

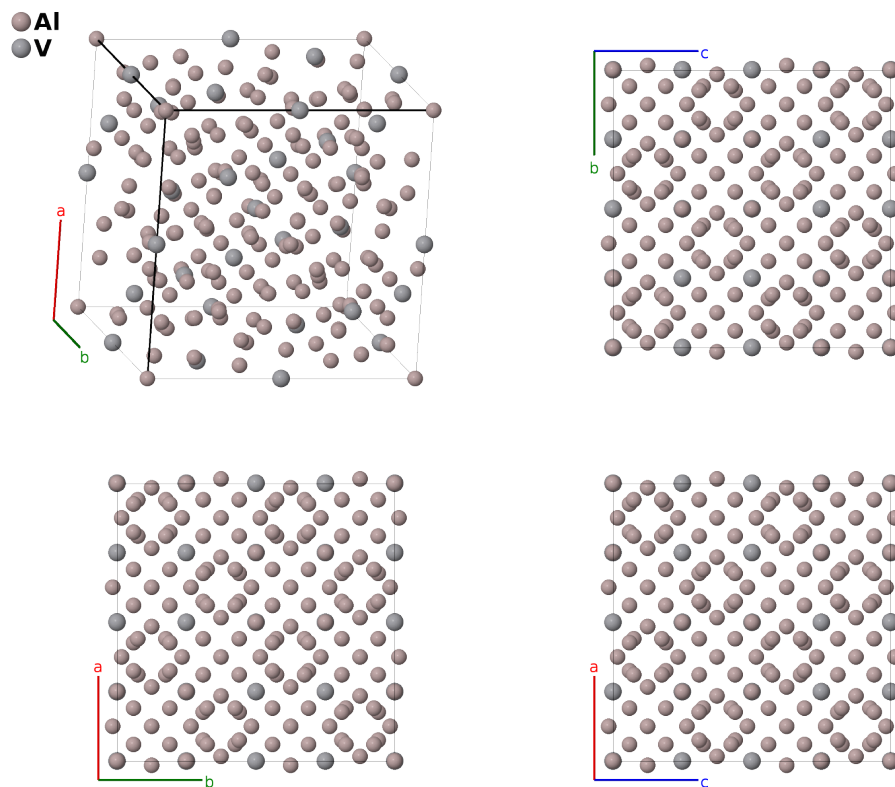
Al₁₀V Structure:

A10B_cF176_227_cfg_d-001

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<https://afLOW.org/p/WWX6>

https://afLOW.org/p/A10B_cF176_227_cfg_d-001

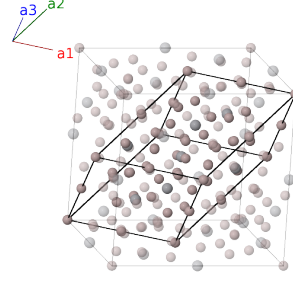


Prototype	Al ₁₀ V
AFLOW prototype label	A10B_cF176_227_cfg_d-001
ICSD	58202
Pearson symbol	cF176
Space group number	227
Space group symbol	$Fd\bar{3}m$
AFLOW prototype command	<code>afLOW --proto=A10B_cF176_227_cfg_d-001 --params=a, x₃, x₄, z₄</code>

- (Brown, 1957) gives the structural information in setting 1 of space group $Fd\bar{3}m$ #227. We shifted the origin by $(a/8, a/8, a/8)$ to change this to the standard setting 2.

Face-centered Cubic primitive vectors

$$\begin{aligned}\mathbf{a}_1 &= \frac{1}{2}a\hat{y} + \frac{1}{2}a\hat{z} \\ \mathbf{a}_2 &= \frac{1}{2}a\hat{x} + \frac{1}{2}a\hat{z} \\ \mathbf{a}_3 &= \frac{1}{2}a\hat{x} + \frac{1}{2}a\hat{y}\end{aligned}$$



