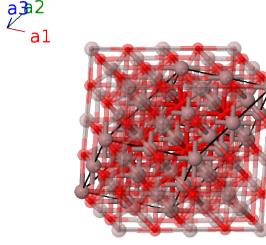
Prototype	Ga <sub>2</sub> O <sub>3</sub>
AFLOW prototype label	A11B4_cF120_227_acdf_e-001
ICSD	236276
Pearson symbol	cF120
Space group number	227
Space group symbol	$Fd\bar{3}m$
AFLOW prototype command	<code>aflow --proto=A11B4_cF120_227_acdf_e-001 --params=a, x<sub>4</sub>, x<sub>5</sub></code>

- Ga<sub>2</sub>O<sub>3</sub> exhibits a variety of structures:
  - $\alpha$ Ga<sub>2</sub>O<sub>3</sub>, which has the corundum ( $D_{5h}$ ) structure ,
  - $\beta$ Ga<sub>2</sub>O<sub>3</sub>,
  - $\gamma$ Ga<sub>2</sub>O<sub>3</sub>, this structure, and
  - $\epsilon$ Ga<sub>2</sub>O<sub>3</sub>, a structure with many vacancies which can be approximated by the  $\kappa$  alumina structure.

- In  $\gamma\text{Ga}_2\text{O}_3$  none of the gallium sites have full occupancy. Ga-I and Ga-II are 74.1% occupied, Ga-III is 6.6% occupied, and Ga-IV is only 2.4% occupied.

### Face-centered Cubic primitive vectors

$$\begin{aligned}\mathbf{a}_1 &= \frac{1}{2}a\hat{\mathbf{y}} + \frac{1}{2}a\hat{\mathbf{z}} \\ \mathbf{a}_2 &= \frac{1}{2}a\hat{\mathbf{x}} + \frac{1}{2}a\hat{\mathbf{z}} \\ \mathbf{a}_3 &= \frac{1}{2}a\hat{\mathbf{x}} + \frac{1}{2}a\hat{\mathbf{y}}\end{aligned}$$



