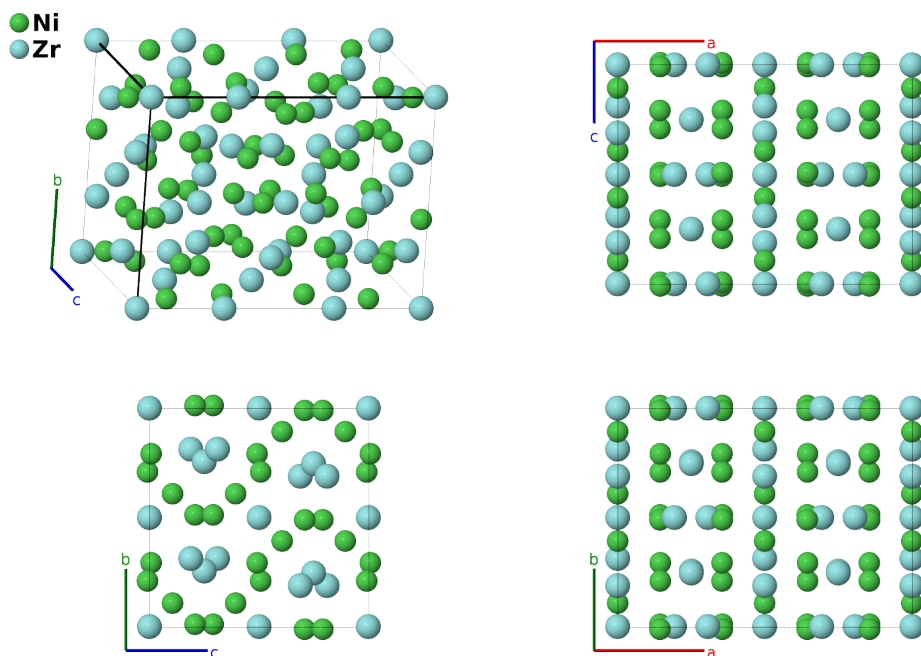


# Zr<sub>7</sub>Ni<sub>10</sub> Structure: A10B7\_oC68\_64\_f2g\_adeF-001

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<https://afLOW.org/p/7BKZ>

[https://afLOW.org/p/A10B7\\_oC68\\_64\\_f2g\\_adeF-001](https://afLOW.org/p/A10B7_oC68_64_f2g_adeF-001)



Prototype	Ni <sub>10</sub> Zr <sub>7</sub>
AFLOW prototype label	A10B7_oC68_64_f2g_adeF-001
ICSD	240191
Pearson symbol	oC68
Space group number	64
Space group symbol	<i>Cmce</i>
AFLOW prototype command	<code>afLOW --proto=A10B7_oC68_64_f2g_adeF-001 --params=a, b/a, c/a, x<sub>2</sub>, y<sub>3</sub>, y<sub>4</sub>, z<sub>4</sub>, y<sub>5</sub>, z<sub>5</sub>, x<sub>6</sub>, y<sub>6</sub>, z<sub>6</sub>, x<sub>7</sub>, y<sub>7</sub>, z<sub>7</sub></code>

## Other compounds with this structure

Hf<sub>7</sub>Ni<sub>10</sub>

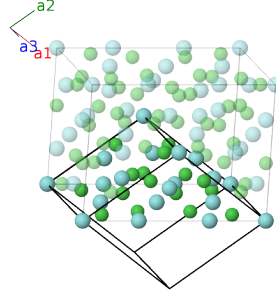
- (Kirkpatrick, 1962) originally placed this structure in space group *Aba2* #41, and early structure compilations such as (Pearson, 1967) quote this structure. (Joubert, 1977) showed that the structure has an inversion site and placed the system in space group *Cmca* #64.