Basis vectors

	Lattice coordinates		Cartesian coordinates	Wyckoff position	Atom type
\mathbf{B}_1	0	$=$	0	(16c)	Al I
\mathbf{B}_2	$\frac{1}{2}\mathbf{a}_3$	$=$	$\frac{1}{4}a\hat{x} + \frac{1}{4}a\hat{y}$	(16c)	Al I
\mathbf{B}_3	$\frac{1}{2}\mathbf{a}_2$	$=$	$\frac{1}{4}a\hat{x} + \frac{1}{4}a\hat{z}$	(16c)	Al I
\mathbf{B}_4	$\frac{1}{2}\mathbf{a}_1$	$=$	$\frac{1}{4}a\hat{y} + \frac{1}{4}a\hat{z}$	(16c)	Al I
\mathbf{B}_5	$\frac{1}{2}\mathbf{a}_1 + \frac{1}{2}\mathbf{a}_2 + \frac{1}{2}\mathbf{a}_3$	$=$	$\frac{1}{2}a\hat{x} + \frac{1}{2}a\hat{y} + \frac{1}{2}a\hat{z}$	(16d)	V I
\mathbf{B}_6	$\frac{1}{2}\mathbf{a}_1 + \frac{1}{2}\mathbf{a}_2$	$=$	$\frac{1}{4}a\hat{x} + \frac{1}{4}a\hat{y} + \frac{1}{2}a\hat{z}$	(16d)	V I
\mathbf{B}_7	$\frac{1}{2}\mathbf{a}_1 + \frac{1}{2}\mathbf{a}_3$	$=$	$\frac{1}{4}a\hat{x} + \frac{1}{2}a\hat{y} + \frac{1}{4}a\hat{z}$	(16d)	V I
\mathbf{B}_8	$\frac{1}{2}\mathbf{a}_2 + \frac{1}{2}\mathbf{a}_3$	$=$	$\frac{1}{2}a\hat{x} + \frac{1}{4}a\hat{y} + \frac{1}{4}a\hat{z}$	(16d)	V I
\mathbf{B}_9	$-(x_3 - \frac{1}{4})\mathbf{a}_1 + x_3\mathbf{a}_2 + x_3\mathbf{a}_3$	$=$	$ax_3\hat{x} + \frac{1}{8}a\hat{y} + \frac{1}{8}a\hat{z}$	(48f)	Al II
\mathbf{B}_{10}	$x_3\mathbf{a}_1 - (x_3 - \frac{1}{4})\mathbf{a}_2 - (x_3 - \frac{1}{4})\mathbf{a}_3$	$=$	$-a(x_3 - \frac{1}{4})\hat{x} + \frac{1}{8}a\hat{y} + \frac{1}{8}a\hat{z}$	(48f)	Al II
\mathbf{B}_{11}	$x_3\mathbf{a}_1 - (x_3 - \frac{1}{4})\mathbf{a}_2 + x_3\mathbf{a}_3$	$=$	$\frac{1}{8}a\hat{x} + ax_3\hat{y} + \frac{1}{8}a\hat{z}$	(48f)	Al II
\mathbf{B}_{12}	$-(x_3 - \frac{1}{4})\mathbf{a}_1 + x_3\mathbf{a}_2 - (x_3 - \frac{1}{4})\mathbf{a}_3$	$=$	$\frac{1}{8}a\hat{x} - a(x_3 - \frac{1}{4})\hat{y} + \frac{1}{8}a\hat{z}$	(48f)	Al II
\mathbf{B}_{13}	$x_3\mathbf{a}_1 + x_3\mathbf{a}_2 - (x_3 - \frac{1}{4})\mathbf{a}_3$	$=$	$\frac{1}{8}a\hat{x} + \frac{1}{8}a\hat{y} + ax_3\hat{z}$	(48f)	Al II