### Basis vectors

	Lattice coordinates	Cartesian coordinates	Wyckoff position	Atom type
$\mathbf{B}_1$ =	$\frac{1}{8}\mathbf{a}_1 + \frac{1}{8}\mathbf{a}_2 + \frac{1}{8}\mathbf{a}_3$	$\frac{1}{8}a\hat{\mathbf{x}} + \frac{1}{8}a\hat{\mathbf{y}} + \frac{1}{8}a\hat{\mathbf{z}}$	(8a)	Ga I
$\mathbf{B}_2$ =	$\frac{7}{8}\mathbf{a}_1 + \frac{7}{8}\mathbf{a}_2 + \frac{7}{8}\mathbf{a}_3$	$\frac{7}{8}a\hat{\mathbf{x}} + \frac{7}{8}a\hat{\mathbf{y}} + \frac{7}{8}a\hat{\mathbf{z}}$	(8a)	Ga I
$\mathbf{B}_3$ =	0	0	(16c)	Ga II
$\mathbf{B}_4$ =	$\frac{1}{2}\mathbf{a}_3$	$\frac{1}{4}a\hat{\mathbf{x}} + \frac{1}{4}a\hat{\mathbf{y}}$	(16c)	Ga II
$\mathbf{B}_5$ =	$\frac{1}{2}\mathbf{a}_2$	$\frac{1}{4}a\hat{\mathbf{x}} + \frac{1}{4}a\hat{\mathbf{z}}$	(16c)	Ga II
$\mathbf{B}_6$ =	$\frac{1}{2}\mathbf{a}_1$	$\frac{1}{4}a\hat{\mathbf{y}} + \frac{1}{4}a\hat{\mathbf{z}}$	(16c)	Ga II
$\mathbf{B}_7$ =	$\frac{1}{2}\mathbf{a}_1 + \frac{1}{2}\mathbf{a}_2 + \frac{1}{2}\mathbf{a}_3$	$\frac{1}{2}a\hat{\mathbf{x}} + \frac{1}{2}a\hat{\mathbf{y}} + \frac{1}{2}a\hat{\mathbf{z}}$	(16d)	Ga III
$\mathbf{B}_8$ =	$\frac{1}{2}\mathbf{a}_1 + \frac{1}{2}\mathbf{a}_2$	$\frac{1}{4}a\hat{\mathbf{x}} + \frac{1}{4}a\hat{\mathbf{y}} + \frac{1}{2}a\hat{\mathbf{z}}$	(16d)	Ga III
$\mathbf{B}_9$ =	$\frac{1}{2}\mathbf{a}_1 + \frac{1}{2}\mathbf{a}_3$	$\frac{1}{4}a\hat{\mathbf{x}} + \frac{1}{2}a\hat{\mathbf{y}} + \frac{1}{4}a\hat{\mathbf{z}}$	(16d)	Ga III
$\mathbf{B}_{10}$ =	$\frac{1}{2}\mathbf{a}_2 + \frac{1}{2}\mathbf{a}_3$	$\frac{1}{2}a\hat{\mathbf{x}} + \frac{1}{4}a\hat{\mathbf{y}} + \frac{1}{4}a\hat{\mathbf{z}}$	(16d)	Ga III
$\mathbf{B}_{11}$ =	$x_4\mathbf{a}_1 + x_4\mathbf{a}_2 + x_4\mathbf{a}_3$	$ax_4\hat{\mathbf{x}} + ax_4\hat{\mathbf{y}} + ax_4\hat{\mathbf{z}}$	(32e)	O I
$\mathbf{B}_{12}$ =	$x_4\mathbf{a}_1 + x_4\mathbf{a}_2 - (3x_4 - \frac{1}{2})\mathbf{a}_3$	$-a(x_4 - \frac{1}{4})\hat{\mathbf{x}} - a(x_4 - \frac{1}{4})\hat{\mathbf{y}} + ax_4\hat{\mathbf{z}}$	(32e)	O I
$\mathbf{B}_{13}$ =	$x_4\mathbf{a}_1 - (3x_4 - \frac{1}{2})\mathbf{a}_2 + x_4\mathbf{a}_3$	$-a(x_4 - \frac{1}{4})\hat{\mathbf{x}} + ax_4\hat{\mathbf{y}} - a(x_4 - \frac{1}{4})\hat{\mathbf{z}}$	(32e)	O I
$\mathbf{B}_{14}$ =	$-(3x_4 - \frac{1}{2})\mathbf{a}_1 + x_4\mathbf{a}_2 + x_4\mathbf{a}_3$	$ax_4\hat{\mathbf{x}} - a(x_4 - \frac{1}{4})\hat{\mathbf{y}} - a(x_4 - \frac{1}{4})\hat{\mathbf{z}}$	(32e)	O I
$\mathbf{B}_{15}$ =	$-x_4\mathbf{a}_1 - x_4\mathbf{a}_2 + (3x_4 + \frac{1}{2})\mathbf{a}_3$	$a(x_4 + \frac{1}{4})\hat{\mathbf{x}} + a(x_4 + \frac{1}{4})\hat{\mathbf{y}} - ax_4\hat{\mathbf{z}}$	(32e)	O I
$\mathbf{B}_{16}$ =	$-x_4\mathbf{a}_1 - x_4\mathbf{a}_2 - x_4\mathbf{a}_3$	$-ax_4\hat{\mathbf{x}} - ax_4\hat{\mathbf{y}} - ax_4\hat{\mathbf{z}}$	(32e)	O I
$\mathbf{B}_{17}$ =	$-x_4\mathbf{a}_1 + (3x_4 + \frac{1}{2})\mathbf{a}_2 - x_4\mathbf{a}_3$	$a(x_4 + \frac{1}{4})\hat{\mathbf{x}} - ax_4\hat{\mathbf{y}} + a(x_4 + \frac{1}{4})\hat{\mathbf{z}}$	(32e)	O I
$\mathbf{B}_{18}$ =	$(3x_4 + \frac{1}{2})\mathbf{a}_1 - x_4\mathbf{a}_2 - x_4\mathbf{a}_3$	$-ax_4\hat{\mathbf{x}} + a(x_4 + \frac{1}{4})\hat{\mathbf{y}} + a(x_4 + \frac{1}{4})\hat{\mathbf{z}}$	(32e)	O I
$\mathbf{B}_{19}$ =	$-(x_5 - \frac{1}{4})\mathbf{a}_1 + x_5\mathbf{a}_2 + x_5\mathbf{a}_3$	$ax_5\hat{\mathbf{x}} + \frac{1}{8}a\hat{\mathbf{y}} + \frac{1}{8}a\hat{\mathbf{z}}$	(48f)	Ga IV
$\mathbf{B}_{20}$ =	$x_5\mathbf{a}_1 - (x_5 - \frac{1}{4})\mathbf{a}_2 - (x_5 - \frac{1}{4})\mathbf{a}_3$	$-a(x_5 - \frac{1}{4})\hat{\mathbf{x}} + \frac{1}{8}a\hat{\mathbf{y}} + \frac{1}{8}a\hat{\mathbf{z}}$	(48f)	Ga IV
$\mathbf{B}_{21}$ =	$x_5\mathbf{a}_1 - (x_5 - \frac{1}{4})\mathbf{a}_2 + x_5\mathbf{a}_3$	$\frac{1}{8}a\hat{\mathbf{x}} + ax_5\hat{\mathbf{y}} + \frac{1}{8}a\hat{\mathbf{z}}$	(48f)	Ga IV
$\mathbf{B}_{22}$ =	$-(x_5 - \frac{1}{4})\mathbf{a}_1 + x_5\mathbf{a}_2 - (x_5 - \frac{1}{4})\mathbf{a}_3$	$\frac{1}{8}a\hat{\mathbf{x}} - a(x_5 - \frac{1}{4})\hat{\mathbf{y}} + \frac{1}{8}a\hat{\mathbf{z}}$	(48f)	Ga IV
$\mathbf{B}_{23}$ =	$x_5\mathbf{a}_1 + x_5\mathbf{a}_2 - (x_5 - \frac{1}{4})\mathbf{a}_3$	$\frac{1}{8}a\hat{\mathbf{x}} + \frac{1}{8}a\hat{\mathbf{y}} + ax_5\hat{\mathbf{z}}$	(48f)	Ga IV
$\mathbf{B}_{24}$ =	$-(x_5 - \frac{1}{4})\mathbf{a}_1 - (x_5 - \frac{1}{4})\mathbf{a}_2 + x_5\mathbf{a}_3$	$\frac{1}{8}a\hat{\mathbf{x}} + \frac{1}{8}a\hat{\mathbf{y}} - a(x_5 - \frac{1}{4})\hat{\mathbf{z}}$	(48f)	Ga IV
$\mathbf{B}_{25}$ =	$(x_5 + \frac{3}{4})\mathbf{a}_1 - x_5\mathbf{a}_2 + (x_5 + \frac{3}{4})\mathbf{a}_3$	$\frac{3}{8}a\hat{\mathbf{x}} + a(x_5 + \frac{3}{4})\hat{\mathbf{y}} + \frac{3}{8}a\hat{\mathbf{z}}$	(48f)	Ga IV