## Base-centered Orthorhombic primitive vectors

$$\mathbf{a}_1 = \frac{1}{2}a \hat{\mathbf{x}} - \frac{1}{2}b \hat{\mathbf{y}}$$

$$\mathbf{a}_2 = \frac{1}{2}a \hat{\mathbf{x}} + \frac{1}{2}b \hat{\mathbf{y}}$$

$$\mathbf{a}_3 = c \hat{\mathbf{z}}$$



## Basis vectors

	Lattice coordinates		Cartesian coordinates	Wyckoff position	Atom type
$\mathbf{B}_1$	$=$	$0$	$=$	$0$	(4a) Zr I
$\mathbf{B}_2$	$=$	$\frac{1}{2} \mathbf{a}_1 + \frac{1}{2} \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	$=$	$\frac{1}{2}a \hat{\mathbf{x}} + \frac{1}{2}c \hat{\mathbf{z}}$	(4a) Zr I
$\mathbf{B}_3$	$=$	$x_2 \mathbf{a}_1 + x_2 \mathbf{a}_2$	$=$	$ax_2 \hat{\mathbf{x}}$	(8d) Zr II
$\mathbf{B}_4$	$=$	$-(x_2 - \frac{1}{2}) \mathbf{a}_1 - (x_2 - \frac{1}{2}) \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	$=$	$-a(x_2 - \frac{1}{2}) \hat{\mathbf{x}} + \frac{1}{2}c \hat{\mathbf{z}}$	(8d) Zr II
$\mathbf{B}_5$	$=$	$-x_2 \mathbf{a}_1 - x_2 \mathbf{a}_2$	$=$	$-ax_2 \hat{\mathbf{x}}$	(8d) Zr II
$\mathbf{B}_6$	$=$	$(x_2 + \frac{1}{2}) \mathbf{a}_1 + (x_2 + \frac{1}{2}) \mathbf{a}_2 + \frac{1}{2} \mathbf{a}_3$	$=$	$a(x_2 + \frac{1}{2}) \hat{\mathbf{x}} + \frac{1}{2}c \hat{\mathbf{z}}$	(8d) Zr II
$\mathbf{B}_7$	$=$	$-(y_3 - \frac{1}{4}) \mathbf{a}_1 + (y_3 + \frac{1}{4}) \mathbf{a}_2 + \frac{1}{4} \mathbf{a}_3$	$=$	$\frac{1}{4}a \hat{\mathbf{x}} + by_3 \hat{\mathbf{y}} + \frac{1}{4}c \hat{\mathbf{z}}$	(8e) Zr III
$\mathbf{B}_8$	$=$	$(y_3 + \frac{1}{4}) \mathbf{a}_1 - (y_3 - \frac{1}{4}) \mathbf{a}_2 + \frac{3}{4} \mathbf{a}_3$	$=$	$\frac{1}{4}a \hat{\mathbf{x}} - by_3 \hat{\mathbf{y}} + \frac{3}{4}c \hat{\mathbf{z}}$	(8e) Zr III
$\mathbf{B}_9$	$=$	$(y_3 + \frac{3}{4}) \mathbf{a}_1 - (y_3 - \frac{3}{4}) \mathbf{a}_2 + \frac{3}{4} \mathbf{a}_3$	$=$	$\frac{3}{4}a \hat{\mathbf{x}} - by_3 \hat{\mathbf{y}} + \frac{3}{4}c \hat{\mathbf{z}}$	(8e) Zr III
$\mathbf{B}_{10}$	$=$	$-(y_3 - \frac{3}{4}) \mathbf{a}_1 + (y_3 + \frac{3}{4}) \mathbf{a}_2 + \frac{1}{4} \mathbf{a}_3$	$=$	$\frac{3}{4}a \hat{\mathbf{x}} + by_3 \hat{\mathbf{y}} + \frac{1}{4}c \hat{\mathbf{z}}$	(8e) Zr III
$\mathbf{B}_{11}$	$=$	$-y_4 \mathbf{a}_1 + y_4 \mathbf{a}_2 + z_4 \mathbf{a}_3$	$=$	$by_4 \hat{\mathbf{y}} + cz_4 \hat{\mathbf{z}}$	(8f) Ni I