\mathbf{B}_{14}	$-(x_3 - \frac{1}{4})\mathbf{a}_1 - (x_3 - \frac{1}{4})\mathbf{a}_2 + x_3\mathbf{a}_3$	$=$	$\frac{1}{8}a\hat{x} + \frac{1}{8}a\hat{y} - a(x_3 - \frac{1}{4})\hat{z}$	(48f)	Al II
\mathbf{B}_{15}	$(x_3 + \frac{3}{4})\mathbf{a}_1 - x_3\mathbf{a}_2 + (x_3 + \frac{3}{4})\mathbf{a}_3$	$=$	$\frac{3}{8}a\hat{x} + a(x_3 + \frac{3}{4})\hat{y} + \frac{3}{8}a\hat{z}$	(48f)	Al II
\mathbf{B}_{16}	$-x_3\mathbf{a}_1 + (x_3 + \frac{3}{4})\mathbf{a}_2 - x_3\mathbf{a}_3$	$=$	$\frac{3}{8}a\hat{x} - ax_3\hat{y} + \frac{3}{8}a\hat{z}$	(48f)	Al II
\mathbf{B}_{17}	$-x_3\mathbf{a}_1 + (x_3 + \frac{3}{4})\mathbf{a}_2 + (x_3 + \frac{3}{4})\mathbf{a}_3$	$=$	$a(x_3 + \frac{3}{4})\hat{x} + \frac{3}{8}a\hat{y} + \frac{3}{8}a\hat{z}$	(48f)	Al II
\mathbf{B}_{18}	$(x_3 + \frac{3}{4})\mathbf{a}_1 - x_3\mathbf{a}_2 - x_3\mathbf{a}_3$	$=$	$-ax_3\hat{x} + \frac{3}{8}a\hat{y} + \frac{3}{8}a\hat{z}$	(48f)	Al II
\mathbf{B}_{19}	$-x_3\mathbf{a}_1 - x_3\mathbf{a}_2 + (x_3 + \frac{3}{4})\mathbf{a}_3$	$=$	$\frac{3}{8}a\hat{x} + \frac{3}{8}a\hat{y} - ax_3\hat{z}$	(48f)	Al II
\mathbf{B}_{20}	$(x_3 + \frac{3}{4})\mathbf{a}_1 + (x_3 + \frac{3}{4})\mathbf{a}_2 - x_3\mathbf{a}_3$	$=$	$\frac{3}{8}a\hat{x} + \frac{3}{8}a\hat{y} + a(x_3 + \frac{3}{4})\hat{z}$	(48f)	Al II
\mathbf{B}_{21}	$z_4\mathbf{a}_1 + z_4\mathbf{a}_2 + (2x_4 - z_4)\mathbf{a}_3$	$=$	$ax_4\hat{x} + ax_4\hat{y} + az_4\hat{z}$	(96g)	Al III
\mathbf{B}_{22}	$z_4\mathbf{a}_1 + z_4\mathbf{a}_2 - (2x_4 + z_4 - \frac{1}{2})\mathbf{a}_3$	$=$	$-a(x_4 - \frac{1}{4})\hat{x} - a(x_4 - \frac{1}{4})\hat{y} + az_4\hat{z}$	(96g)	Al III
\mathbf{B}_{23}	$(2x_4 - z_4)\mathbf{a}_1 - (2x_4 + z_4 - \frac{1}{2})\mathbf{a}_2 + z_4\mathbf{a}_3$	$=$	$-a(x_4 - \frac{1}{4})\hat{x} + ax_4\hat{y} - a(z_4 - \frac{1}{4})\hat{z}$	(96g)	Al III
\mathbf{B}_{24}	$-(2x_4 + z_4 - \frac{1}{2})\mathbf{a}_1 + (2x_4 - z_4)\mathbf{a}_2 + z_4\mathbf{a}_3$	$=$	$ax_4\hat{x} - a(x_4 - \frac{1}{4})\hat{y} - a(z_4 - \frac{1}{4})\hat{z}$	(96g)	Al III