$$\begin{aligned}
\mathbf{B}_{26} &= -x_5 \mathbf{a}_1 + \left(x_5 + \frac{3}{4}\right) \mathbf{a}_2 - x_5 \mathbf{a}_3 & = & \frac{3}{8}a\hat{\mathbf{x}} - ax_5\hat{\mathbf{y}} + \frac{3}{8}a\hat{\mathbf{z}} & (48f) & \text{Ga IV} \\
\mathbf{B}_{27} &= -x_5 \mathbf{a}_1 + \left(x_5 + \frac{3}{4}\right) \mathbf{a}_2 + \left(x_5 + \frac{3}{4}\right) \mathbf{a}_3 & = & a\left(x_5 + \frac{3}{4}\right)\hat{\mathbf{x}} + \frac{3}{8}a\hat{\mathbf{y}} + \frac{3}{8}a\hat{\mathbf{z}} & (48f) & \text{Ga IV} \\
\mathbf{B}_{28} &= \left(x_5 + \frac{3}{4}\right) \mathbf{a}_1 - x_5 \mathbf{a}_2 - x_5 \mathbf{a}_3 & = & -ax_5\hat{\mathbf{x}} + \frac{3}{8}a\hat{\mathbf{y}} + \frac{3}{8}a\hat{\mathbf{z}} & (48f) & \text{Ga IV} \\
\mathbf{B}_{29} &= -x_5 \mathbf{a}_1 - x_5 \mathbf{a}_2 + \left(x_5 + \frac{3}{4}\right) \mathbf{a}_3 & = & \frac{3}{8}a\hat{\mathbf{x}} + \frac{3}{8}a\hat{\mathbf{y}} - ax_5\hat{\mathbf{z}} & (48f) & \text{Ga IV} \\
\mathbf{B}_{30} &= \left(x_5 + \frac{3}{4}\right) \mathbf{a}_1 + \left(x_5 + \frac{3}{4}\right) \mathbf{a}_2 - x_5 \mathbf{a}_3 & = & \frac{3}{8}a\hat{\mathbf{x}} + \frac{3}{8}a\hat{\mathbf{y}} + a\left(x_5 + \frac{3}{4}\right)\hat{\mathbf{z}} & (48f) & \text{Ga IV}
\end{aligned}$$

## References

- [1] H. Y. Playford, A. C. Hannon, E. R. Barney, and R. I. Walton, *Structures of Uncharacterised Polymorphs of Gallium Oxide from Total Neutron Diffraction*, Chem. Euro. J. **19**, 2803–2813 (2013), doi:10.1002/chem.201203359.