$\mathbf{B}_{12}$	$=$	$(y_4 + \frac{1}{2}) \mathbf{a}_1 - (y_4 - \frac{1}{2}) \mathbf{a}_2 + (z_4 + \frac{1}{2}) \mathbf{a}_3$	$=$	$\frac{1}{2}a \hat{\mathbf{x}} - by_4 \hat{\mathbf{y}} + c(z_4 + \frac{1}{2}) \hat{\mathbf{z}}$	(8f) Ni I
$\mathbf{B}_{13}$	$=$	$-(y_4 - \frac{1}{2}) \mathbf{a}_1 + (y_4 + \frac{1}{2}) \mathbf{a}_2 - (z_4 - \frac{1}{2}) \mathbf{a}_3$	$=$	$\frac{1}{2}a \hat{\mathbf{x}} + by_4 \hat{\mathbf{y}} - c(z_4 - \frac{1}{2}) \hat{\mathbf{z}}$	(8f) Ni I
$\mathbf{B}_{14}$	$=$	$y_4 \mathbf{a}_1 - y_4 \mathbf{a}_2 - z_4 \mathbf{a}_3$	$=$	$-by_4 \hat{\mathbf{y}} - cz_4 \hat{\mathbf{z}}$	(8f) Ni I
$\mathbf{B}_{15}$	$=$	$-y_5 \mathbf{a}_1 + y_5 \mathbf{a}_2 + z_5 \mathbf{a}_3$	$=$	$by_5 \hat{\mathbf{y}} + cz_5 \hat{\mathbf{z}}$	(8f) Zr IV
$\mathbf{B}_{16}$	$=$	$(y_5 + \frac{1}{2}) \mathbf{a}_1 - (y_5 - \frac{1}{2}) \mathbf{a}_2 + (z_5 + \frac{1}{2}) \mathbf{a}_3$	$=$	$\frac{1}{2}a \hat{\mathbf{x}} - by_5 \hat{\mathbf{y}} + c(z_5 + \frac{1}{2}) \hat{\mathbf{z}}$	(8f) Zr IV
$\mathbf{B}_{17}$	$=$	$-(y_5 - \frac{1}{2}) \mathbf{a}_1 + (y_5 + \frac{1}{2}) \mathbf{a}_2 - (z_5 - \frac{1}{2}) \mathbf{a}_3$	$=$	$\frac{1}{2}a \hat{\mathbf{x}} + by_5 \hat{\mathbf{y}} - c(z_5 - \frac{1}{2}) \hat{\mathbf{z}}$	(8f) Zr IV
$\mathbf{B}_{18}$	$=$	$y_5 \mathbf{a}_1 - y_5 \mathbf{a}_2 - z_5 \mathbf{a}_3$	$=$	$-by_5 \hat{\mathbf{y}} - cz_5 \hat{\mathbf{z}}$	(8f) Zr IV
$\mathbf{B}_{19}$	$=$	$(x_6 - y_6) \mathbf{a}_1 + (x_6 + y_6) \mathbf{a}_2 + z_6 \mathbf{a}_3$	$=$	$ax_6 \hat{\mathbf{x}} + by_6 \hat{\mathbf{y}} + cz_6 \hat{\mathbf{z}}$	(16g) Ni II
$\mathbf{B}_{20}$	$=$	$(-x_6 + y_6 + \frac{1}{2}) \mathbf{a}_1 - (x_6 + y_6 - \frac{1}{2}) \mathbf{a}_2 + (z_6 + \frac{1}{2}) \mathbf{a}_3$	$=$	$-a(x_6 - \frac{1}{2}) \hat{\mathbf{x}} - by_6 \hat{\mathbf{y}} + c(z_6 + \frac{1}{2}) \hat{\mathbf{z}}$	(16g) Ni II
$\mathbf{B}_{21}$	$=$	$-(x_6 + y_6 - \frac{1}{2}) \mathbf{a}_1 + (-x_6 + y_6 + \frac{1}{2}) \mathbf{a}_2 - (z_6 - \frac{1}{2}) \mathbf{a}_3$	$=$	$-a(x_6 - \frac{1}{2}) \hat{\mathbf{x}} + by_6 \hat{\mathbf{y}} - c(z_6 - \frac{1}{2}) \hat{\mathbf{z}}$	(16g) Ni II