$$\begin{aligned}
\mathbf{B}_{25} &= (2x_4 - z_4) \mathbf{a}_1 + z_4 \mathbf{a}_2 + z_4 \mathbf{a}_3 &= & az_4 \hat{\mathbf{x}} + ax_4 \hat{\mathbf{y}} + ax_4 \hat{\mathbf{z}} &(96g) & \text{Al III} \\
\mathbf{B}_{26} &= -(2x_4 + z_4 - \frac{1}{2}) \mathbf{a}_1 + z_4 \mathbf{a}_2 + z_4 \mathbf{a}_3 &= & az_4 \hat{\mathbf{x}} - a(x_4 - \frac{1}{4}) \hat{\mathbf{y}} - a(x_4 - \frac{1}{4}) \hat{\mathbf{z}} &(96g) & \text{Al III} \\
\mathbf{B}_{27} &= z_4 \mathbf{a}_1 + (2x_4 - z_4) \mathbf{a}_2 - (2x_4 + z_4 - \frac{1}{2}) \mathbf{a}_3 &= & -a(z_4 - \frac{1}{4}) \hat{\mathbf{x}} - a(x_4 - \frac{1}{4}) \hat{\mathbf{y}} + ax_4 \hat{\mathbf{z}} &(96g) & \text{Al III} \\
\mathbf{B}_{28} &= z_4 \mathbf{a}_1 - (2x_4 + z_4 - \frac{1}{2}) \mathbf{a}_2 + (2x_4 - z_4) \mathbf{a}_3 &= & -a(z_4 - \frac{1}{4}) \hat{\mathbf{x}} + ax_4 \hat{\mathbf{y}} - a(x_4 - \frac{1}{4}) \hat{\mathbf{z}} &(96g) & \text{Al III} \\
\mathbf{B}_{29} &= z_4 \mathbf{a}_1 + (2x_4 - z_4) \mathbf{a}_2 + z_4 \mathbf{a}_3 &= & ax_4 \hat{\mathbf{x}} + az_4 \hat{\mathbf{y}} + ax_4 \hat{\mathbf{z}} &(96g) & \text{Al III} \\
\mathbf{B}_{30} &= z_4 \mathbf{a}_1 - (2x_4 + z_4 - \frac{1}{2}) \mathbf{a}_2 + z_4 \mathbf{a}_3 &= & -a(x_4 - \frac{1}{4}) \hat{\mathbf{x}} + az_4 \hat{\mathbf{y}} - a(x_4 - \frac{1}{4}) \hat{\mathbf{z}} &(96g) & \text{Al III} \\
\mathbf{B}_{31} &= -(2x_4 + z_4 - \frac{1}{2}) \mathbf{a}_1 + z_4 \mathbf{a}_2 + (2x_4 - z_4) \mathbf{a}_3 &= & ax_4 \hat{\mathbf{x}} - a(z_4 - \frac{1}{4}) \hat{\mathbf{y}} - a(x_4 - \frac{1}{4}) \hat{\mathbf{z}} &(96g) & \text{Al III} \\
\mathbf{B}_{32} &= (2x_4 - z_4) \mathbf{a}_1 + z_4 \mathbf{a}_2 - (2x_4 + z_4 - \frac{1}{2}) \mathbf{a}_3 &= & -a(x_4 - \frac{1}{4}) \hat{\mathbf{x}} - a(z_4 - \frac{1}{4}) \hat{\mathbf{y}} + ax_4 \hat{\mathbf{z}} &(96g) & \text{Al III} \\
\mathbf{B}_{33} &= -z_4 \mathbf{a}_1 - z_4 \mathbf{a}_2 + (2x_4 + z_4 + \frac{1}{2}) \mathbf{a}_3 &= & a(x_4 + \frac{1}{4}) \hat{\mathbf{x}} + a(x_4 + \frac{1}{4}) \hat{\mathbf{y}} - az_4 \hat{\mathbf{z}} &(96g) & \text{Al III} \\
\mathbf{B}_{34} &= -z_4 \mathbf{a}_1 - z_4 \mathbf{a}_2 - (2x_4 - z_4) \mathbf{a}_3 &= & -ax_4 \hat{\mathbf{x}} - ax_4 \hat{\mathbf{y}} - az_4 \hat{\mathbf{z}} &(96g) & \text{Al III} \\
\mathbf{B}_{35} &= -(2x_4 - z_4) \mathbf{a}_1 + (2x_4 + z_4 + \frac{1}{2}) \mathbf{a}_2 - z_4 \mathbf{a}_3 &= & a(x_4 + \frac{1}{4}) \hat{\mathbf{x}} - ax_4 \hat{\mathbf{y}} + a(z_4 + \frac{1}{4}) \hat{\mathbf{z}} &(96g) & \text{Al III} \\