$$\begin{aligned}
\mathbf{B}_{22} &= \frac{(x_6 + y_6) \mathbf{a}_1 + (x_6 - y_6) \mathbf{a}_2 - z_6 \mathbf{a}_3}{z_6} = ax_6 \hat{\mathbf{x}} - by_6 \hat{\mathbf{y}} - cz_6 \hat{\mathbf{z}} & (16g) & \text{Ni II} \\
\mathbf{B}_{23} &= \frac{-(x_6 - y_6) \mathbf{a}_1 - (x_6 + y_6) \mathbf{a}_2 - z_6 \mathbf{a}_3}{z_6} = -ax_6 \hat{\mathbf{x}} - by_6 \hat{\mathbf{y}} - cz_6 \hat{\mathbf{z}} & (16g) & \text{Ni II} \\
\mathbf{B}_{24} &= \frac{(x_6 - y_6 + \frac{1}{2}) \mathbf{a}_1 + (x_6 + y_6 + \frac{1}{2}) \mathbf{a}_2 - (z_6 - \frac{1}{2}) \mathbf{a}_3}{z_6} = a(x_6 + \frac{1}{2}) \hat{\mathbf{x}} + by_6 \hat{\mathbf{y}} - c(z_6 - \frac{1}{2}) \hat{\mathbf{z}} & (16g) & \text{Ni II} \\
\mathbf{B}_{25} &= \frac{(x_6 + y_6 + \frac{1}{2}) \mathbf{a}_1 + (x_6 - y_6 + \frac{1}{2}) \mathbf{a}_2 + (z_6 + \frac{1}{2}) \mathbf{a}_3}{z_6} = a(x_6 + \frac{1}{2}) \hat{\mathbf{x}} - by_6 \hat{\mathbf{y}} + c(z_6 + \frac{1}{2}) \hat{\mathbf{z}} & (16g) & \text{Ni II} \\
\mathbf{B}_{26} &= \frac{-(x_6 + y_6) \mathbf{a}_1 - (x_6 - y_6) \mathbf{a}_2 + z_6 \mathbf{a}_3}{z_6} = -ax_6 \hat{\mathbf{x}} + by_6 \hat{\mathbf{y}} + cz_6 \hat{\mathbf{z}} & (16g) & \text{Ni II} \\
\mathbf{B}_{27} &= \frac{(x_7 - y_7) \mathbf{a}_1 + (x_7 + y_7) \mathbf{a}_2 + z_7 \mathbf{a}_3}{z_7} = ax_7 \hat{\mathbf{x}} + by_7 \hat{\mathbf{y}} + cz_7 \hat{\mathbf{z}} & (16g) & \text{Ni III} \\
\mathbf{B}_{28} &= \frac{(-x_7 + y_7 + \frac{1}{2}) \mathbf{a}_1 - (x_7 + y_7 - \frac{1}{2}) \mathbf{a}_2 + (z_7 + \frac{1}{2}) \mathbf{a}_3}{z_7} = -a(x_7 - \frac{1}{2}) \hat{\mathbf{x}} - by_7 \hat{\mathbf{y}} + c(z_7 + \frac{1}{2}) \hat{\mathbf{z}} & (16g) & \text{Ni III} \\
\mathbf{B}_{29} &= \frac{-(x_7 + y_7 - \frac{1}{2}) \mathbf{a}_1 + (-x_7 + y_7 + \frac{1}{2}) \mathbf{a}_2 - (z_7 - \frac{1}{2}) \mathbf{a}_3}{z_7} = -a(x_7 - \frac{1}{2}) \hat{\mathbf{x}} + by_7 \hat{\mathbf{y}} - c(z_7 - \frac{1}{2}) \hat{\mathbf{z}} & (16g) & \text{Ni III} \\
\mathbf{B}_{30} &= \frac{(x_7 + y_7) \mathbf{a}_1 + (x_7 - y_7) \mathbf{a}_2 - z_7 \mathbf{a}_3}{z_7} = ax_7 \hat{\mathbf{x}} - by_7 \hat{\mathbf{y}} - cz_7 \hat{\mathbf{z}} & (16g) & \text{Ni III} \\
\mathbf{B}_{31} &= \frac{-(x_7 - y_7) \mathbf{a}_1 - (x_7 + y_7) \mathbf{a}_2 - z_7 \mathbf{a}_3}{z_7} = -ax_7 \hat{\mathbf{x}} - by_7 \hat{\mathbf{y}} - cz_7 \hat{\mathbf{z}} & (16g) & \text{Ni III} \\
\mathbf{B}_{32} &= \frac{(x_7 - y_7 + \frac{1}{2}) \mathbf{a}_1 + (x_7 + y_7 + \frac{1}{2}) \mathbf{a}_2 - (z_7 - \frac{1}{2}) \mathbf{a}_3}{z_7} = a(x_7 + \frac{1}{2}) \hat{\mathbf{x}} + by_7 \hat{\mathbf{y}} - c(z_7 - \frac{1}{2}) \hat{\mathbf{z}} & (16g) & \text{Ni III} \\
\mathbf{B}_{33} &= \frac{(x_7 + y_7 + \frac{1}{2}) \mathbf{a}_1 + (x_7 - y_7 + \frac{1}{2}) \mathbf{a}_2 + (z_7 + \frac{1}{2}) \mathbf{a}_3}{z_7} = a(x_7 + \frac{1}{2}) \hat{\mathbf{x}} - by_7 \hat{\mathbf{y}} + c(z_7 + \frac{1}{2}) \hat{\mathbf{z}} & (16g) & \text{Ni III} \\
\mathbf{B}_{34} &= \frac{-(x_7 + y_7) \mathbf{a}_1 - (x_7 - y_7) \mathbf{a}_2 + z_7 \mathbf{a}_3}{z_7} = -ax_7 \hat{\mathbf{x}} + by_7 \hat{\mathbf{y}} + cz_7 \hat{\mathbf{z}} & (16g) & \text{Ni III}
\end{aligned}$$