\mathbf{B}_{36} &= (2x_4 + z_4 + \frac{1}{2}) \mathbf{a}_1 - (2x_4 - z_4) \mathbf{a}_2 - z_4 \mathbf{a}_3 &= & -ax_4 \hat{\mathbf{x}} + a(x_4 + \frac{1}{4}) \hat{\mathbf{y}} + a(z_4 + \frac{1}{4}) \hat{\mathbf{z}} &(96g) & \text{Al III} \\
\mathbf{B}_{37} &= -(2x_4 - z_4) \mathbf{a}_1 - z_4 \mathbf{a}_2 + (2x_4 + z_4 + \frac{1}{2}) \mathbf{a}_3 &= & a(x_4 + \frac{1}{4}) \hat{\mathbf{x}} + a(z_4 + \frac{1}{4}) \hat{\mathbf{y}} - ax_4 \hat{\mathbf{z}} &(96g) & \text{Al III} \\
\mathbf{B}_{38} &= (2x_4 + z_4 + \frac{1}{2}) \mathbf{a}_1 - z_4 \mathbf{a}_2 - (2x_4 - z_4) \mathbf{a}_3 &= & -ax_4 \hat{\mathbf{x}} + a(z_4 + \frac{1}{4}) \hat{\mathbf{y}} + a(x_4 + \frac{1}{4}) \hat{\mathbf{z}} &(96g) & \text{Al III} \\
\mathbf{B}_{39} &= -z_4 \mathbf{a}_1 - (2x_4 - z_4) \mathbf{a}_2 - z_4 \mathbf{a}_3 &= & -ax_4 \hat{\mathbf{x}} - az_4 \hat{\mathbf{y}} - ax_4 \hat{\mathbf{z}} &(96g) & \text{Al III} \\
\mathbf{B}_{40} &= -z_4 \mathbf{a}_1 + (2x_4 + z_4 + \frac{1}{2}) \mathbf{a}_2 - z_4 \mathbf{a}_3 &= & a(x_4 + \frac{1}{4}) \hat{\mathbf{x}} - az_4 \hat{\mathbf{y}} + a(x_4 + \frac{1}{4}) \hat{\mathbf{z}} &(96g) & \text{Al III} \\
\mathbf{B}_{41} &= -z_4 \mathbf{a}_1 - (2x_4 - z_4) \mathbf{a}_2 + (2x_4 + z_4 + \frac{1}{2}) \mathbf{a}_3 &= & a(z_4 + \frac{1}{4}) \hat{\mathbf{x}} + a(x_4 + \frac{1}{4}) \hat{\mathbf{y}} - ax_4 \hat{\mathbf{z}} &(96g) & \text{Al III} \\
\mathbf{B}_{42} &= -z_4 \mathbf{a}_1 + (2x_4 + z_4 + \frac{1}{2}) \mathbf{a}_2 - (2x_4 - z_4) \mathbf{a}_3 &= & a(z_4 + \frac{1}{4}) \hat{\mathbf{x}} - ax_4 \hat{\mathbf{y}} + a(x_4 + \frac{1}{4}) \hat{\mathbf{z}} &(96g) & \text{Al III} \\
\mathbf{B}_{43} &= (2x_4 + z_4 + \frac{1}{2}) \mathbf{a}_1 - z_4 \mathbf{a}_2 - z_4 \mathbf{a}_3 &= & -az_4 \hat{\mathbf{x}} + a(x_4 + \frac{1}{4}) \hat{\mathbf{y}} + a(x_4 + \frac{1}{4}) \hat{\mathbf{z}} &(96g) & \text{Al III} \\
\mathbf{B}_{44} &= -(2x_4 - z_4) \mathbf{a}_1 - z_4 \mathbf{a}_2 - z_4 \mathbf{a}_3 &= & -az_4 \hat{\mathbf{x}} - ax_4 \hat{\mathbf{y}} - ax_4 \hat{\mathbf{z}} &(96g) & \text{Al III}
\end{aligned}$$

References

- [1] P. J. Brown, *The Structure of $\alpha(V\text{-Al})$* , Acta Cryst. **10**, 133–135 (1957), doi:10.1107/S0365110X57000389.

Found in

- [1] F. Wang, Y.-L. Chiu, D. Eskin, W. Du, and P. R. Shearing, *A grain refinement mechanism of cast commercial purity aluminium by vanadium*, Mater. Charact **181**, 111468 (2021), doi:10.1016/j.matchar.2021.111468.