## References

- [1] J.-M. Joubert, R. Cerný, K. Yvon, M. Latroche, and A. Percheron-Guégan, *Zirconium-Nickel, Zr<sub>7</sub>Ni<sub>10</sub>: Space Group Revision for the Stoichiometric Phase*, Acta Crystallogr. Sect. C **53**, 1536–1538 (1977), doi:10.1107/S0108270197007142.
- [2] M. E. Kirkpatrick, J. F. Smith, and W. L. Larsen, *Structures of the intermediate phases Ni<sub>10</sub>Zr<sub>7</sub> and Ni<sub>10</sub>Hf<sub>7</sub>*, Acta Cryst. **15**, 894–903 (1962), doi:10.1107/S0365110X62002339.
- [3] W. B. Pearson, *A Handbook of Lattice Spacings and Structures of Metals and Alloys, Volume 2, International Series of Monographs on Metal Physics and Physical Metallurgy*, vol. 8 (Pergamon Press, Oxford, London, Edinburgh, New York, Toronto, Sydney, Paris, Braunschweig, 1967).

## Found in

- [1] H. Shen, L. A. Bendersky, K. Young, , and J. Nei, *Fine Structure in Multi-Phase Zr<sub>8</sub>Ni<sub>21</sub>-Zr<sub>7</sub>Ni<sub>10</sub>-Zr<sub>2</sub>Ni<sub>7</sub> Alloy Revealed by Transmission Electron Microscope*, Materials **8**, 4618–4630 (2015), doi:10.3390/ma8074618.